

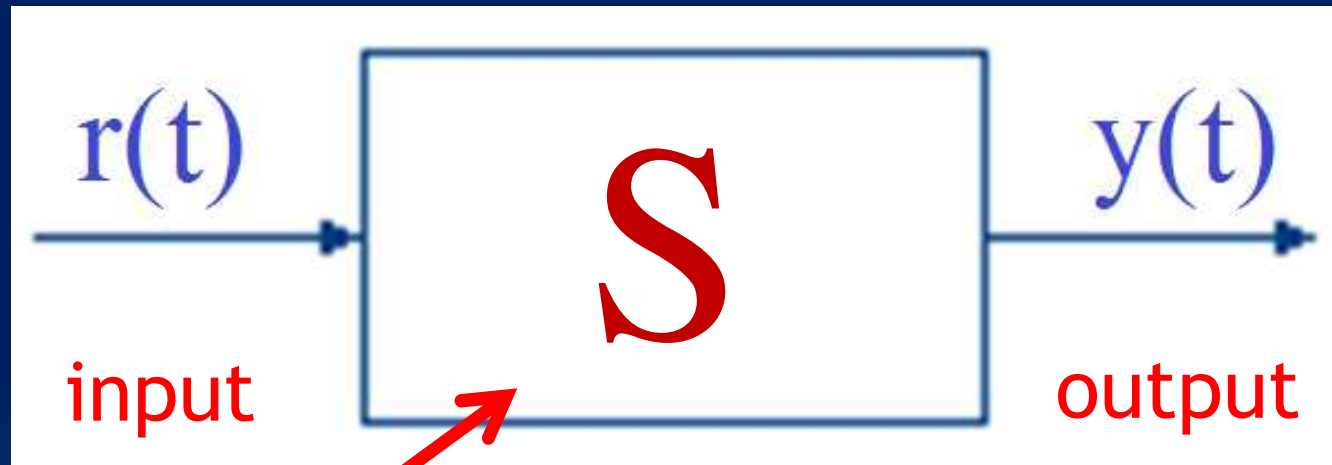
Controlo de Sistemas

7

“Análise no domínio do tempo”
(*Time domain analysis*)

parte II – Sistemas de 2ª ordem

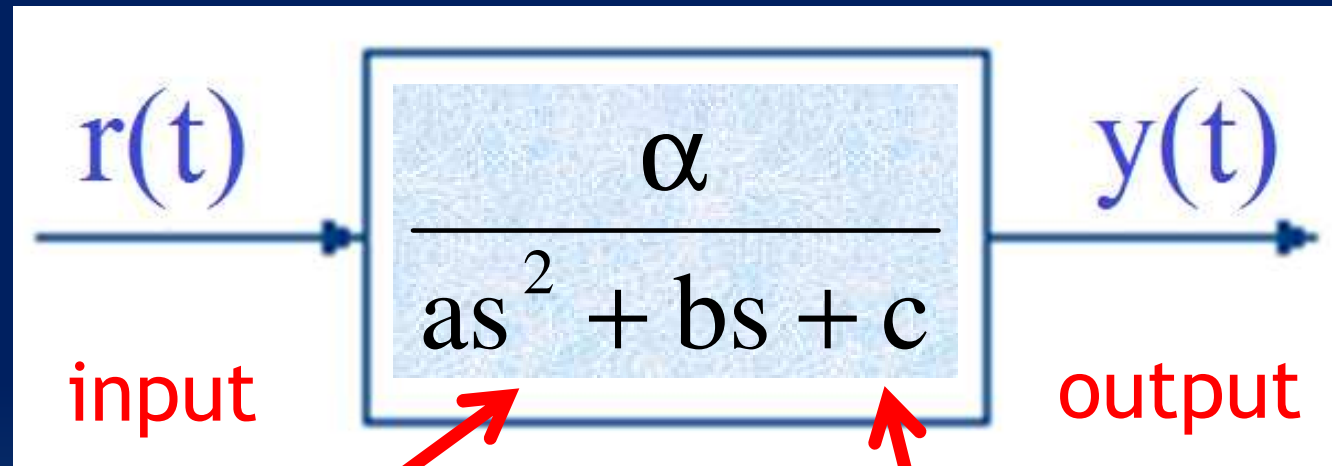
J. A. M. Felippe de Souza



Sistema de segunda ordem

do tipo

$$G(s) = \frac{\alpha}{as^2 + bs + c}$$

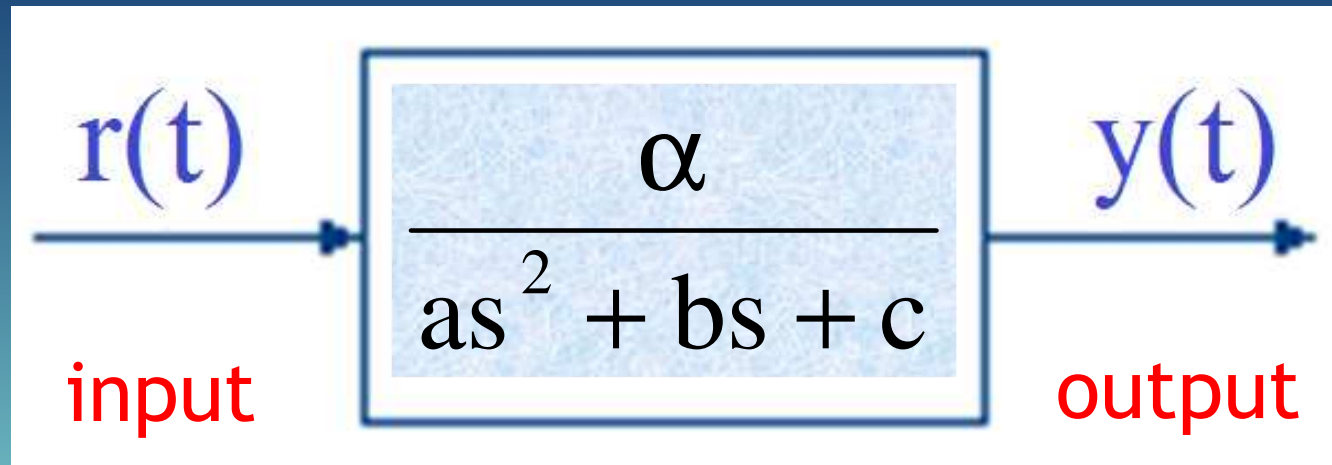


Sistema de segunda ordem

do tipo

$$G(s) = \frac{\alpha}{as^2 + bs + c}$$

Sistemas de segunda ordem:



ou seja:

$$\frac{Y(s)}{R(s)} = \frac{\alpha}{as^2 + bs + c}$$



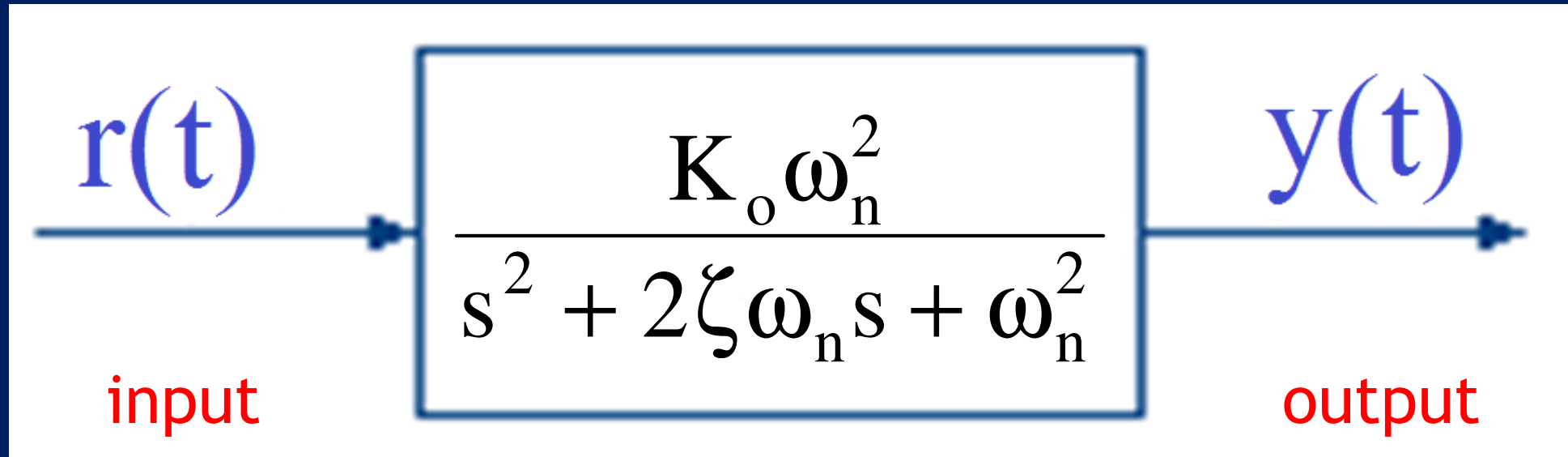
$$\frac{Y(s)}{R(s)} =$$

$$\frac{\frac{\alpha}{a}}{s^2 + \frac{b}{a}s + \frac{c}{a}}$$

$$K_o \omega_n^2$$

$$2\zeta\omega_n$$

$$\omega_n^2$$



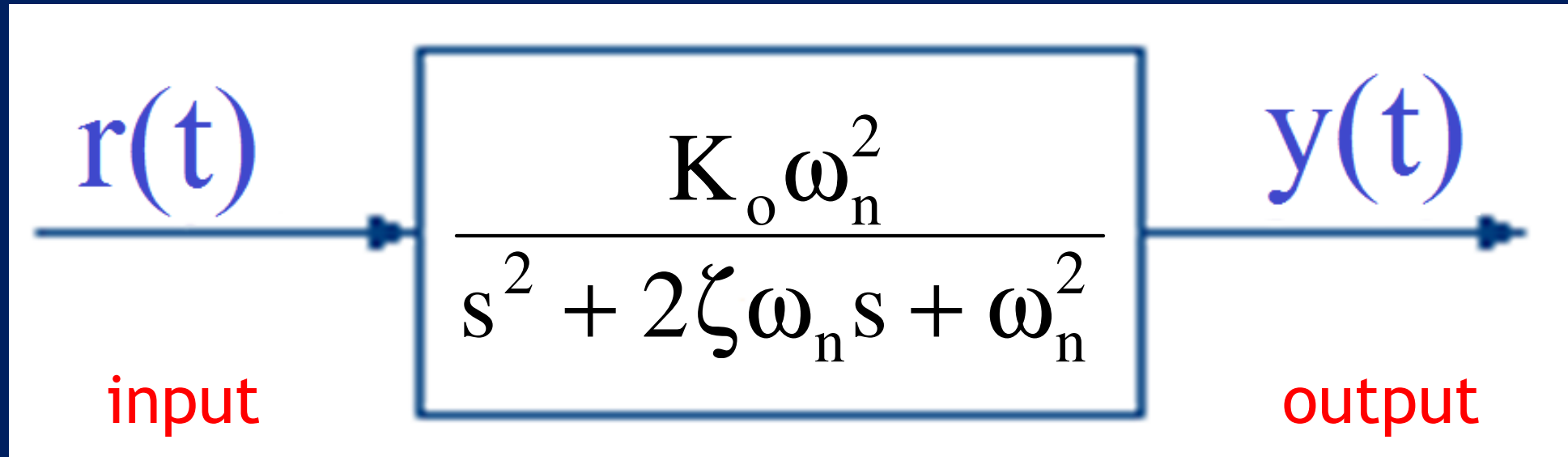
K_o = ganho do sistema

ζ = coeficiente de amortecimento

ω_n = frequência natural

a função de transferência:

$$\frac{Y(s)}{R(s)} = \frac{K_o \omega_n^2}{s^2 + 2\zeta \omega_n s + \omega_n^2}$$



K_o = ganho do sistema

ζ = coeficiente de amortecimento

ω_n = frequência natural

Além destes 3 parâmetros acima, temos também

ω_d = frequência natural amortecida
(*'damping frequency'*)

$$\omega_d = \omega_n \cdot \sqrt{1 - \zeta^2} \quad 0 < \zeta \leq 1$$

Exemplo 1:

$$\frac{Y(s)}{R(s)} = \frac{3}{4s^2 + 12s + 1}$$

pólos:

$$s = -2,914$$

$$s = -0,086$$

$$K_o = 3 \quad \zeta = 3 \quad \omega_n = 0,5$$

polos reais
e distintos

Exemplo 2:

$$\frac{Y(s)}{R(s)} = \frac{3}{s^2 + 2s + 1}$$

polos:

$$s = -1$$

(duplo)

$$K_o = 3 \quad \zeta = 1 \quad \omega_n = 1 \quad \omega_d = 0$$

polos reais
e duplos

Exemplo 3:

$$\frac{Y(s)}{R(s)} = \frac{3}{2s^2 + 2s + 2}$$

polos:

$$s = -0,5 \pm 0,866j$$

$$K_o = 1,5 \quad \zeta = 0,5 \quad \omega_n = 1 \quad \omega_d = 0,866$$

polos
complexos
conjugados

Exemplo 4:

$$\frac{Y(s)}{R(s)} = \frac{3}{s^2 + 1}$$

polos:

$$s = \pm j$$

(imaginários puros)

$$K_o = 3 \quad \zeta = 0 \quad \omega_n = \omega_d = 1$$

polos
complexos
conjugados

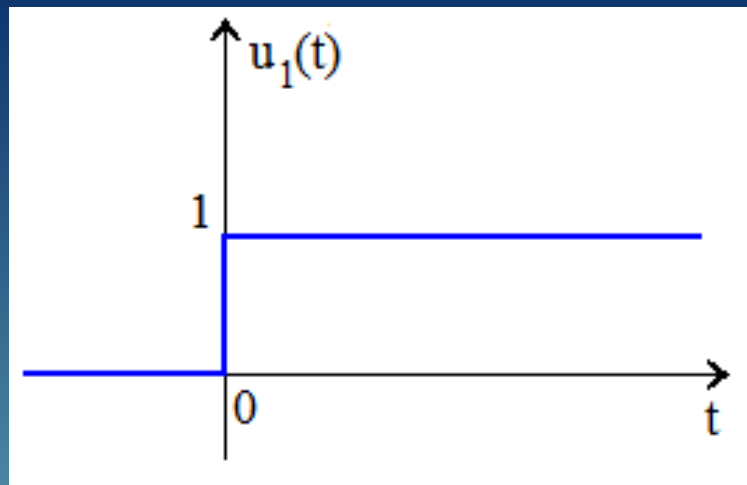
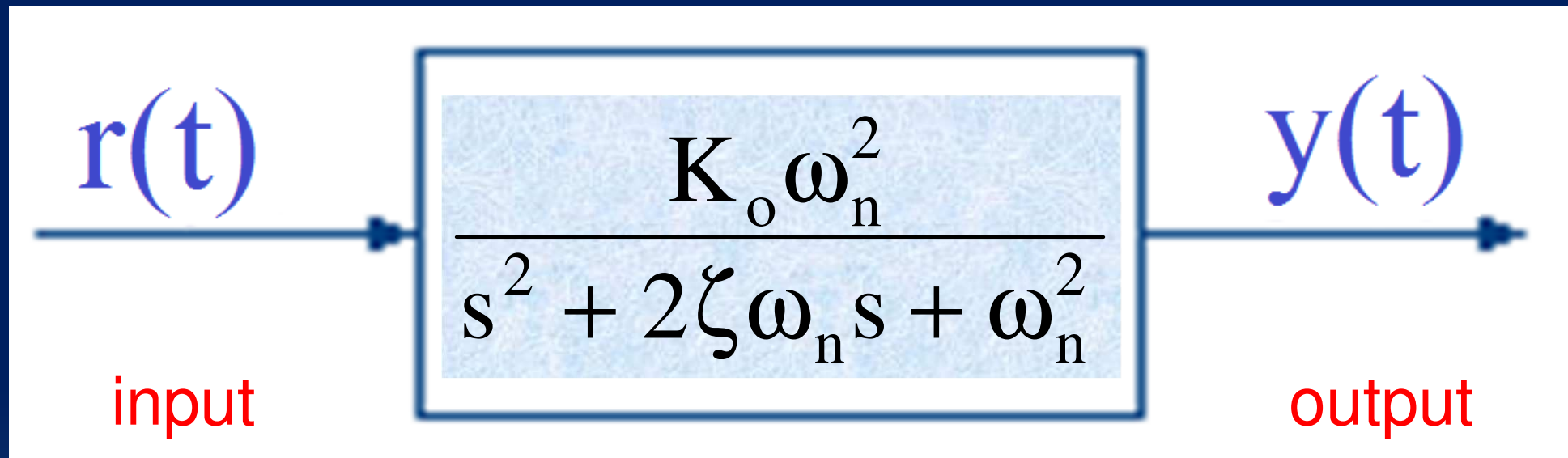
Equação característica:

$$p(s) = s^2 + 2\zeta\omega_n s + \omega_n^2$$

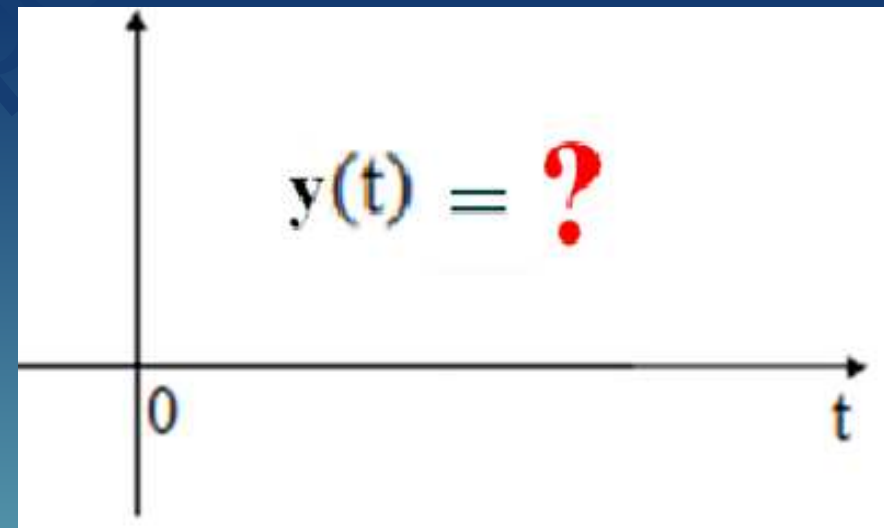
$$\begin{aligned}\Delta &= 4\zeta^2\omega_n^2 - 4\omega_n^2 = \\ &= 4\omega_n^2(\zeta^2 - 1)\end{aligned}$$

$$\left\{ \begin{array}{l} \Delta > 0 \rightarrow (\zeta^2 - 1) > 0 \rightarrow \zeta^2 > 1 \rightarrow \zeta > 1 \\ \Delta = 0 \rightarrow (\zeta^2 - 1) = 0 \rightarrow \zeta^2 = 1 \rightarrow \zeta = 1 \\ \Delta < 0 \rightarrow (\zeta^2 - 1) < 0 \rightarrow \zeta^2 < 1 \rightarrow \zeta < 1 \end{array} \right.$$

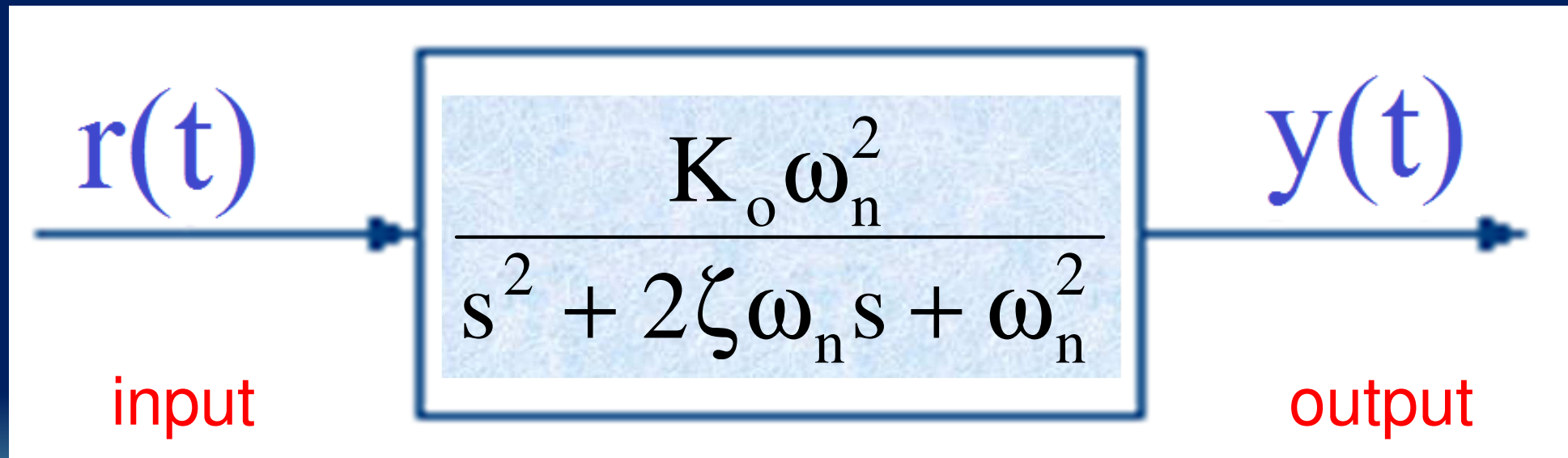
$\zeta > 1 \rightarrow$ polos reais e distintos
 $\zeta = 1 \rightarrow$ polos reais e duplos
 $0 < \zeta < 1 \rightarrow$ polos complexos conjugados



Entrada degrau unitário



Qual é a resposta ao degrau?
(*step response*)

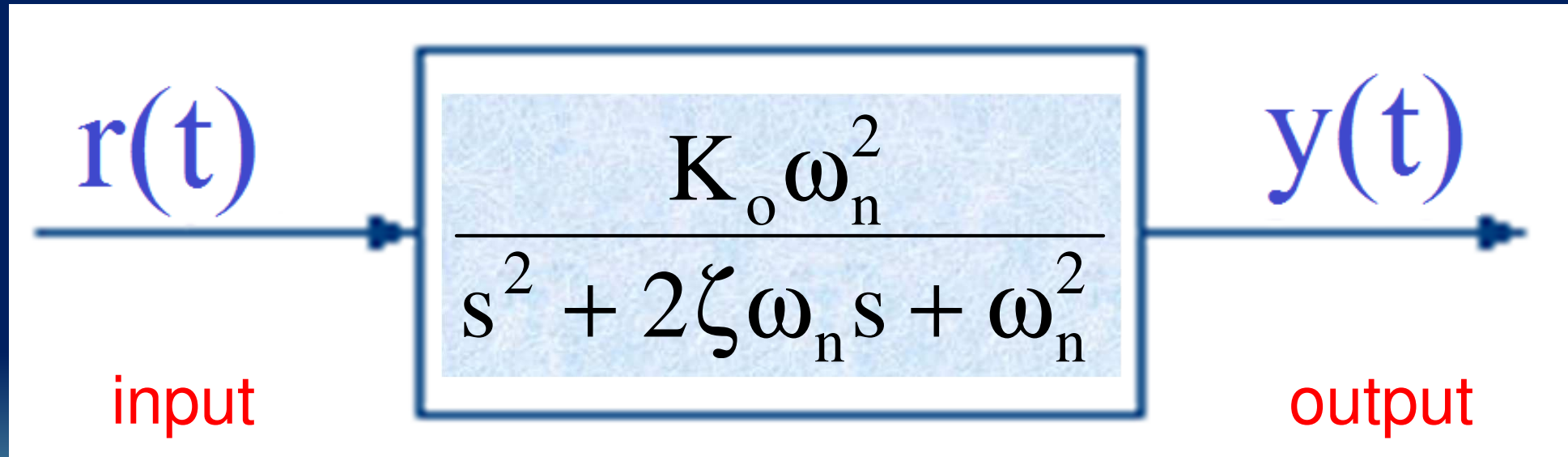


$$Y(s) = \frac{K_o \omega_n^2}{s^2 + 2\zeta \omega_n s + \omega_n^2} \cdot R(s)$$

e como $r(t)$ = degrau unitário:

$$Y(s) = \frac{K_o \omega_n^2}{s^2 + 2\zeta \omega_n s + \omega_n^2} \cdot \frac{1}{s}$$

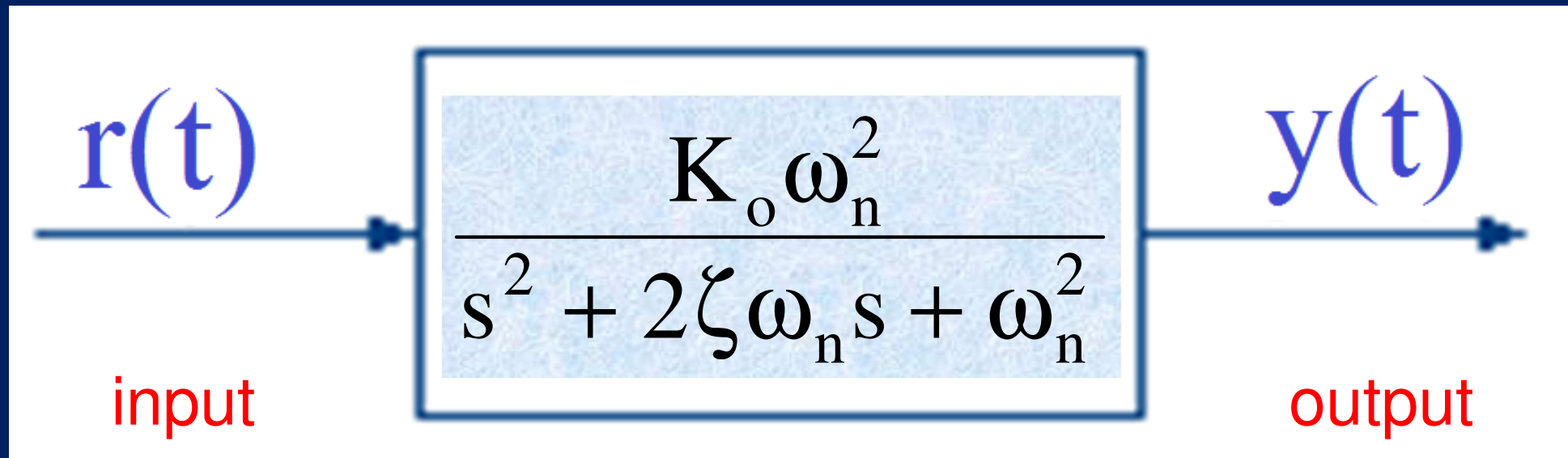
A red arrow points from the $R(s)$ term in the equation above to the $\frac{1}{s}$ term in this equation, which is circled in red.



$$y(t) = \mathcal{L}^{-1}[Y(s)]$$

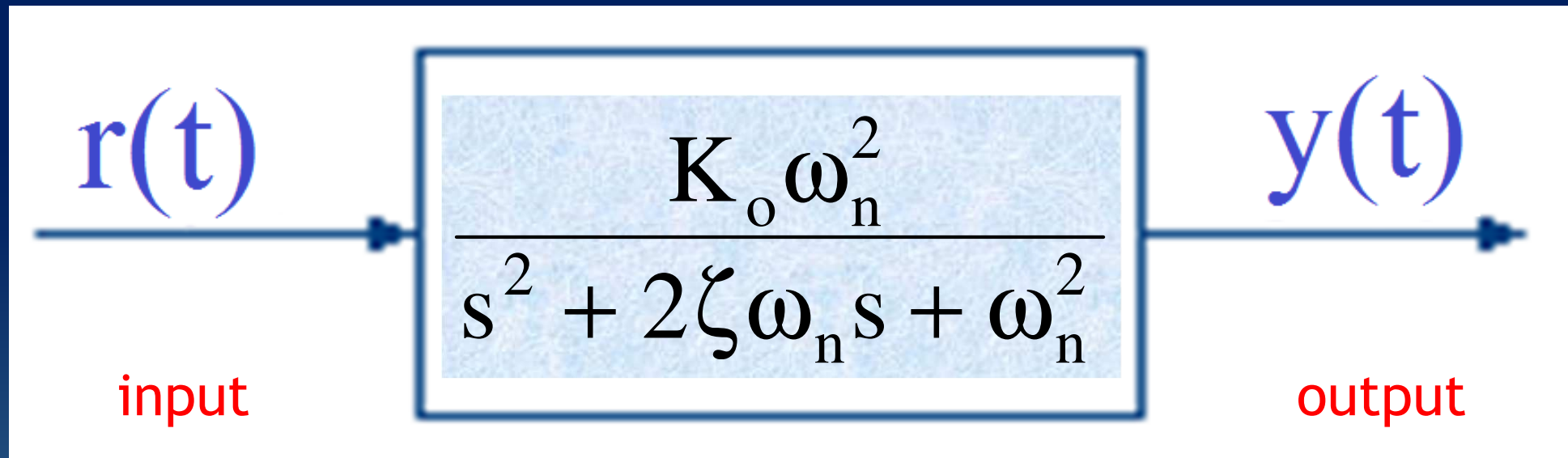
a resposta ao degrau unitário depende do valor de ζ

- a) $0 < \zeta < 1$ (sub amortecido)
- b) $\zeta = 1$ (*amortecimento crítico*)
- c) $\zeta > 1$ (*sobre amortecido*)



Vamos ver agora $y(t)$, as respostas ao **degrau unitário** nestes **3 casos**, a começar pelo caso (a)

a) $0 < \zeta < 1$ (sub amortecido)



$$y(t) = \mathcal{L}^{-1}[Y(s)]$$

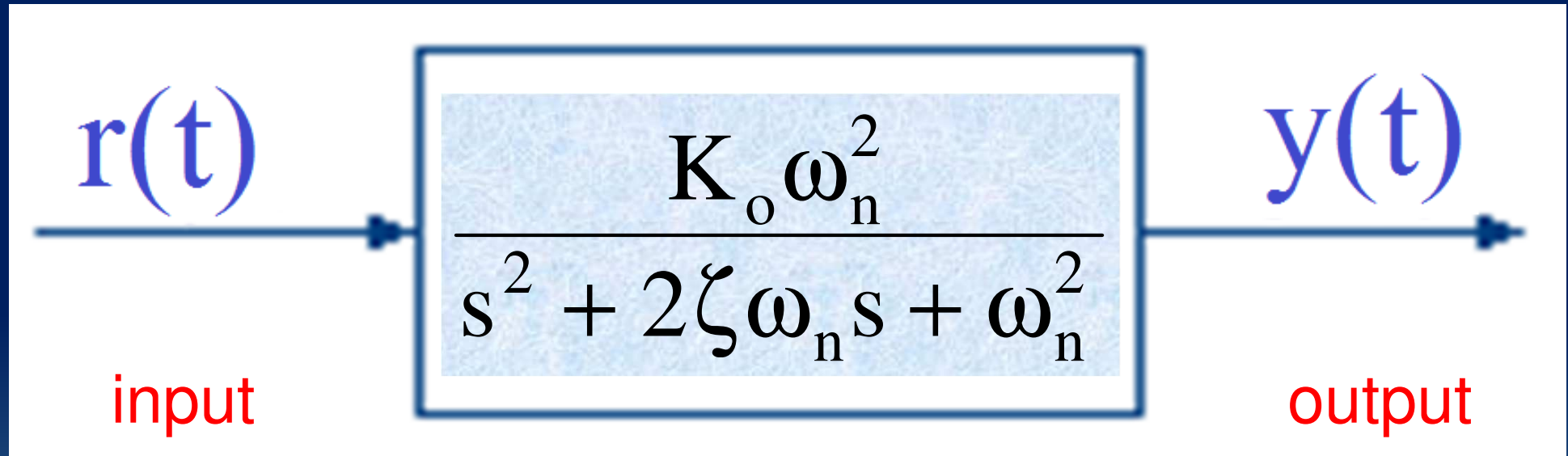
Logo, no caso de $0 < \zeta < 1$ (*sub amortecido*) a resposta ao **degrau unitário** é:

$$y(t) = K_o \left[1 - e^{-\zeta \omega_n t} \left(\cos \omega_d t + \frac{\zeta}{\sqrt{1 - \zeta^2}} \cdot \text{sen } \omega_d t \right) \right], \quad t > 0$$

onde

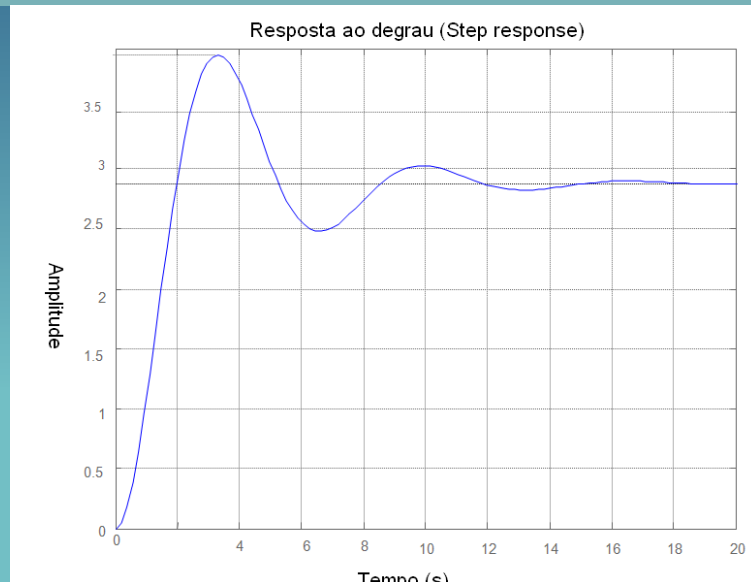
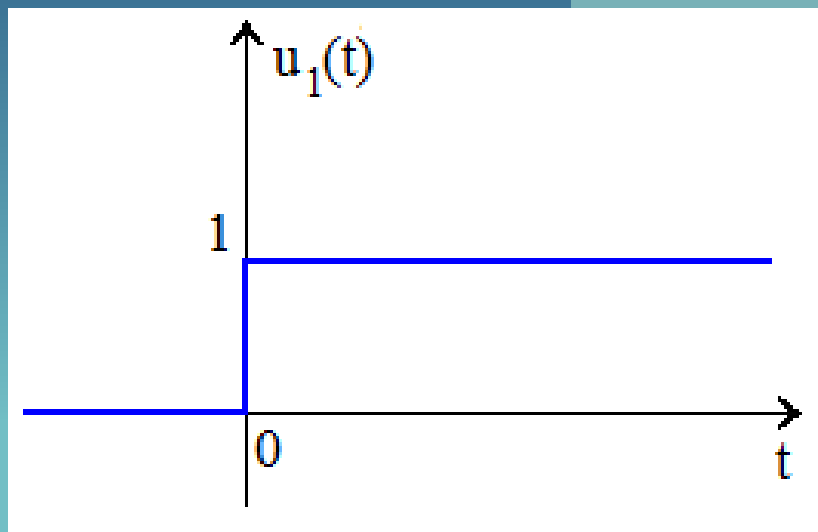
$$\omega_d = \omega_n \cdot \sqrt{1 - \zeta^2}$$

frequência natural amortecida
(*damping frequency*)

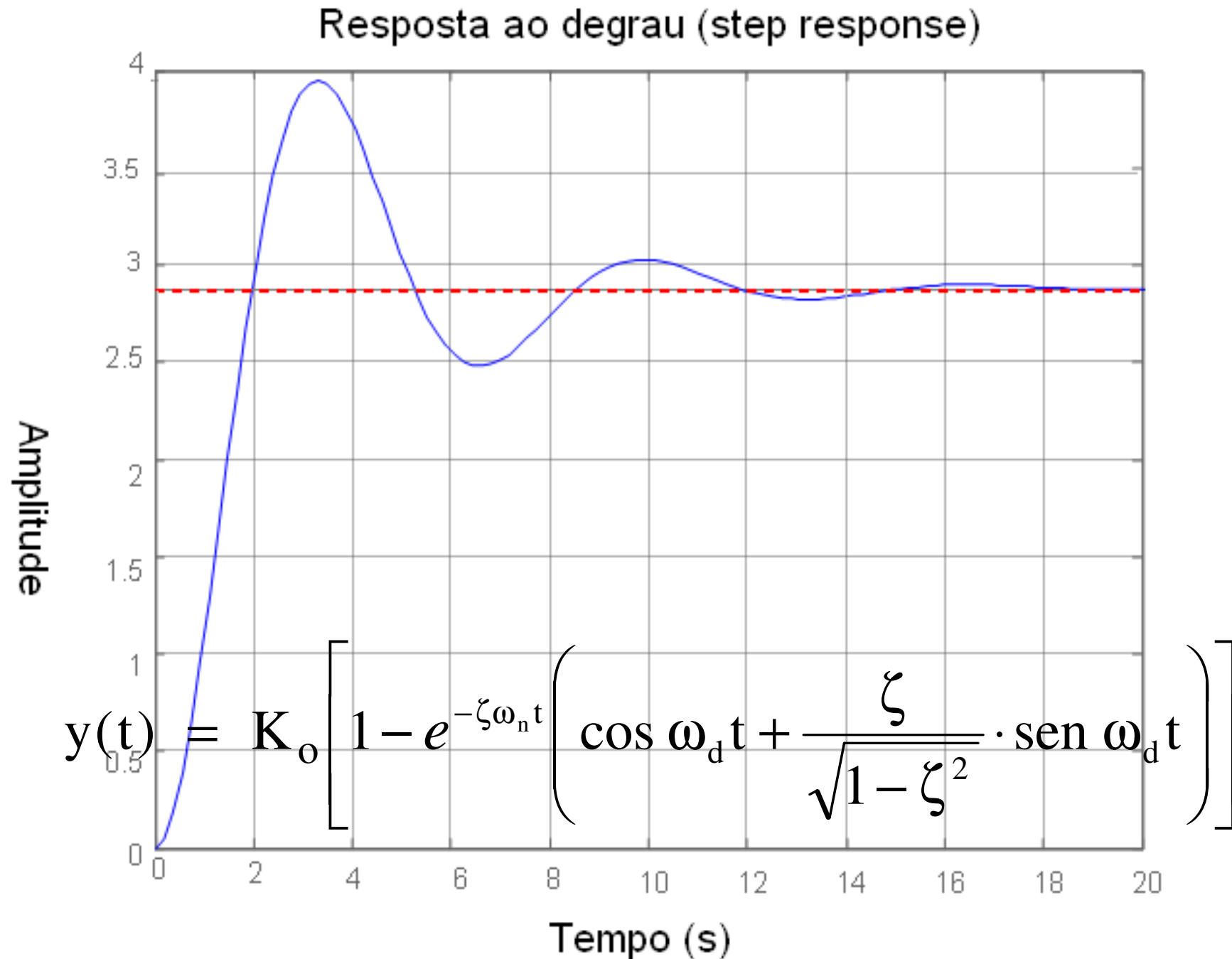


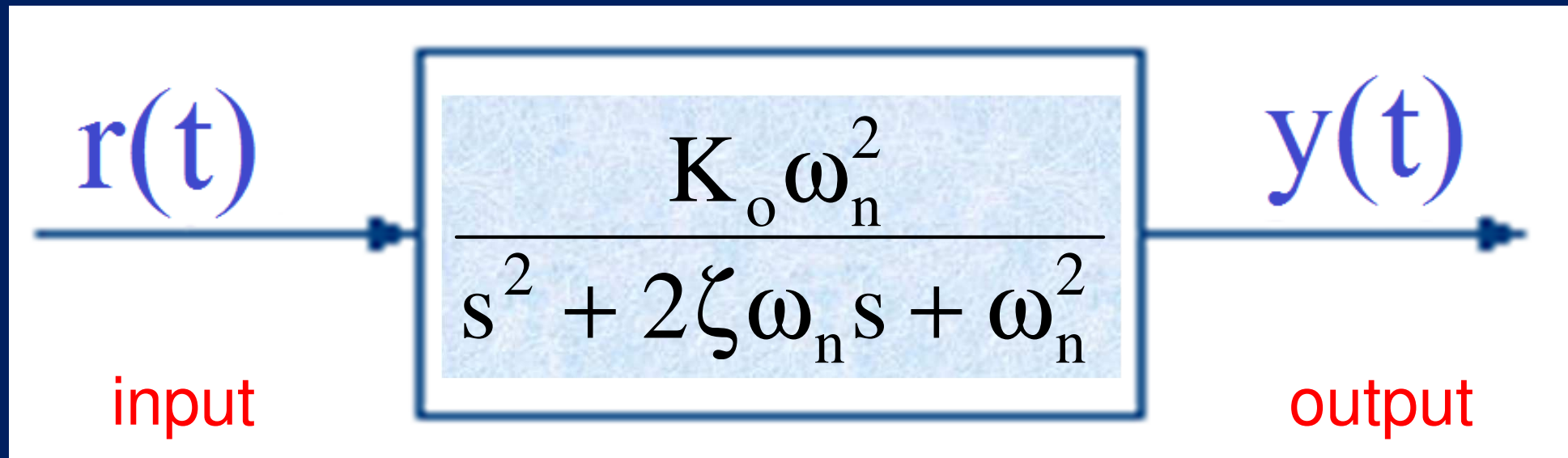
resposta ao degrau unitário:

$$y(t) = K_o \left[1 - e^{-\zeta \omega_n t} \left(\cos \omega_d t + \frac{\zeta}{\sqrt{1 - \zeta^2}} \cdot \text{sen } \omega_d t \right) \right]$$



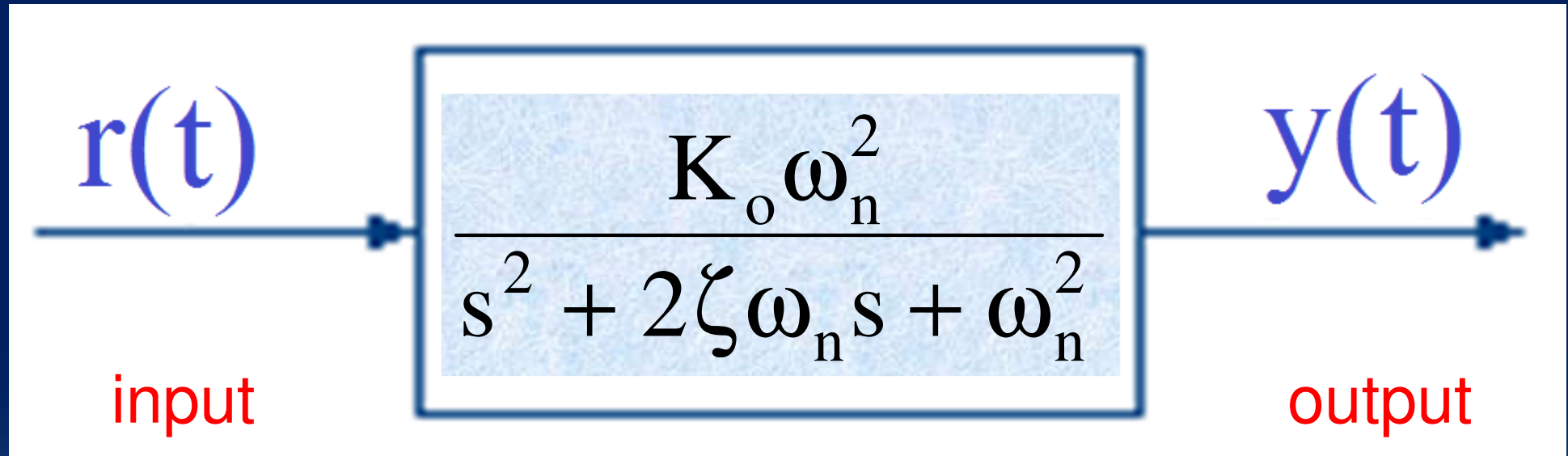
a resposta ao degrau unitário é:





Vamos agora ver $y(t)$, a resposta ao **degrau unitário** para o caso (b)

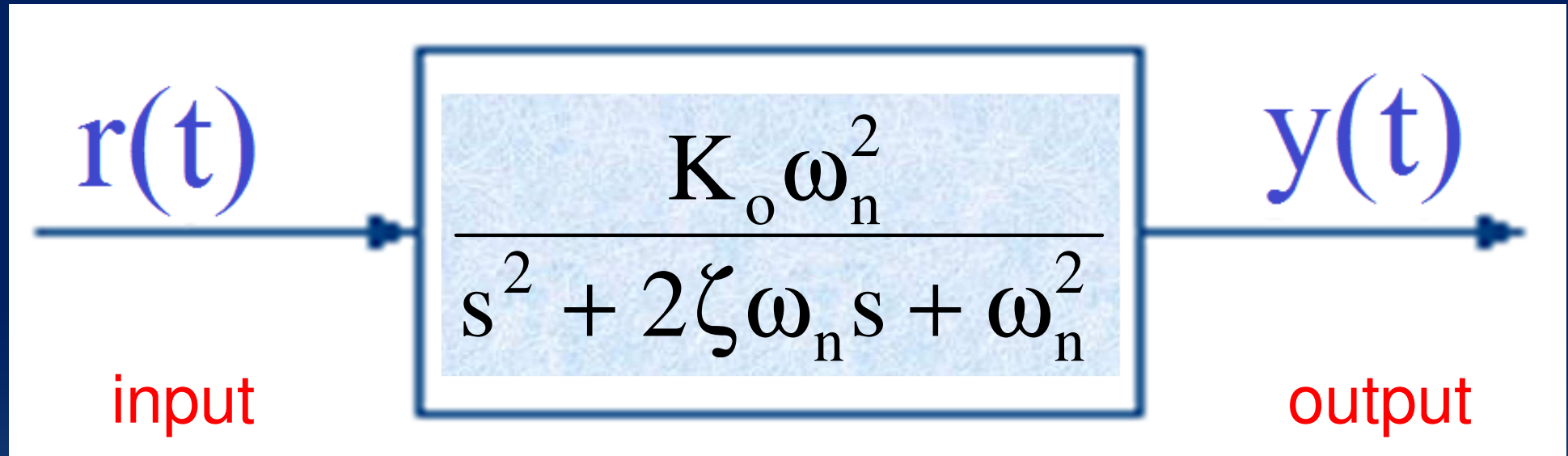
b) $\zeta = 1$ amortecimento crítico)



$$y(t) = \mathcal{L}^{-1}[Y(s)]$$

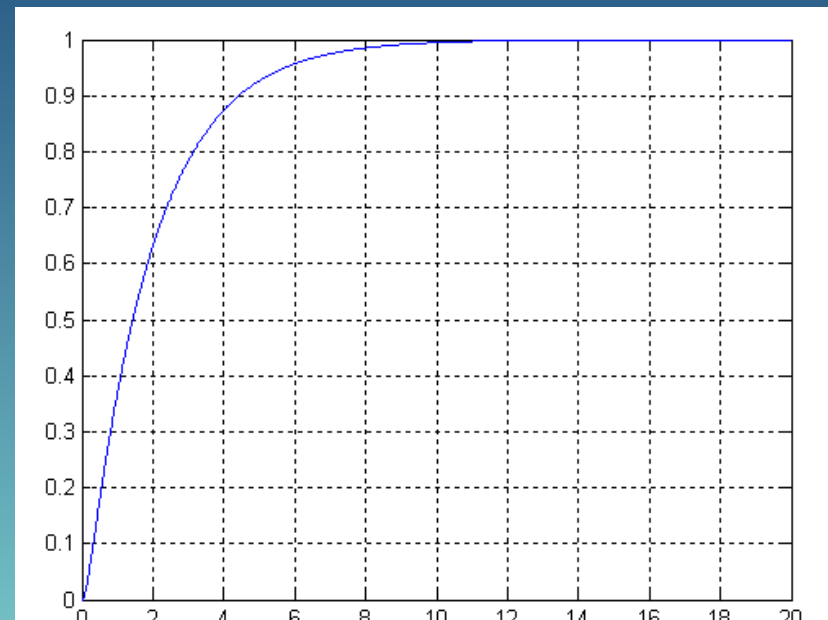
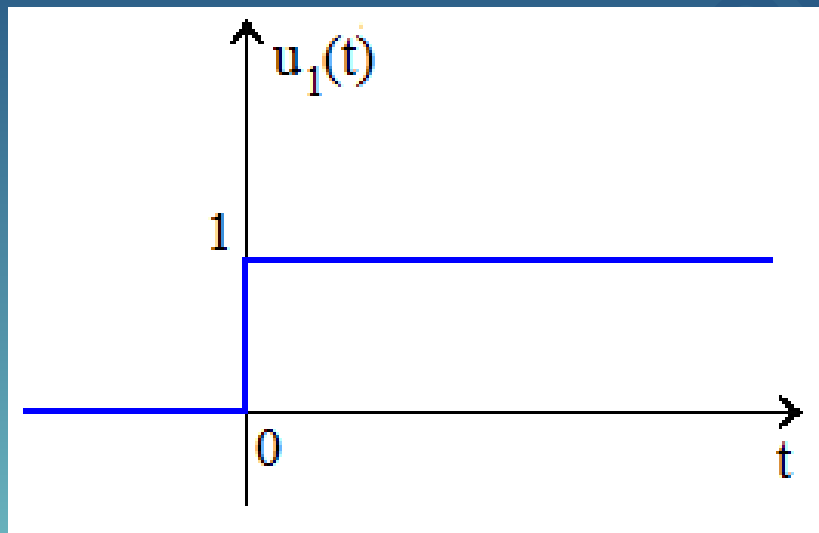
No caso de $\zeta = 1$ (*amortecimento crítico*), a resposta ao degrau unitário é:

$$y(t) = K_o \left[1 - e^{-\zeta \omega_n t} \cdot (1 + \omega_n t) \right], \quad t > 0$$

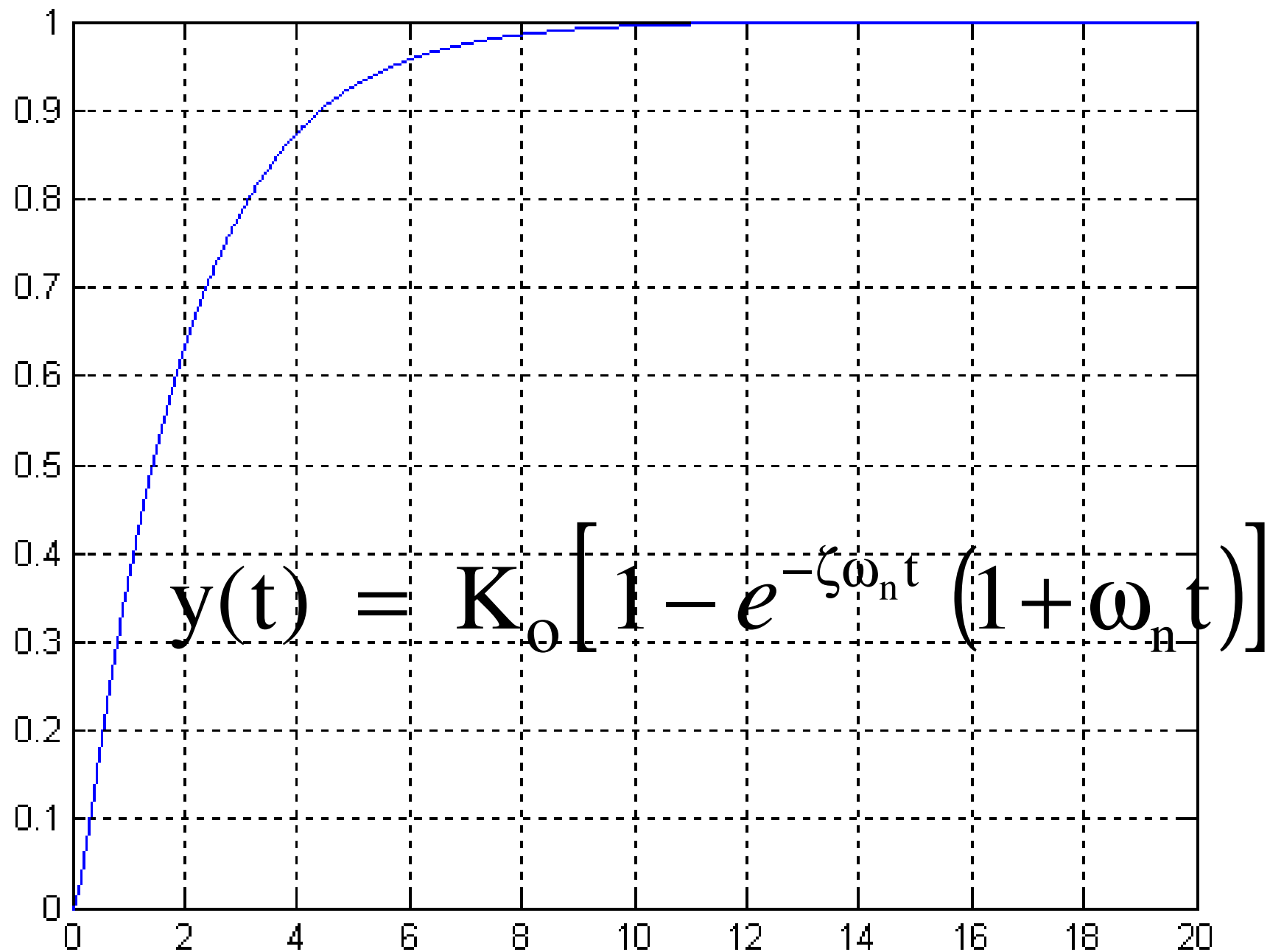


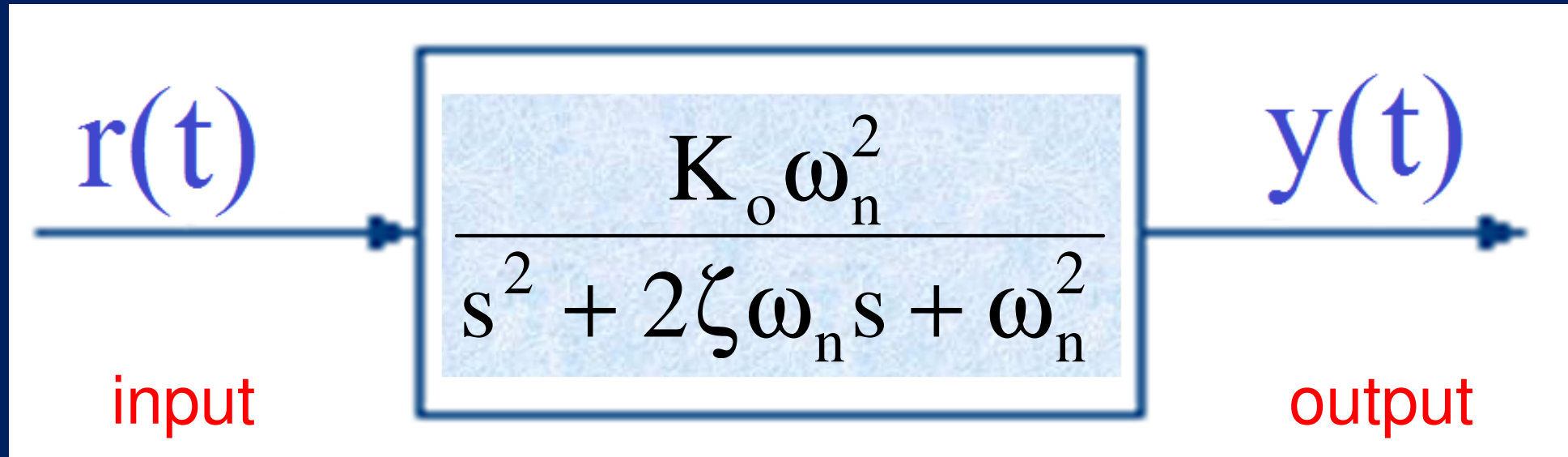
resposta ao degrau unitário:

$$y(t) = K_o \left[1 - e^{-\zeta \omega_n t} (1 + \omega_n t) \right]$$



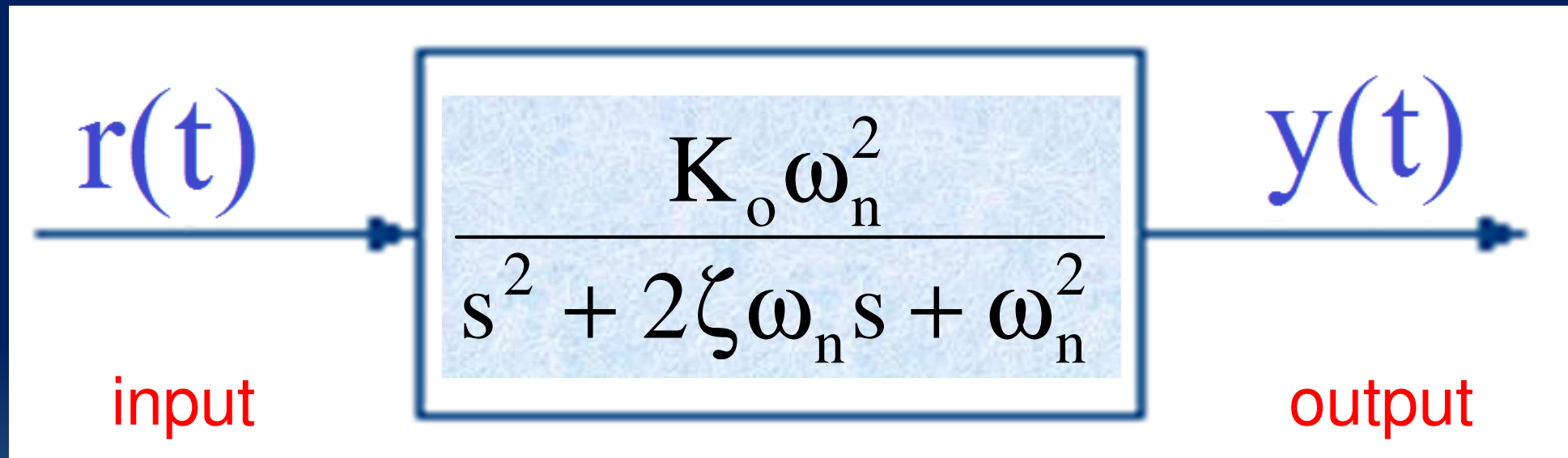
resposta ao degrau unitário é:





Finalmente, vamos agora ver $y(t)$, a resposta ao **degrau unitário** para o caso (c)

c) $\zeta > 1$ sobre-amortecido



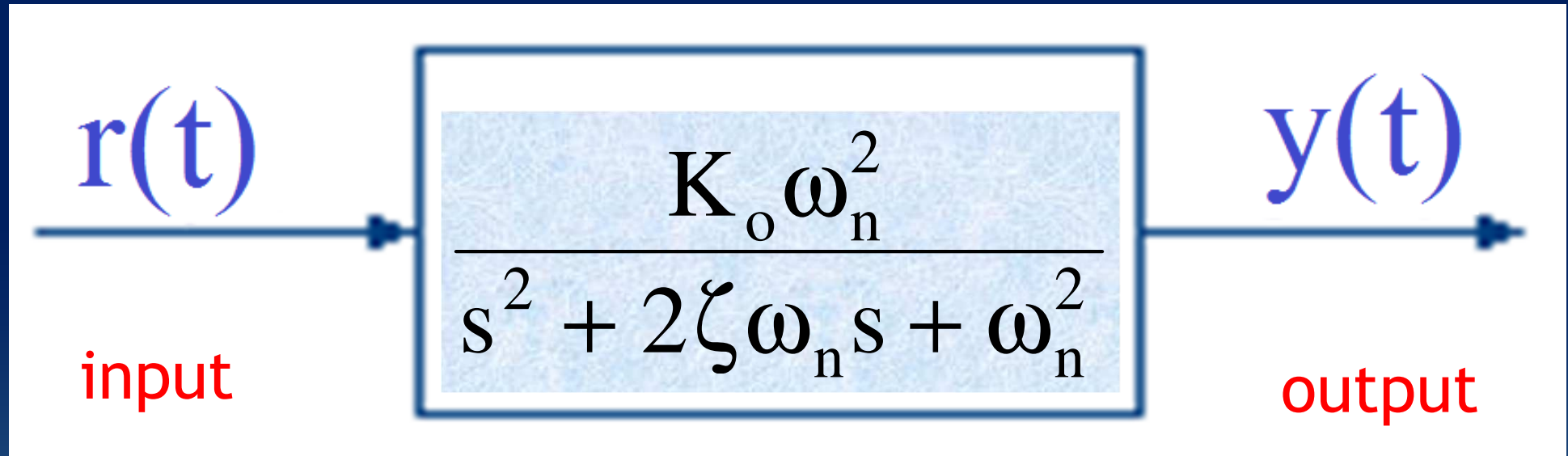
$$y(t) = \mathcal{L}^{-1}[Y(s)]$$

No caso de $\zeta > 1$ (*sobre amortecido*), a resposta ao degrau unitário é:

$$y(t) = K_o \left[1 + \frac{\omega_n}{2\sqrt{\zeta^2 - 1}} \cdot \left(\frac{e^{p_1 t}}{p_1} - \frac{e^{p_2 t}}{p_2} \right) \right], \quad t > 0$$

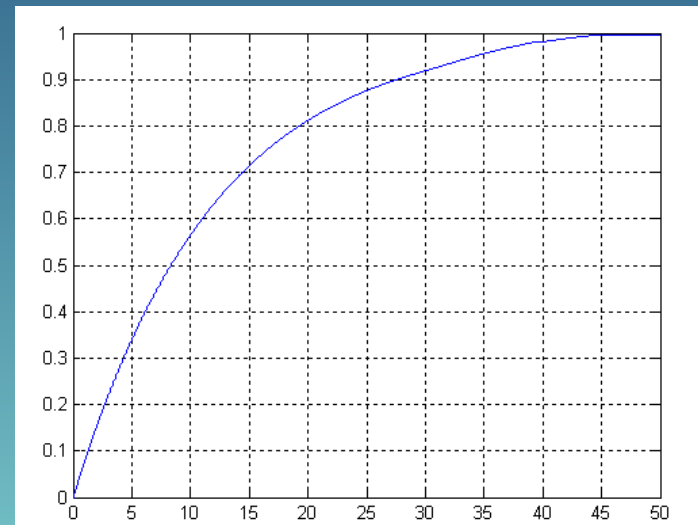
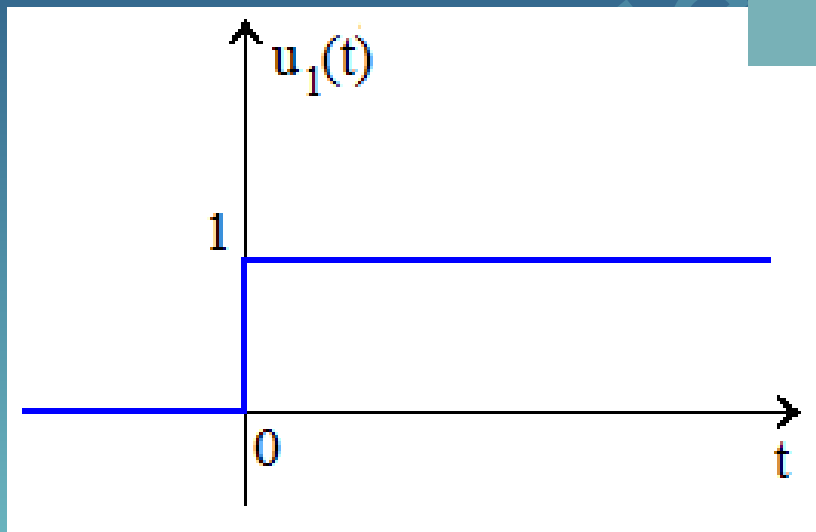
onde

$$p_{1,2} = -\zeta \omega_n \mp \omega_n \sqrt{\zeta^2 - 1} = -\omega_n \left(\zeta \pm \sqrt{\zeta^2 - 1} \right) \text{ Sistema tem polos reais}$$

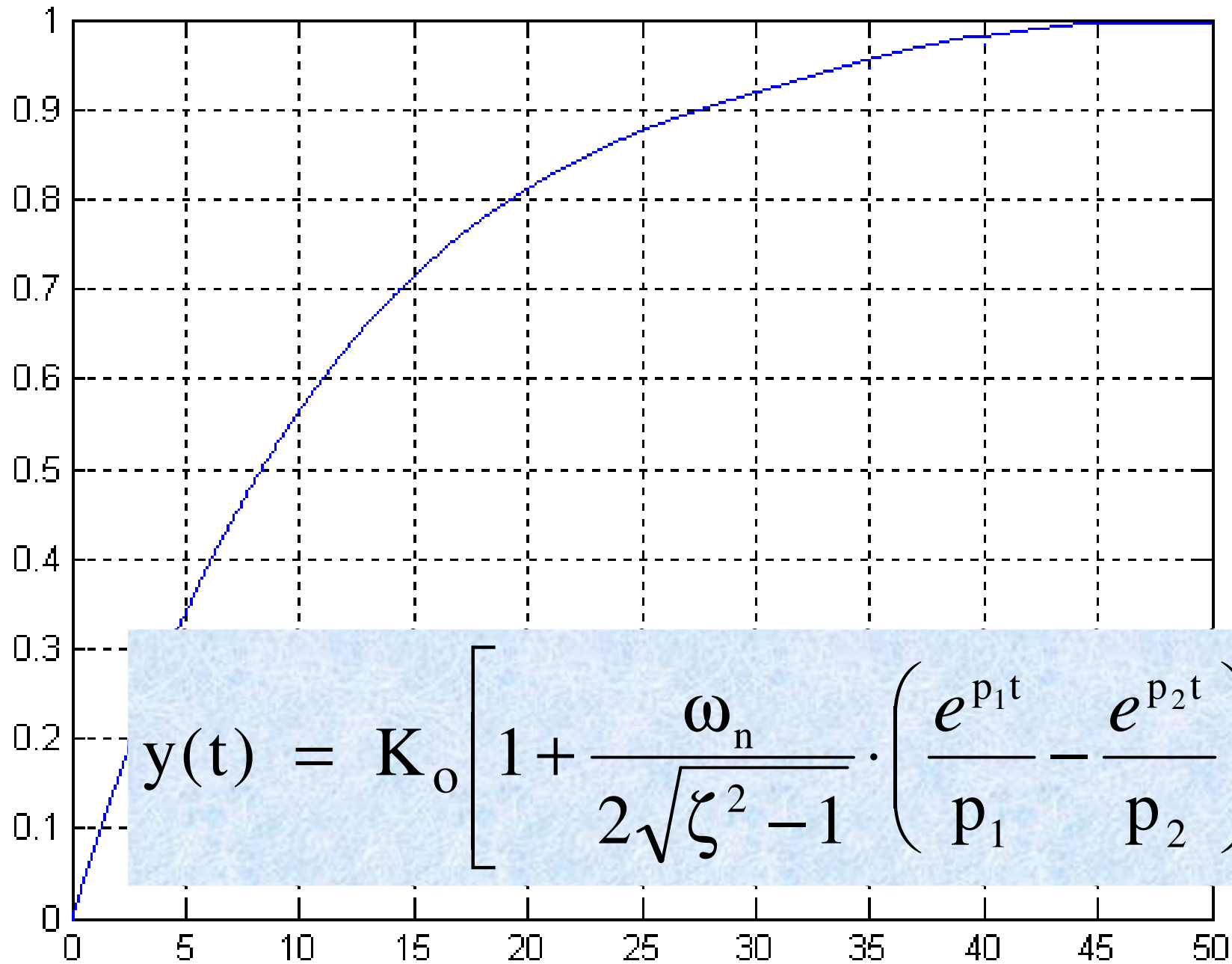


resposta ao degrau unitário:

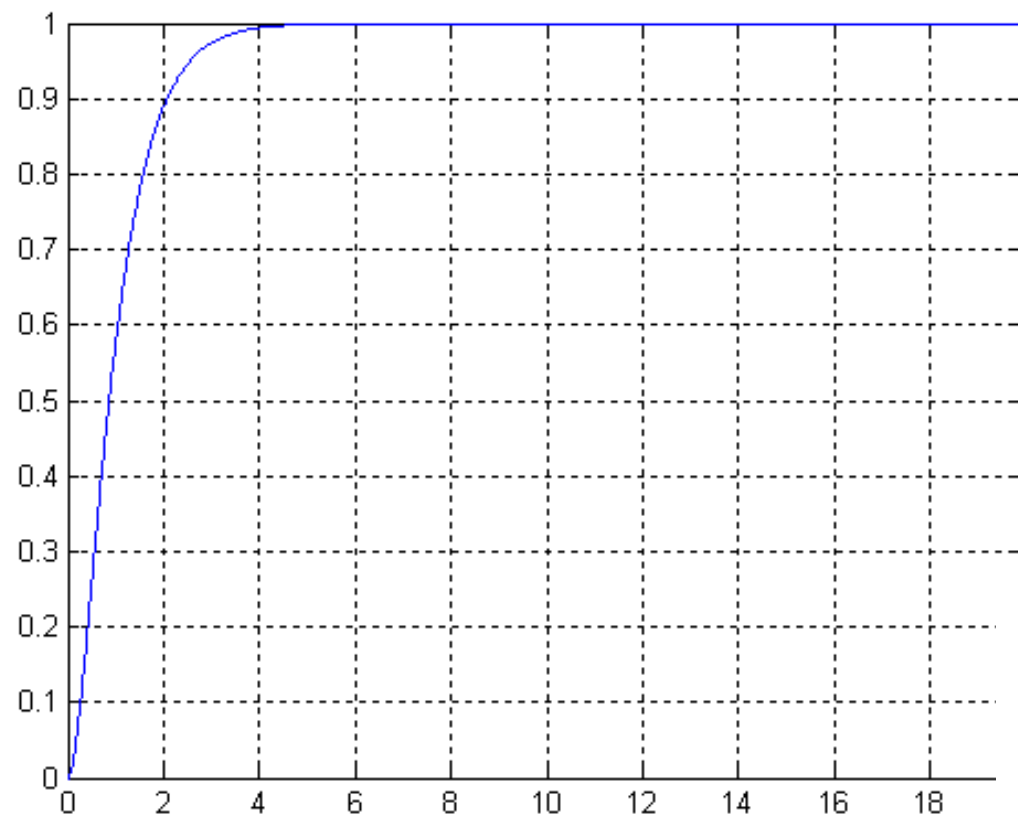
$$y(t) = K_o \left[1 + \frac{\omega_n}{2\sqrt{\zeta^2 - 1}} \cdot \left(\frac{e^{p_1 t}}{p_1} - \frac{e^{p_2 t}}{p_2} \right) \right]$$



resposta ao degrau unitário:



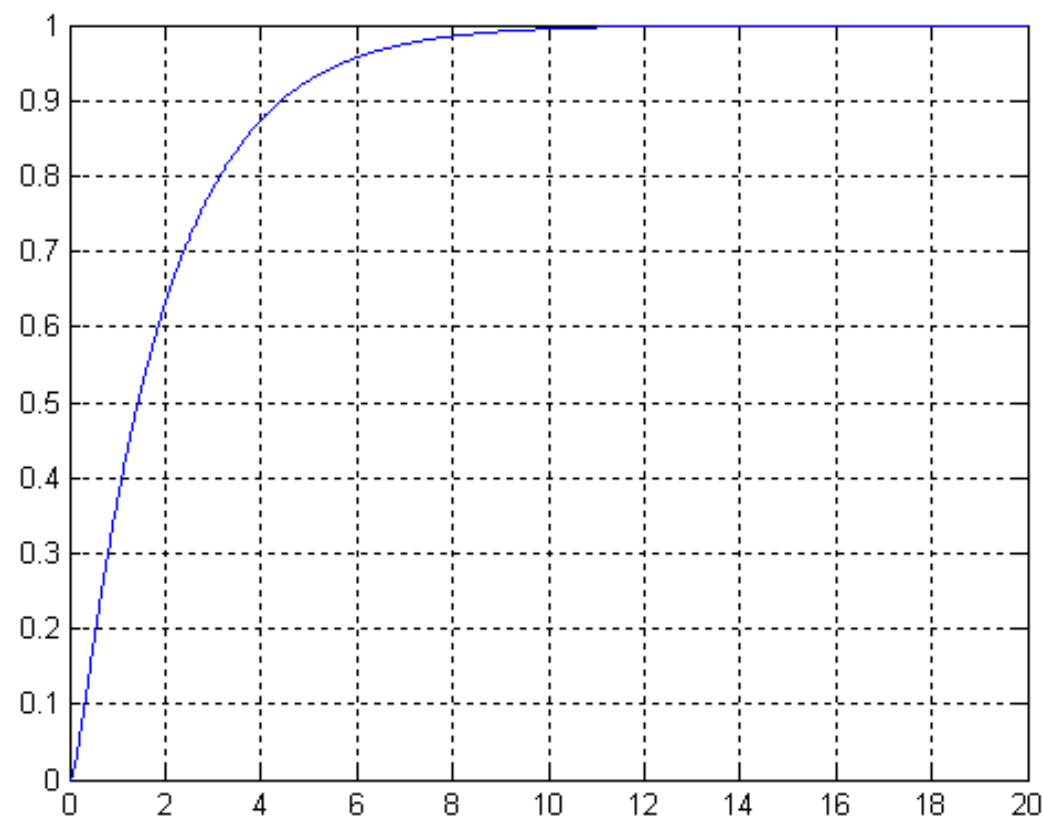
Análise no domínio do tempo - Sistemas de 2ª ordem



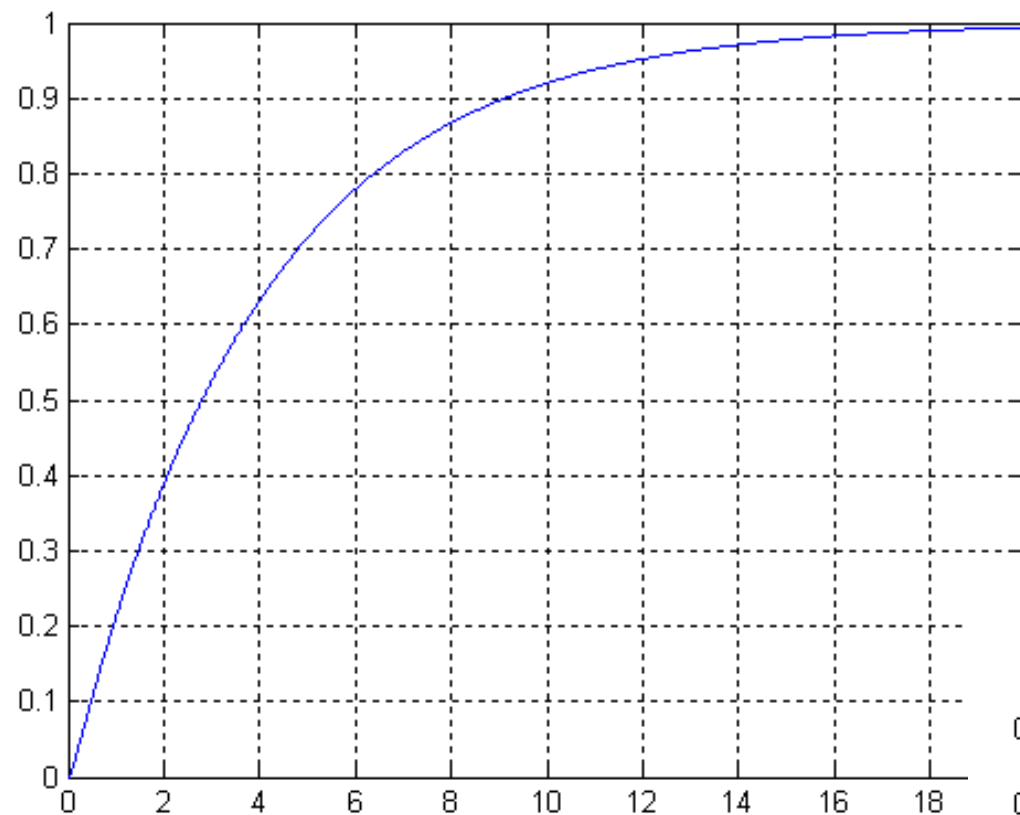
resposta ao
degrau unitário

$\zeta = 1$

$\zeta = 2$



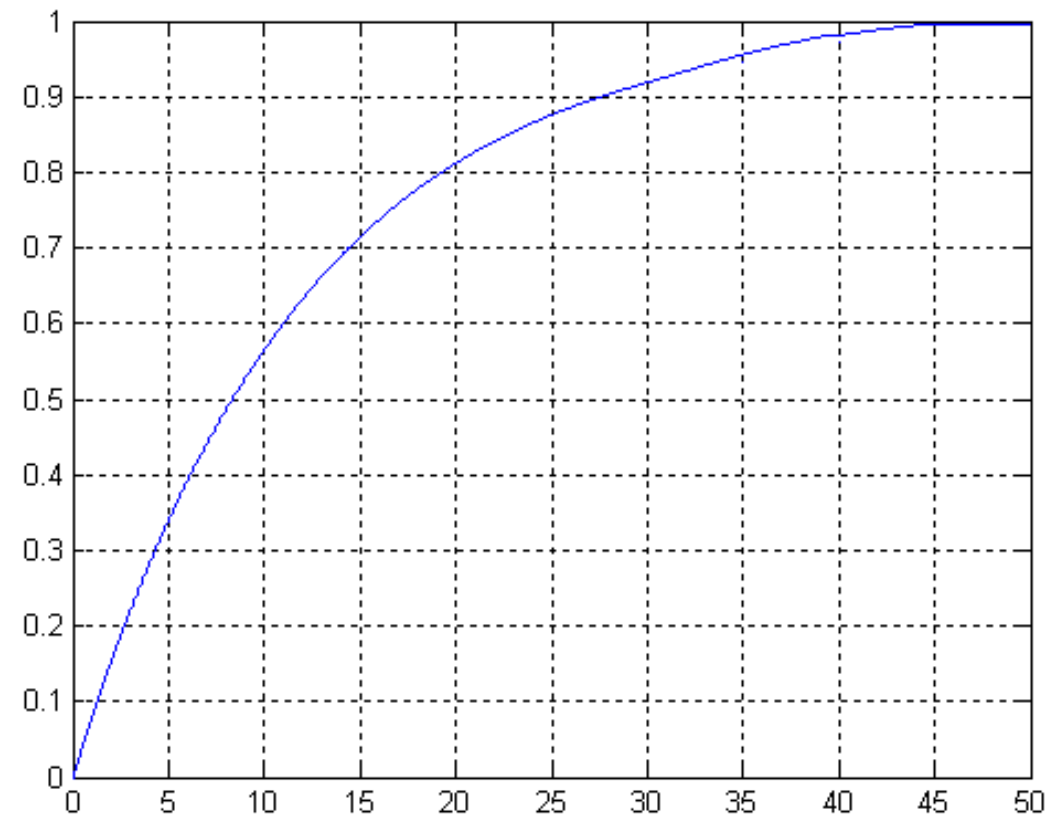
Análise no domínio do tempo - Sistemas de 2ª ordem



resposta ao
degrau unitário

$$\zeta = 4$$

$$\zeta = 12$$



Agora vamos analisar alguns parâmetros associados ao caso *sub amortecido*

$$0 < \zeta < 1 \text{ (sub amortecido)}$$

No caso $0 < \zeta < 1$,

A resposta ao degrau unitário

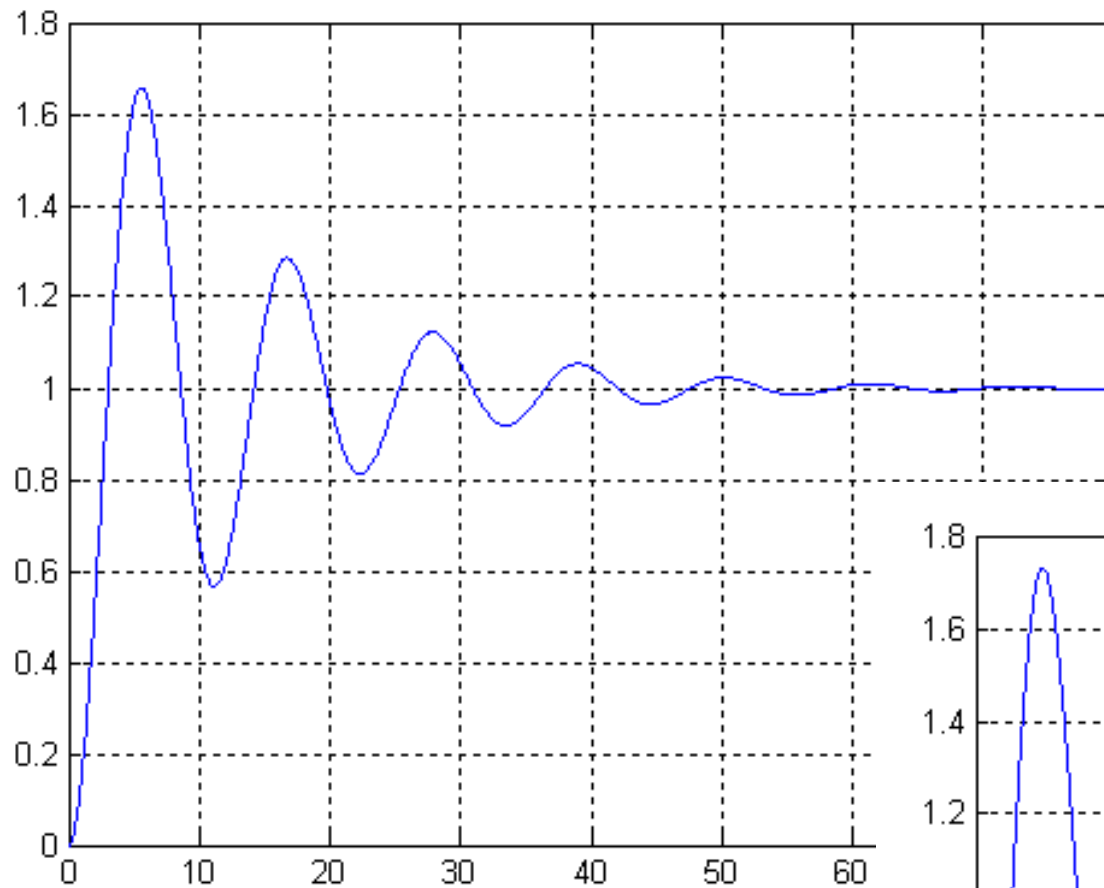
$$y(t) = K_o \left[1 - e^{-\zeta \omega_n t} \left(\cos \omega_d t + \frac{\zeta}{\sqrt{1 - \zeta^2}} \cdot \text{sen } \omega_d t \right) \right], \quad t > 0$$

pode ter muitas formas diferentes, dependendo dos valores de ζ (*coeficiente de amortecimento*), ω_n (*frequência natural*) e K_o (*ganho*)

Observe que ω_d depende de ζ e ω_n

$$\omega_d = \omega_n \cdot \sqrt{1 - \zeta^2} \quad \begin{array}{l} \text{frequência natural amortecida} \\ \text{(damping frequency)} \end{array}$$

Análise no domínio do tempo - Sistemas de 2ª ordem



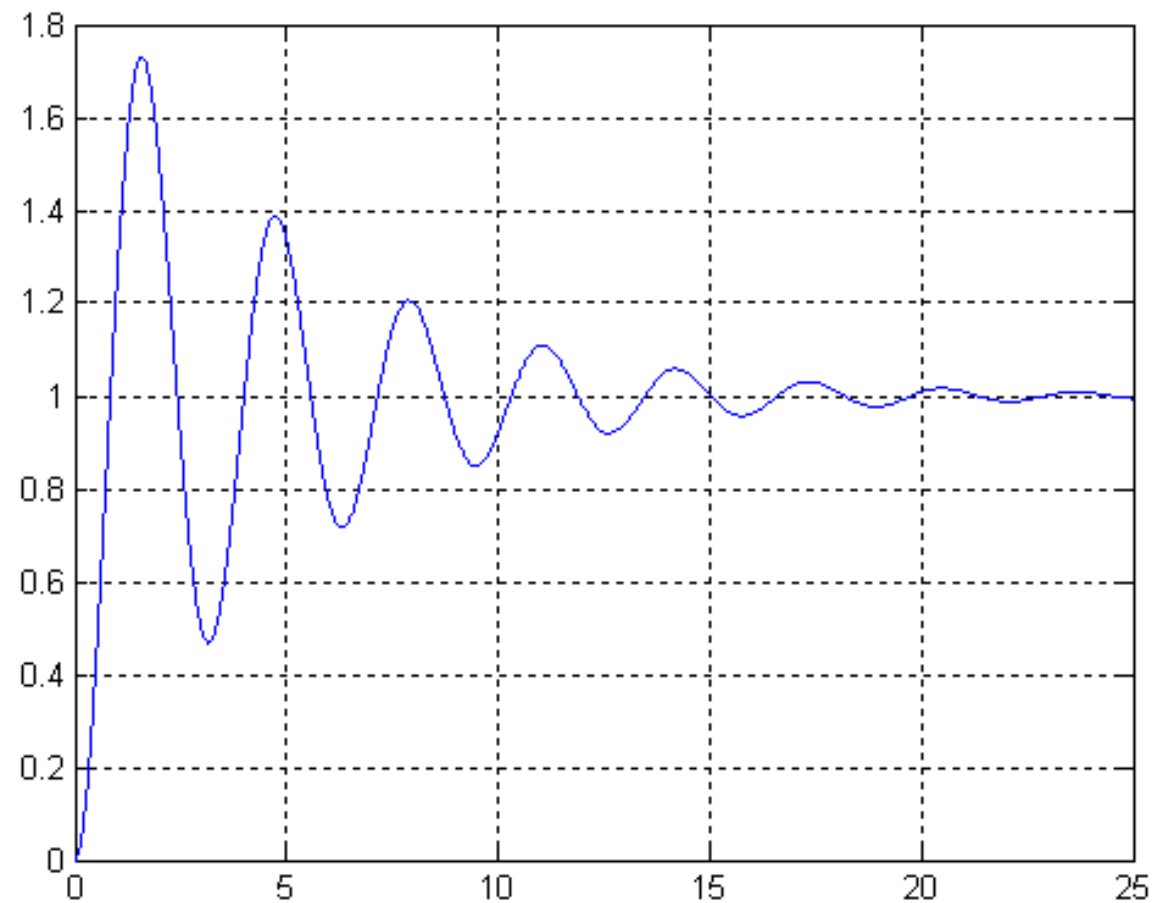
resposta ao
degrau unitário

$$\zeta = 0,132$$

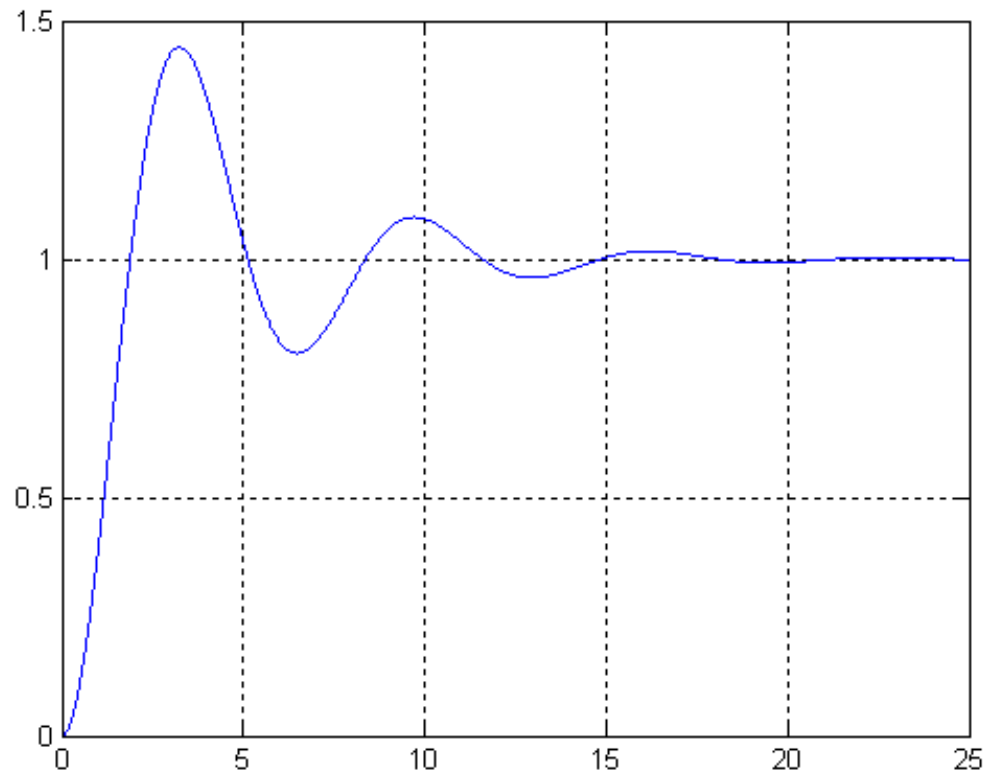
$$\omega_n = 0,57$$

$$\zeta = 0,1$$

$$\omega_n = 2$$



Análise no domínio do tempo - Sistemas de 2ª ordem



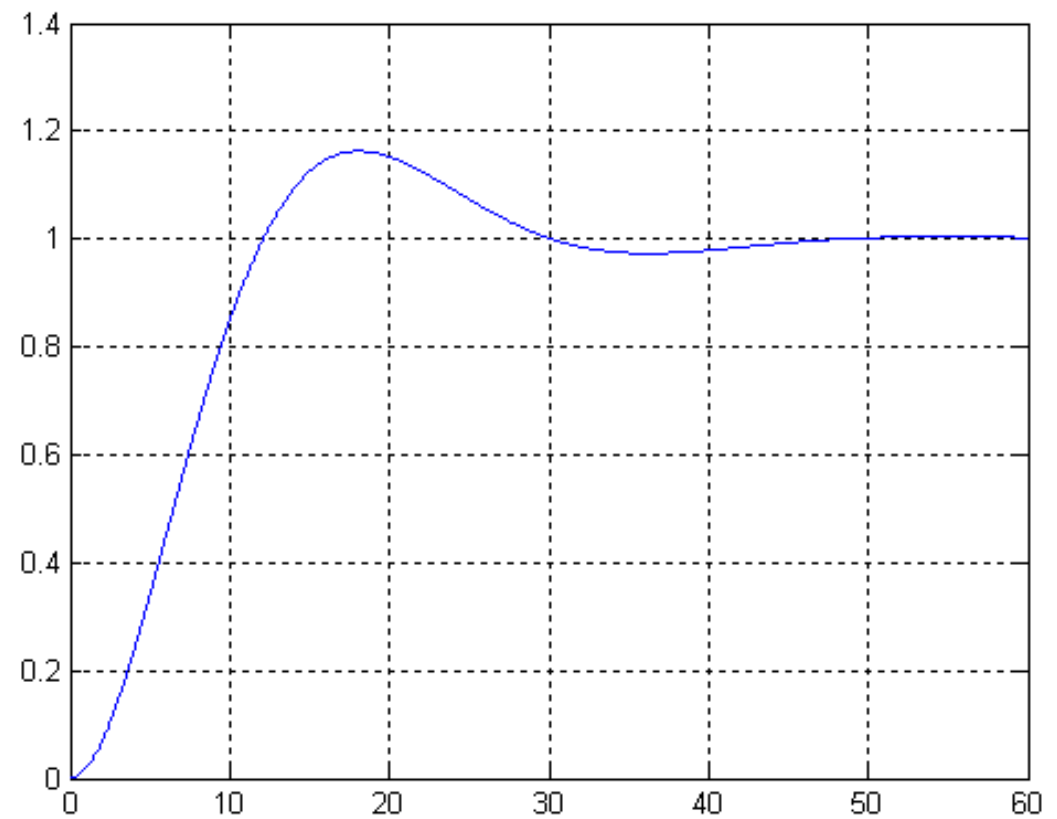
$$\zeta = 0,25$$

$$\omega_n = 1$$

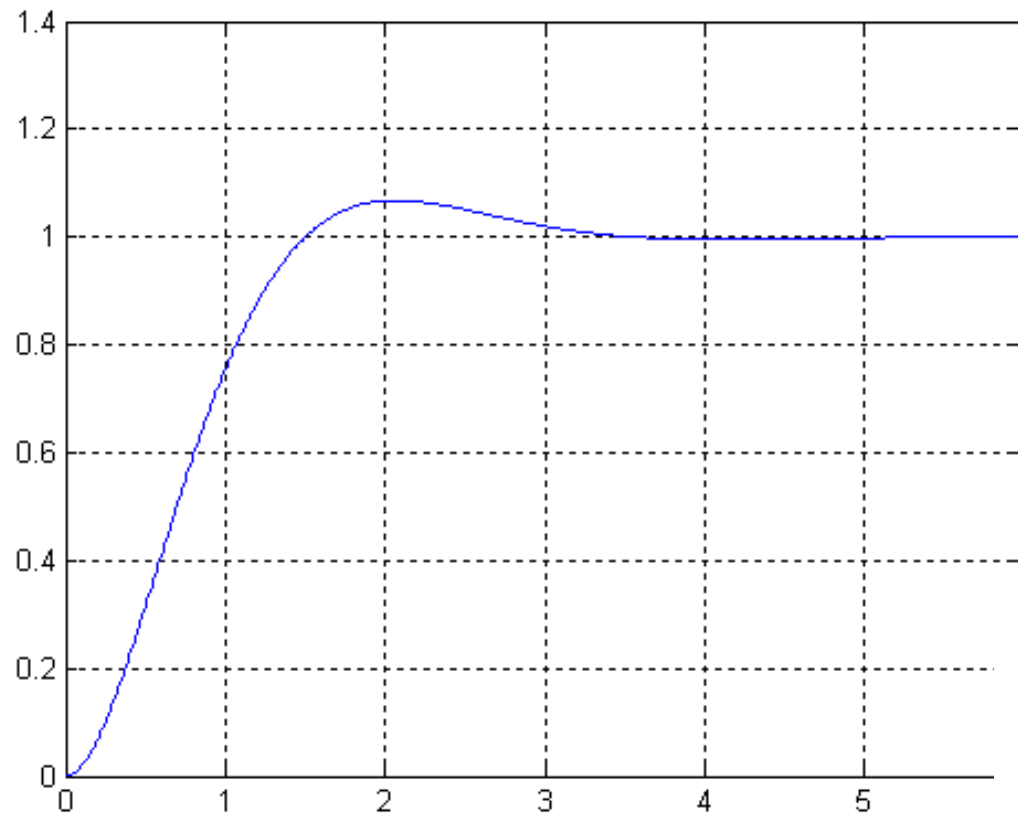
$$\zeta = 0,5$$

$$\omega_n = 0,2$$

resposta ao
degrau unitário



Análise no domínio do tempo - Sistemas de 2ª ordem



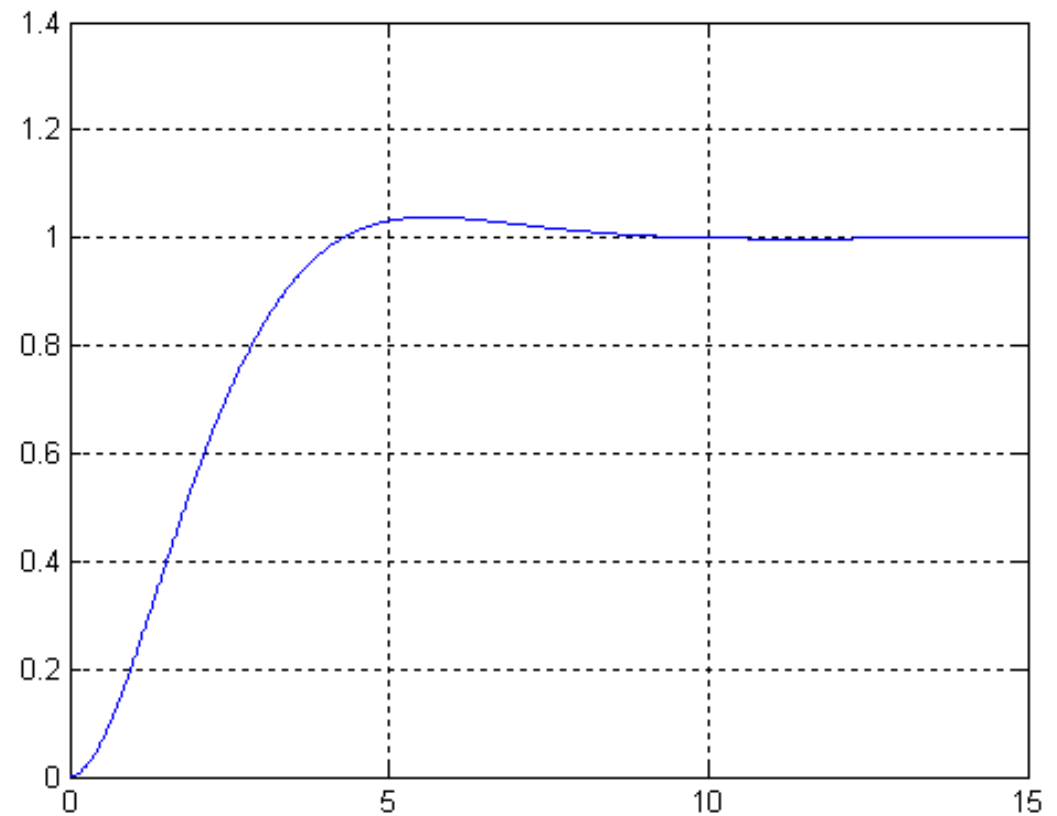
resposta ao
degrau unitário

$$\zeta = 0,65$$

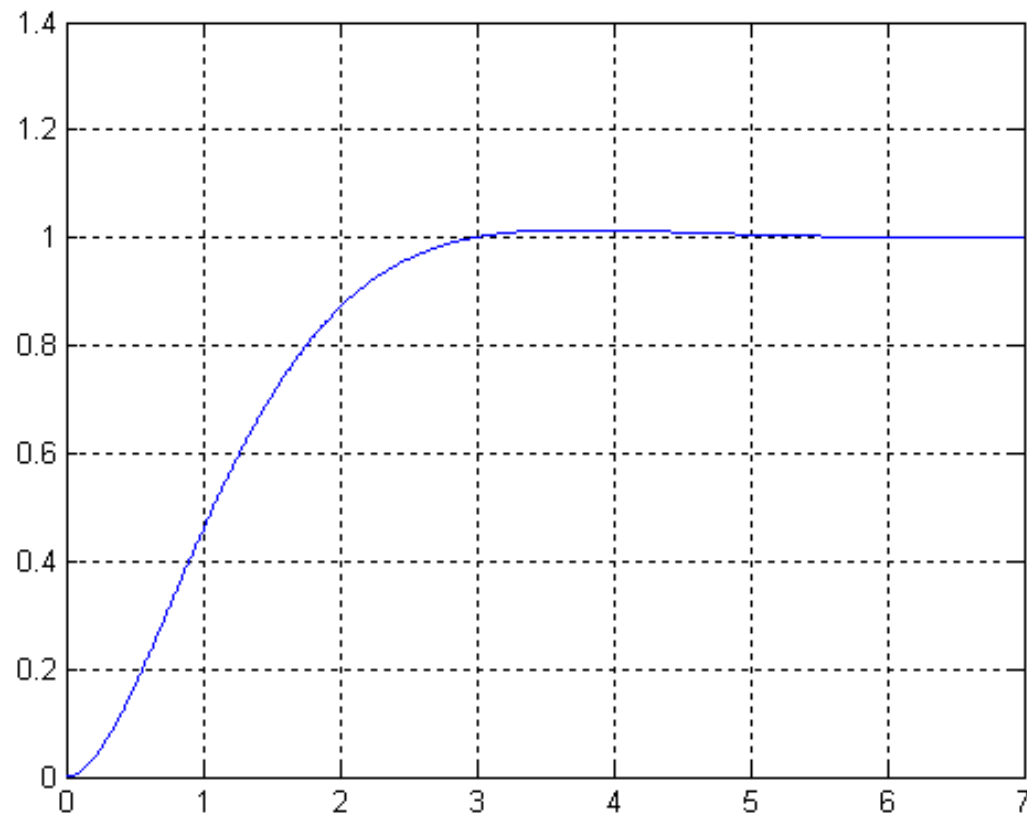
$$\omega_n = 2$$

$$\zeta = 0,72$$

$$\omega_n = 0,8$$



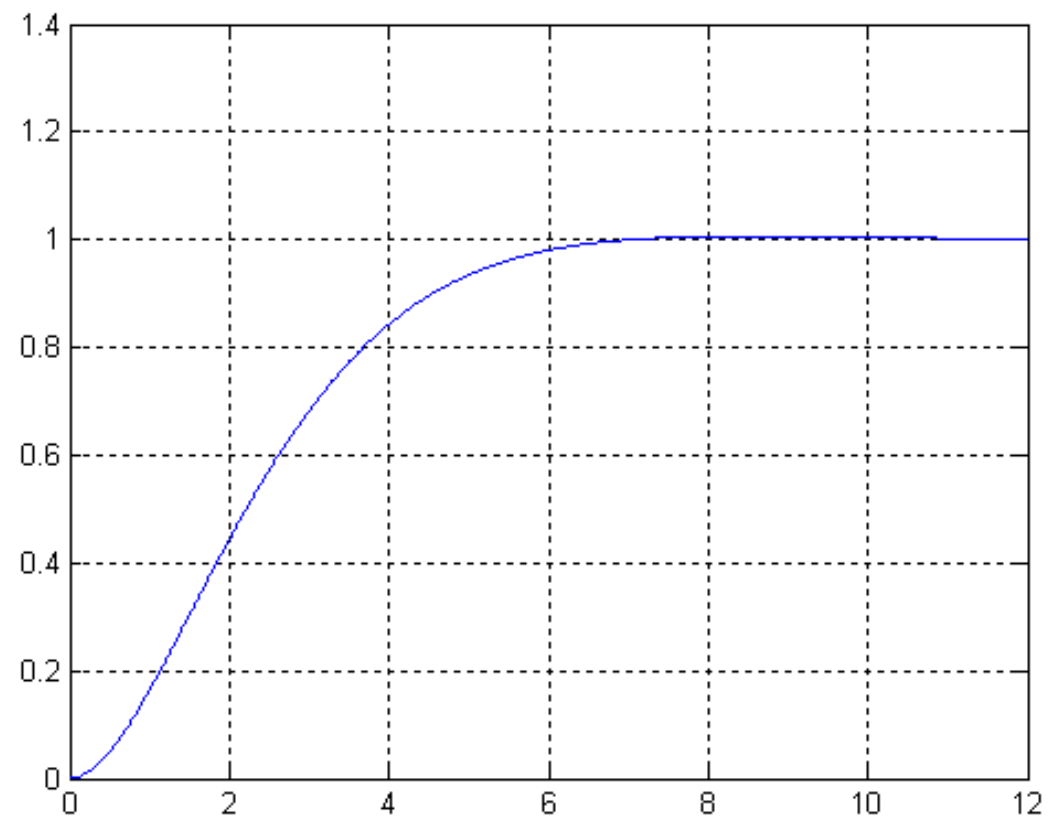
Análise no domínio do tempo - Sistemas de 2ª ordem



$$\zeta = 0,8$$
$$\omega_n = 1,4$$

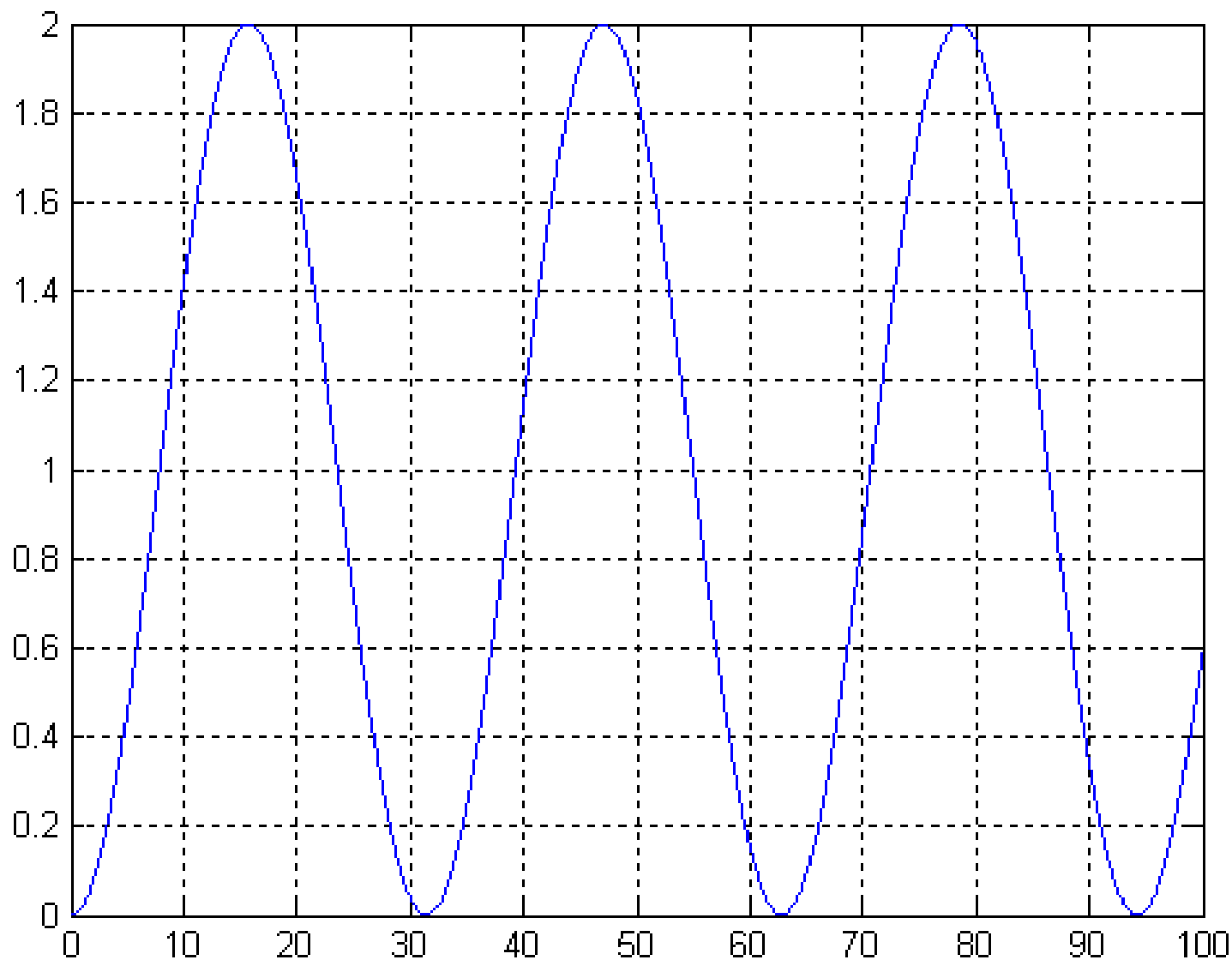
$$\zeta = 0,85$$
$$\omega_n = 0,7$$

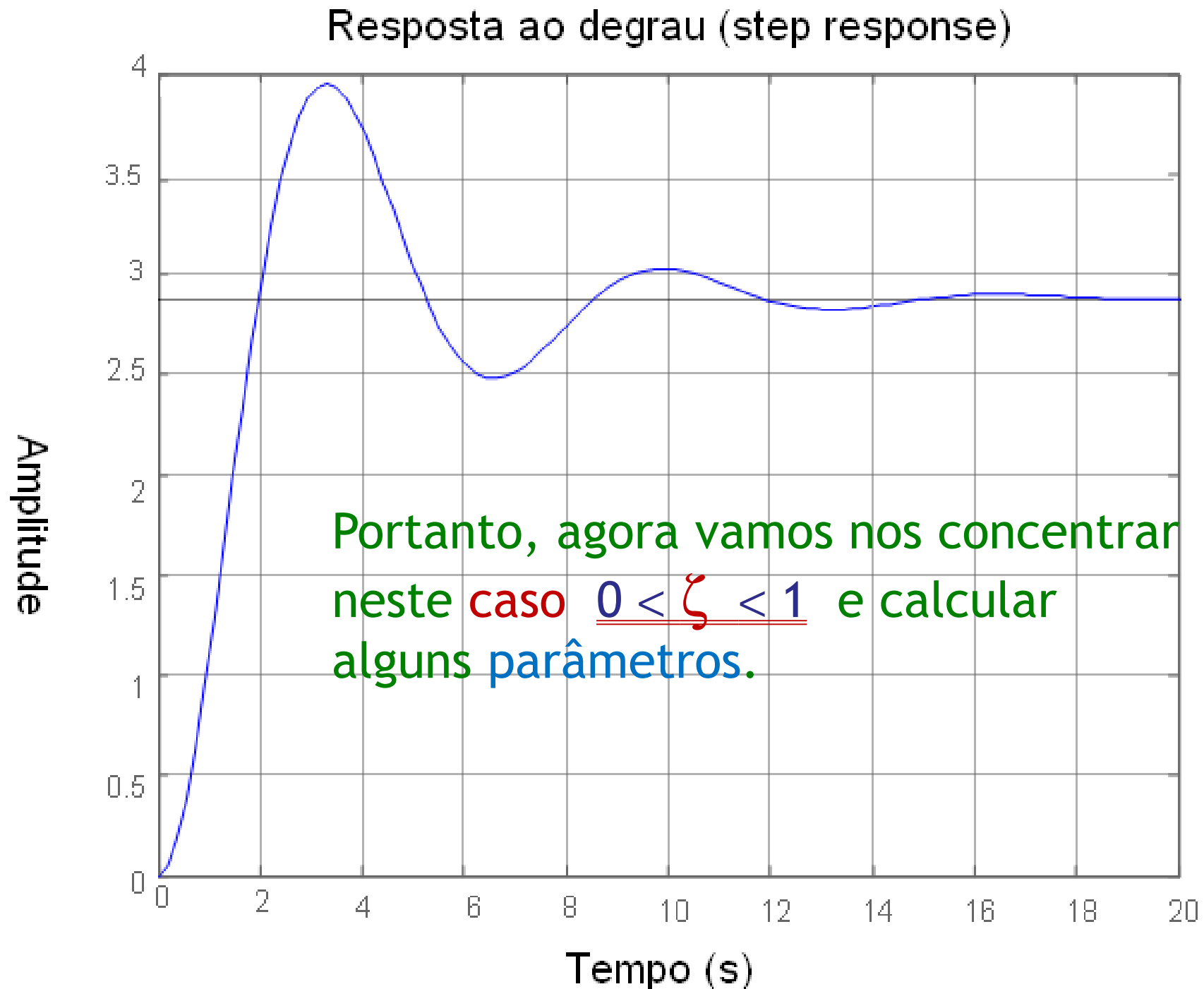
resposta ao
degrau unitário

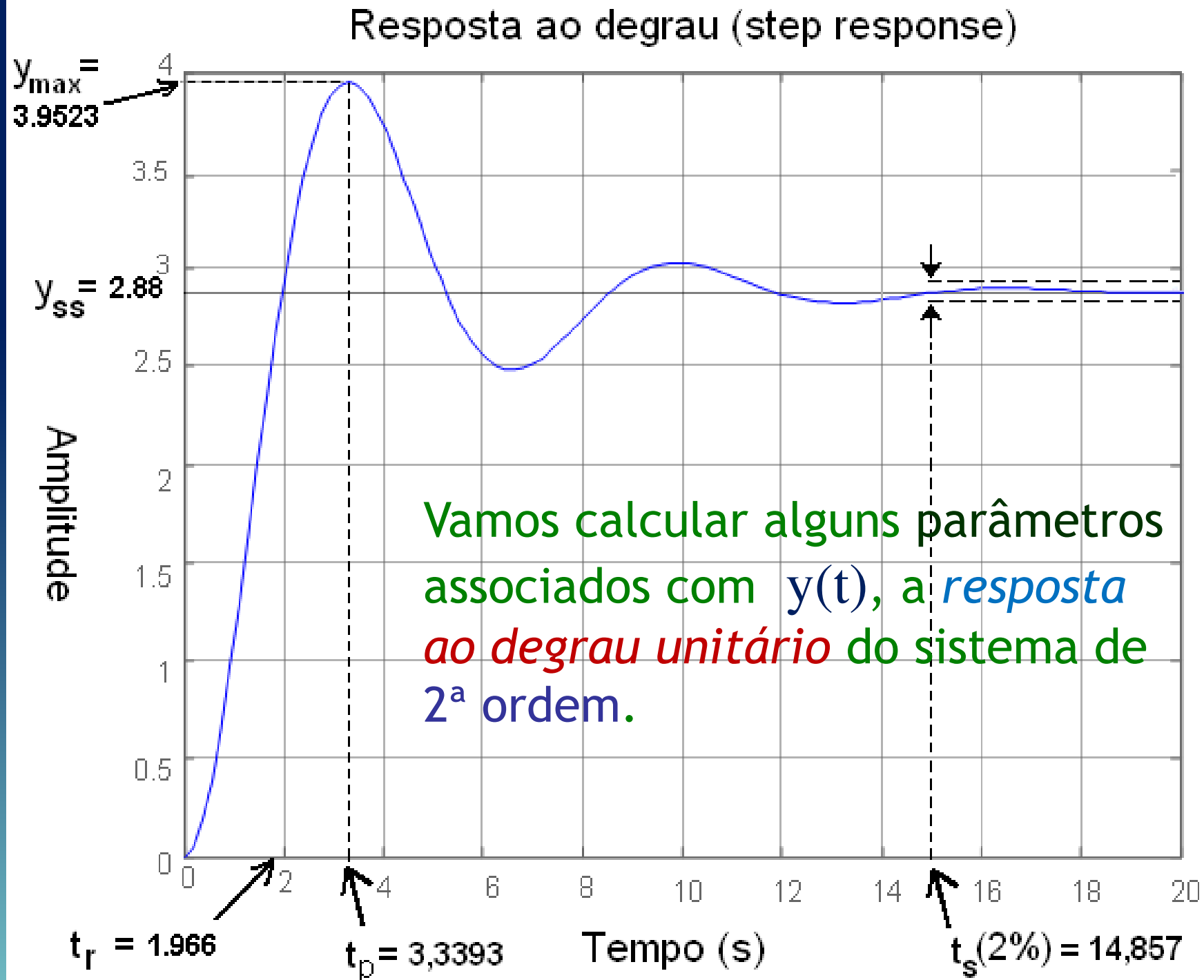


resposta ao
degrau unitário

$$\zeta = 0$$
$$\omega_n = 0,2$$







resposta em estado estacionário
(*steady state output*)

y_{ss}

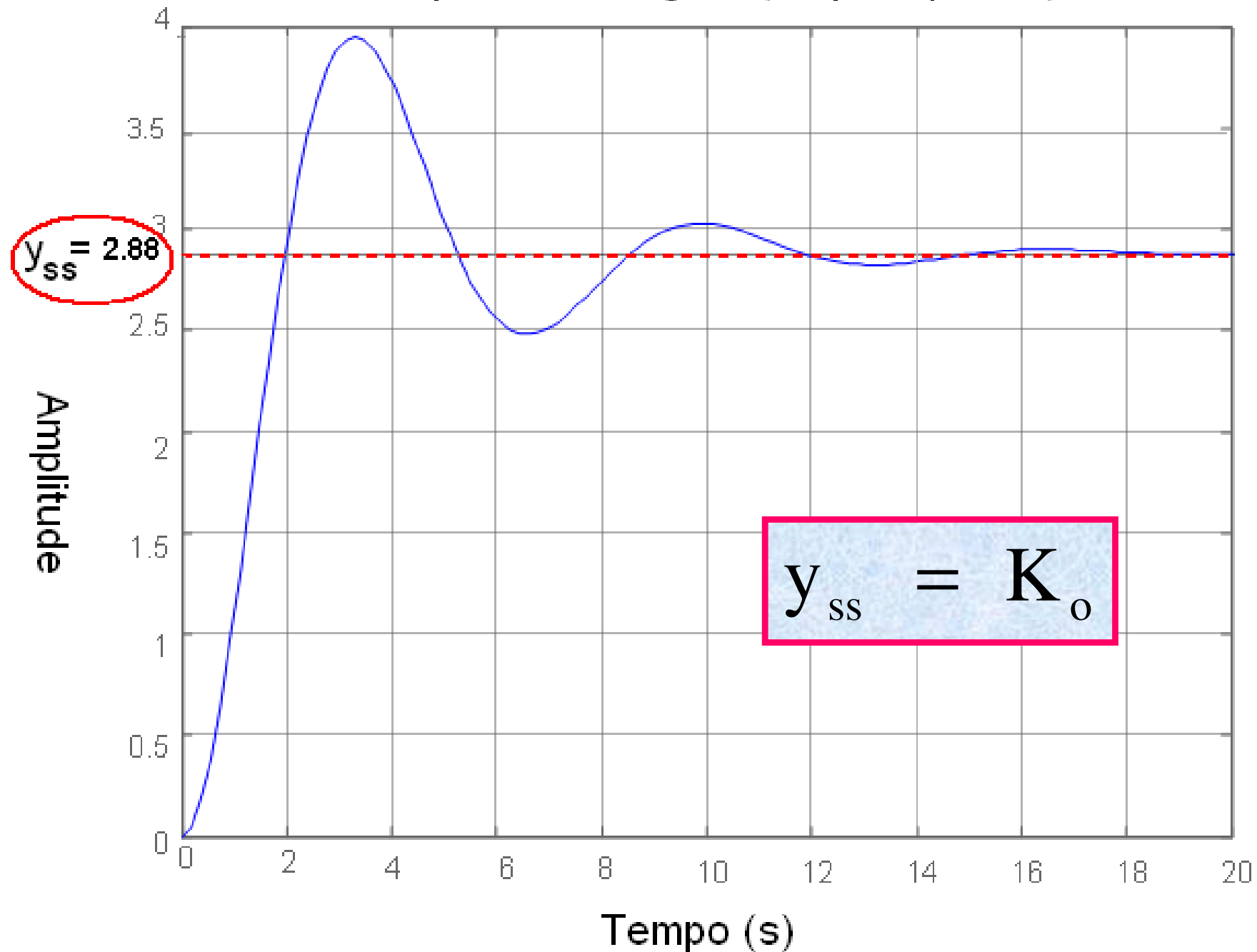
y_{ss} = resposta em estado estacionário ou
saída em regime permanente
(*steady state output*)

$$Y(s) = \frac{K_o \omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2} \cdot R(s) \quad \rightarrow \quad R(s) = \frac{1}{s}$$

$$\begin{aligned} y_{ss} &= \lim_{t \rightarrow \infty} y(t) = \lim_{s \rightarrow 0} s \cdot Y(s) = \\ &= \lim_{s \rightarrow 0} \frac{K_o \omega_n^2 s}{s^2 + 2\zeta\omega_n s + \omega_n^2} \cdot \frac{1}{s} = \\ &= K_o \end{aligned}$$

$$y_{ss} = K_o$$

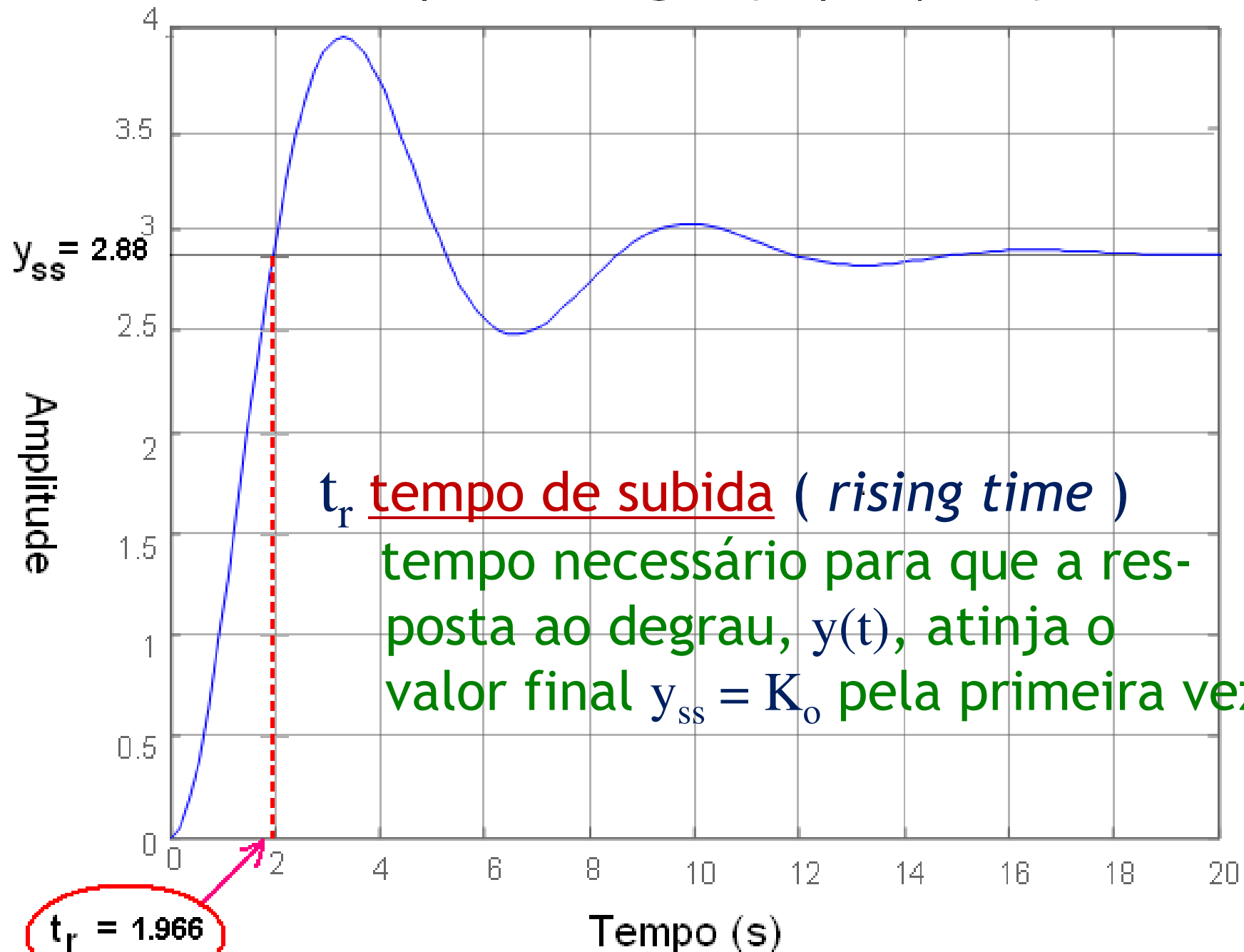
Resposta ao degrau (step response)



tempo de subida
(*rising time*)

t_r

Resposta ao degrau (step response)



t_r = tempo de subida (*rising time*)

é o instante em que $y(t)$ atinge o valor final K_o pela primeira vez.

$$y(t_r) = K_o \left[1 - e^{-\zeta \omega_n t_r} \left(\cos \omega_d t_r + \frac{\zeta}{\sqrt{1-\zeta^2}} \cdot \text{sen } \omega_d t_r \right) \right] = K_o$$

$$e^{-\zeta \omega_n t_r} \left(\cos \omega_d t_r + \frac{\zeta}{\sqrt{1-\zeta^2}} \cdot \text{sen } \omega_d t_r \right) = 0$$

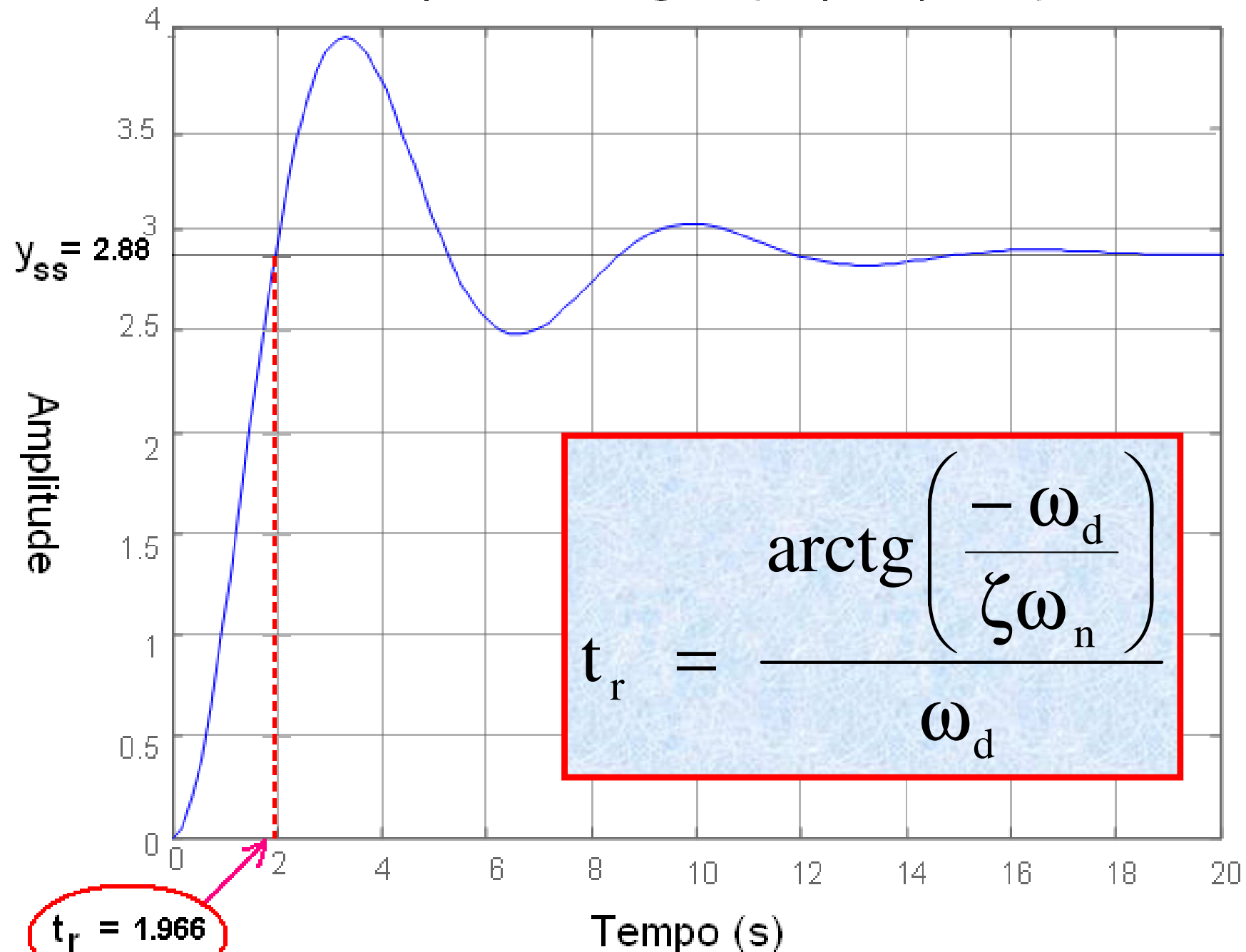
$$\text{tg}(\omega_d t_r) = \frac{-\sqrt{1-\zeta^2}}{\zeta} = \frac{-\omega_d}{\zeta \omega_n}$$

t_r = tempo de subida (*rising time*)
depende dos valores de ζ (*coeficiente de amortecimento*),
e de ω_n (*frequência natural*)

$$t_r = \frac{\arctg\left(\frac{-\omega_d}{\zeta\omega_n}\right)}{\omega_d} = \frac{\arctg\left(\frac{-\sqrt{1-\zeta^2}}{\zeta}\right)}{\omega_d}$$

$$t_r = \arctg(-\omega_d / \zeta\omega_n) / \omega_d$$

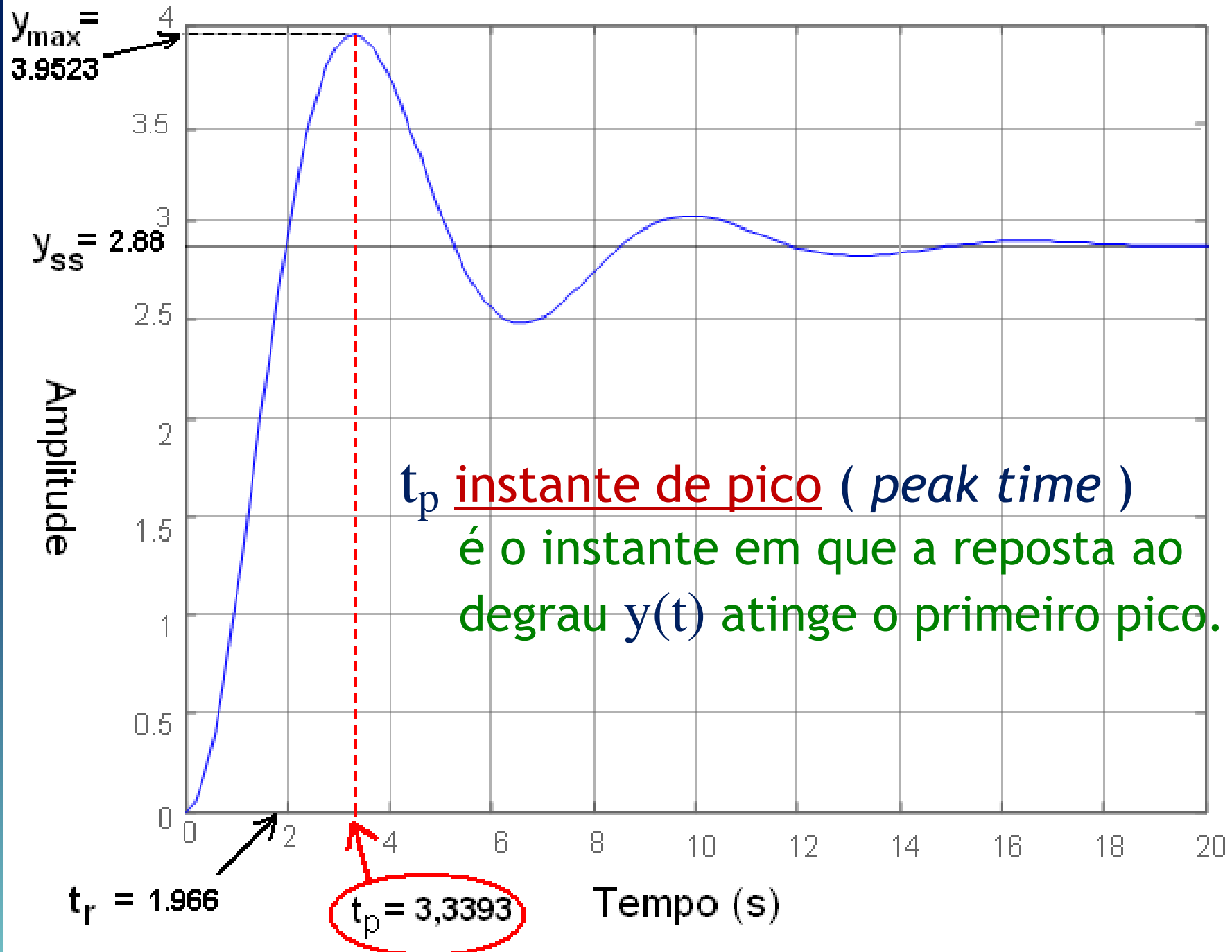
Resposta ao degrau (step response)



instante de pico
(*peak time*)

t_p

Resposta ao degrau (step response)

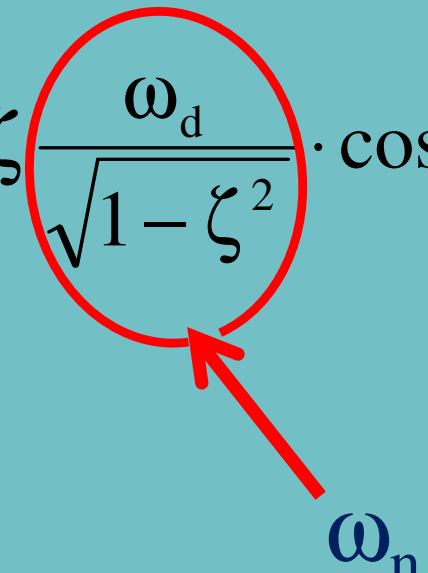


instante de pico
(*peak time*)

$$y_{ss} = K_o \text{ (ganho)}$$

ζ (*coeficiente de amortecimento*),

ω_n (*frequência natural*)

$$y' = \frac{dy}{dt} = K_o \left[\zeta \omega_n \cdot e^{-\zeta \omega_n t} \left(\cos \omega_d t_r + \frac{\zeta}{\sqrt{1 - \zeta^2}} \cdot \text{sen } \omega_d t_r \right) + \right. \\ \left. - e^{-\zeta \omega_n t} \left(-\omega_d \text{sen } \omega_d t_r + \zeta \frac{\omega_d}{\sqrt{1 - \zeta^2}} \cdot \cos \omega_d t_r \right) \right]$$


instante de pico
(*peak time*)

$$\begin{aligned}
 \frac{dy}{dt} &= K_o \cdot e^{-\zeta \omega_n t} \left(\cancel{\zeta \omega_n \cos \omega_d t} + \frac{\zeta^2 \omega_n}{\sqrt{1-\zeta^2}} \cdot \text{sen } \omega_d t + \right. \\
 &\quad \left. + \omega_d \text{sen } \omega_d t - \cancel{\zeta \omega_n \cdot \cos \omega_d t} \right) \\
 &= K_o \cdot e^{-\zeta \omega_n t} \cdot \text{sen } \omega_d t \cdot \left(\frac{\zeta^2 \omega_n}{\sqrt{1-\zeta^2}} + \frac{\omega_n (1-\zeta^2)}{\sqrt{1-\zeta^2}} \right) \\
 &= \cancel{K_o} \cdot \cancel{e^{-\zeta \omega_n t}} \cdot \text{sen } \omega_d t \cdot \frac{\cancel{\omega_n}}{\cancel{\sqrt{1-\zeta^2}}} = 0
 \end{aligned}$$

instante de pico
(*peak time*)

$$\frac{dy}{dt} = 0$$



$$\sin \omega_d t = 0$$



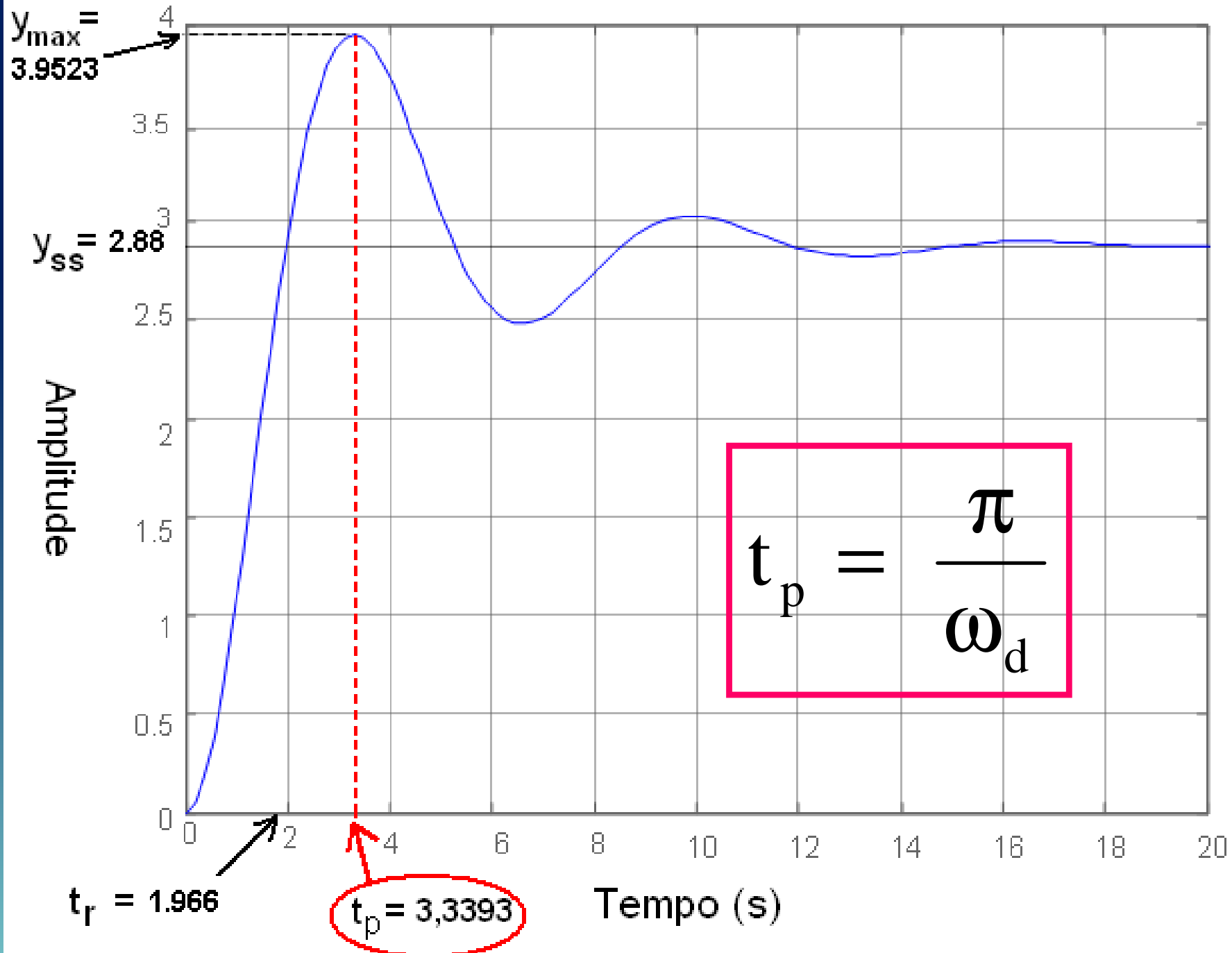
$$\omega_d t = 0, \pi, 2\pi, 3\pi, \dots$$



$$t_p = \frac{\pi}{\omega_d}$$

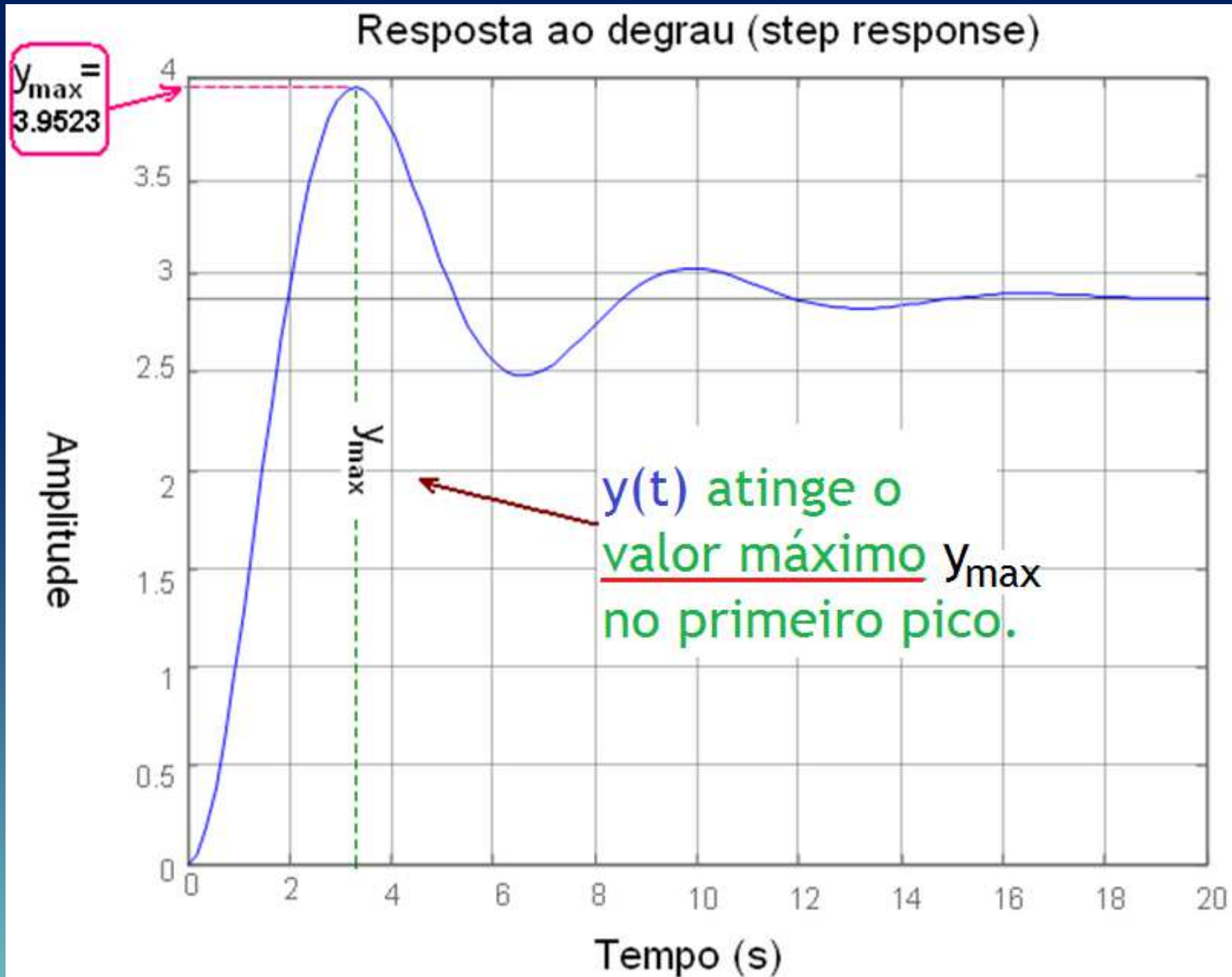
$$t_p = \pi / \omega_d$$

Resposta ao degrau (step response)

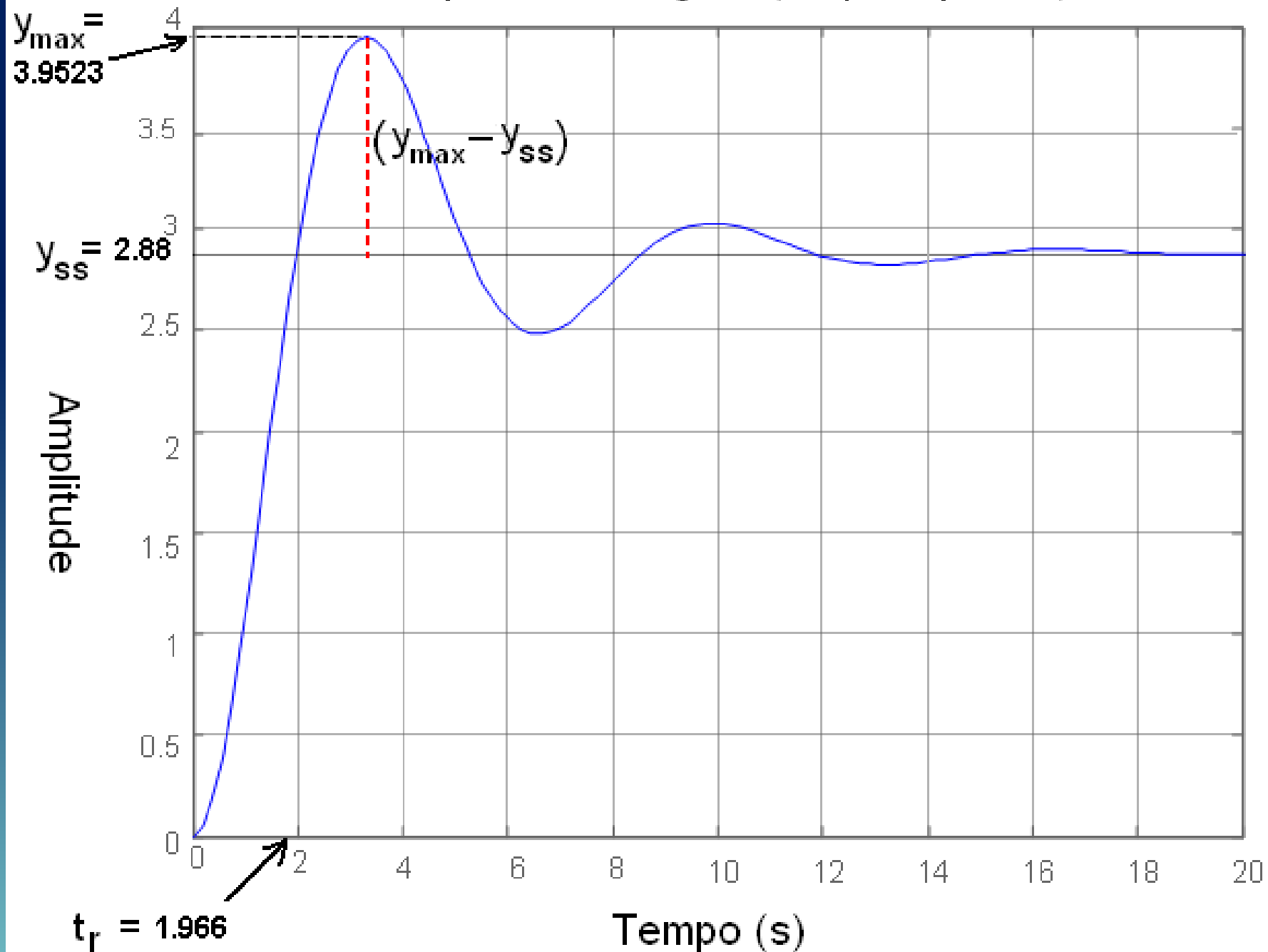


overshoot
(*sobressinal máximo*)

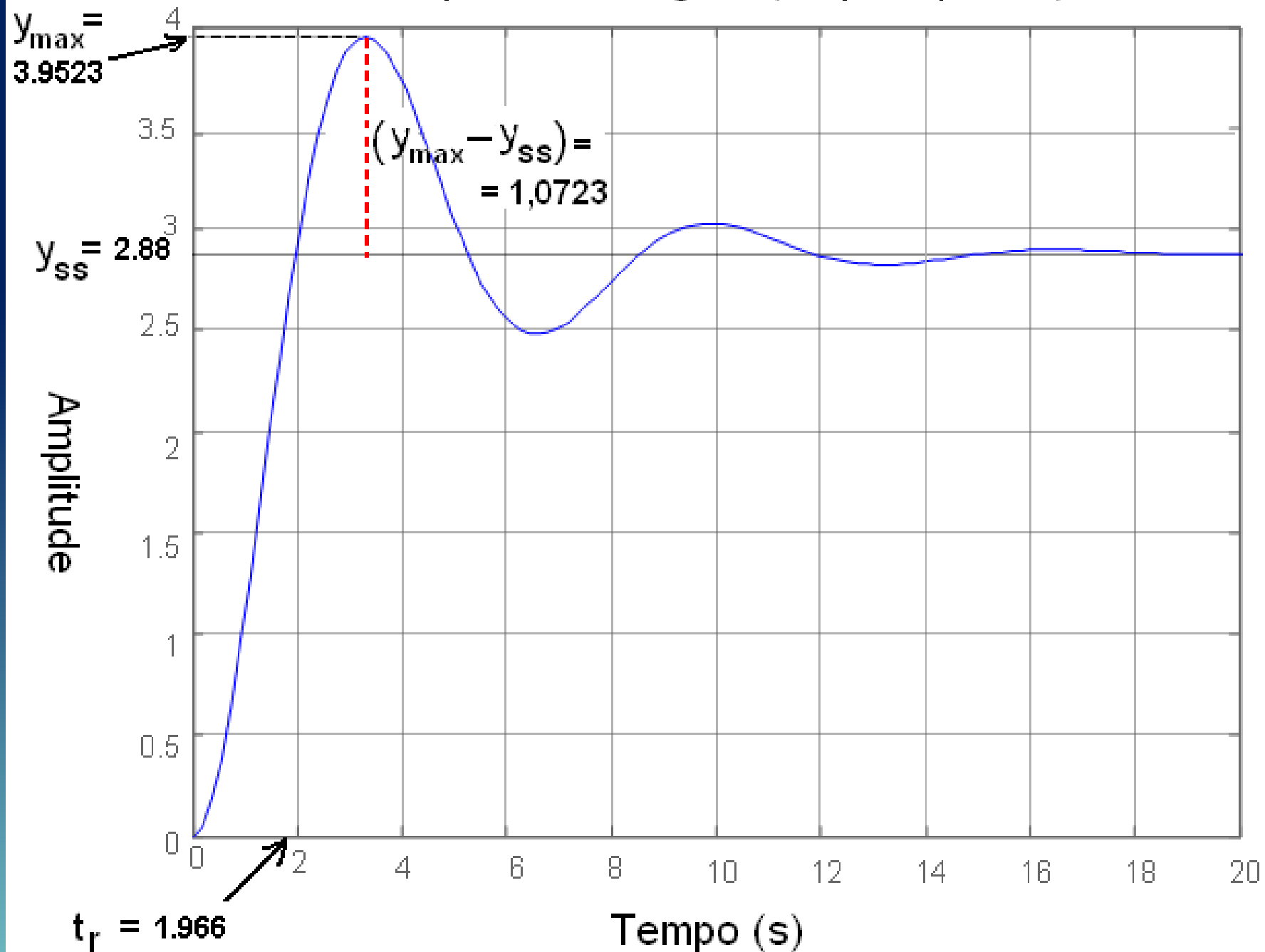
M_p



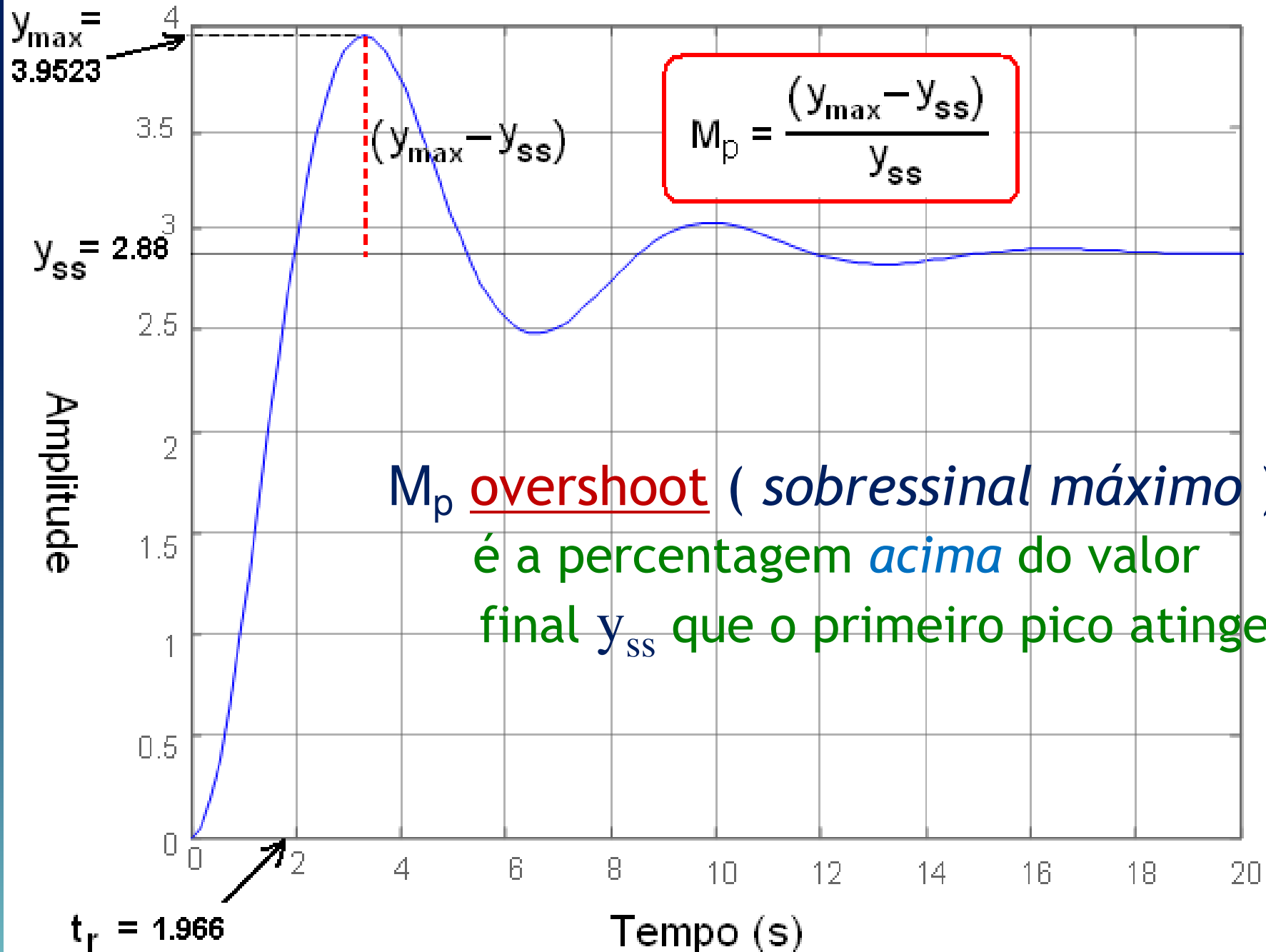
Resposta ao degrau (step response)

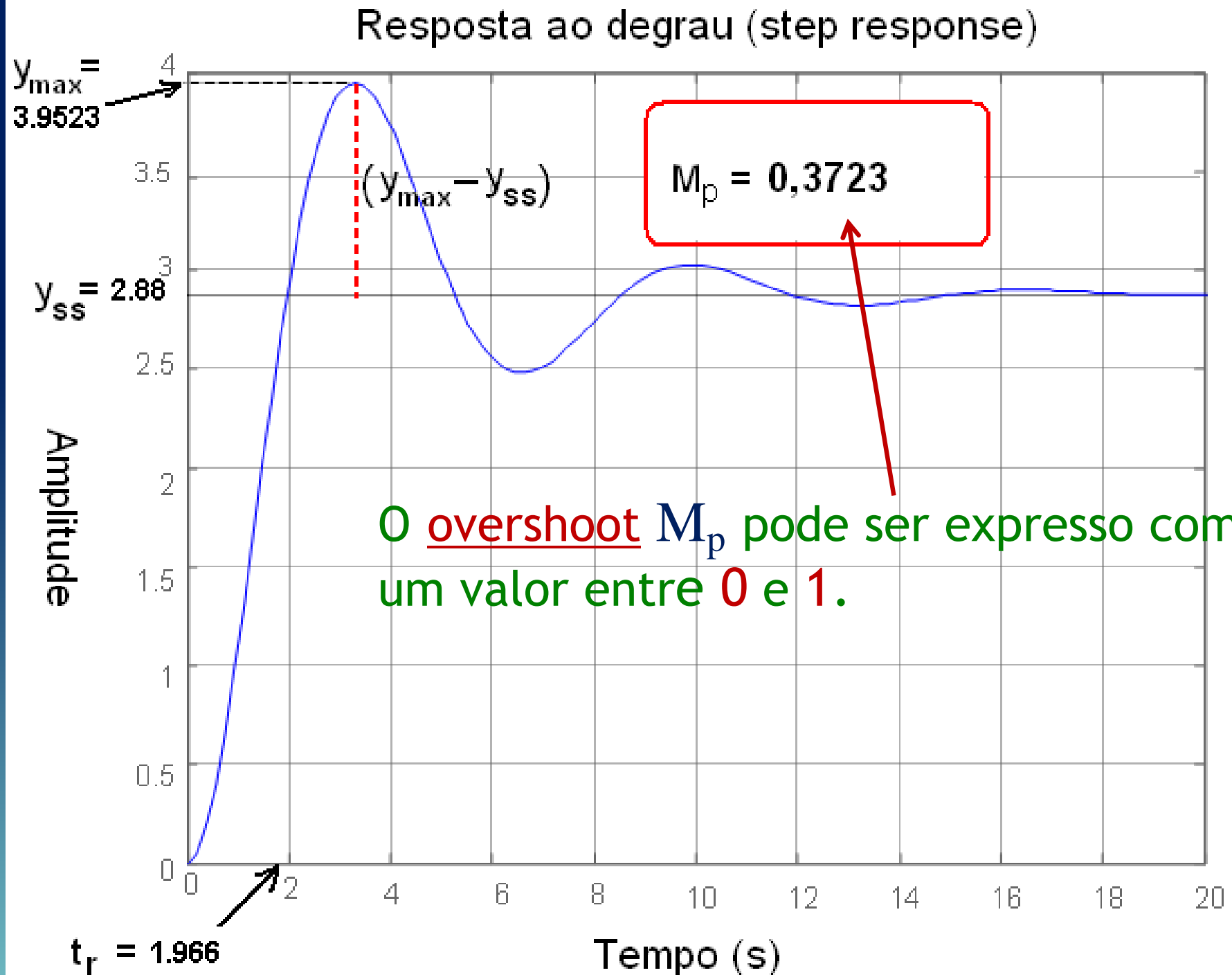


Resposta ao degrau (step response)

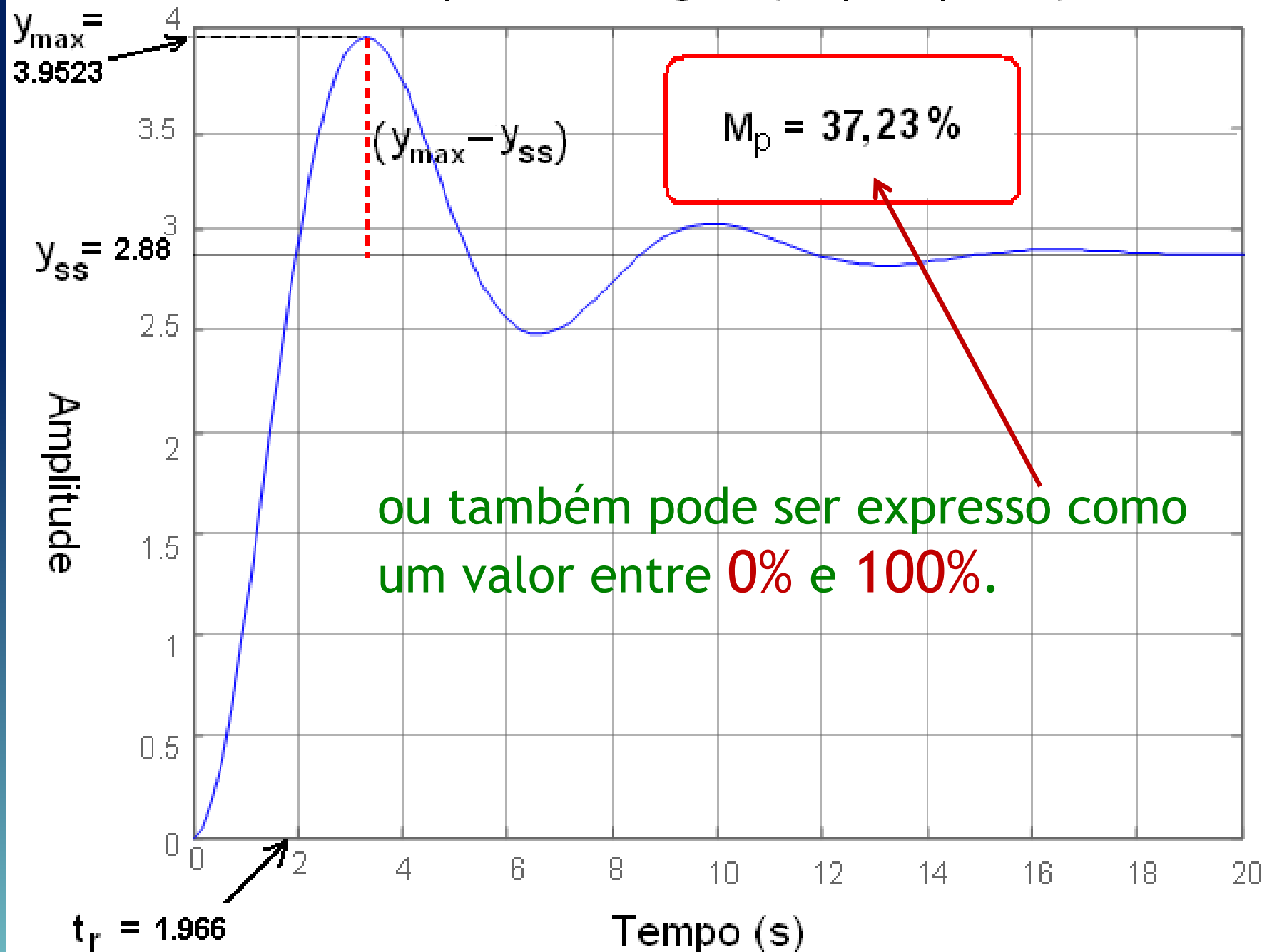


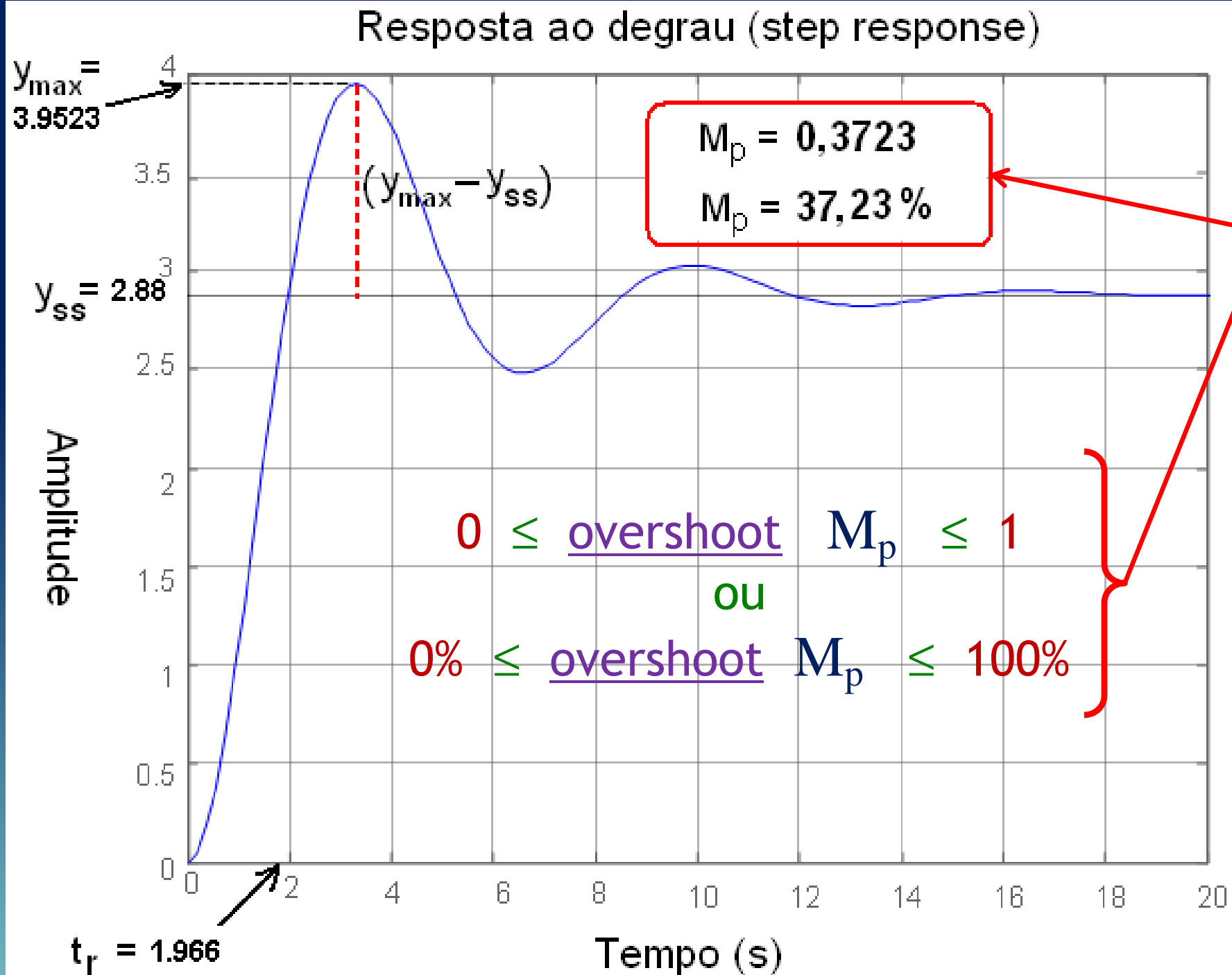
Resposta ao degrau (step response)





Resposta ao degrau (step response)





overshoot
(sobressinal máximo)

$$y_{ss} = K_o \text{ (ganho)}$$

ζ (coeficiente de amortecimento),

ω_n (frequência natural)

$$M_p = \frac{y_{\max} - y_{ss}}{y_{ss}} \quad \text{ou} \quad M_p = \frac{y(t_p) - K_o}{K_o}$$

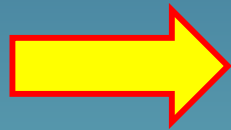
$$M_p = \frac{K_o \left[1 - e^{-\zeta \omega_n t_p} \left(\overbrace{\cos(\pi)}^{-1} - \frac{\zeta}{\sqrt{1-\zeta^2}} \overbrace{\sin(\pi)}^0 \right) \right] - K_o}{K_o}$$

$$M_p = \frac{\cancel{K_o} + K_o e^{-\zeta \omega_n (\pi / \omega_d)} - \cancel{K_o}}{K_o}$$

overshoot

(*sobressinal máximo*)

$$M_p = \frac{K_o e^{\frac{-\zeta \pi}{\sqrt{1-\zeta^2}}}}{K_o}$$



$$M_p = e^{\frac{-\zeta \pi}{\sqrt{1-\zeta^2}}}$$

M_p depende apenas de ζ (*coeficiente de amortecimento*)

overshoot

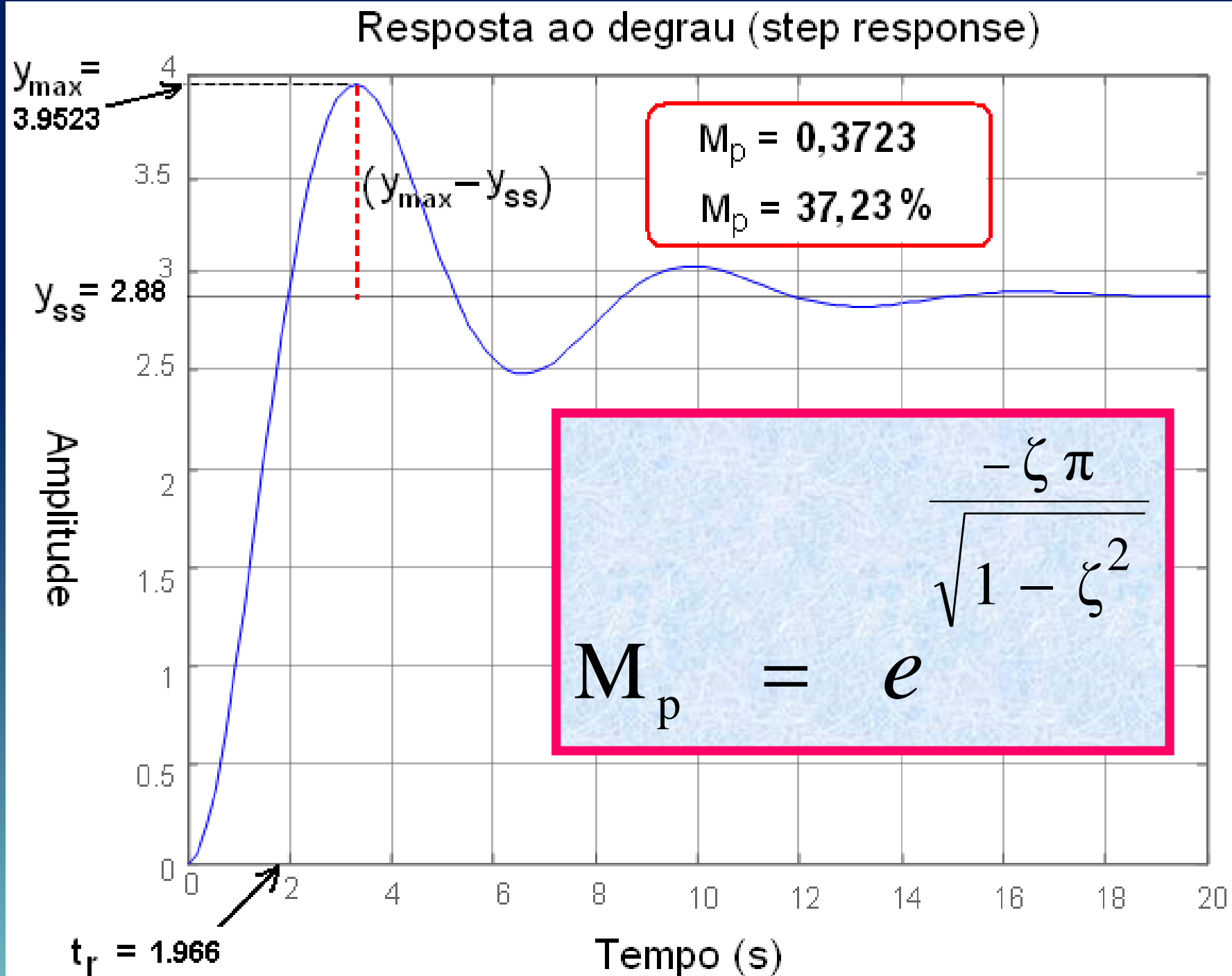
(*sobressinal máximo*)

M_p depende apenas de ζ (*coeficiente de amortecimento*)

$$M_p = e^{\frac{-\zeta \pi}{\sqrt{1 - \zeta^2}}}$$

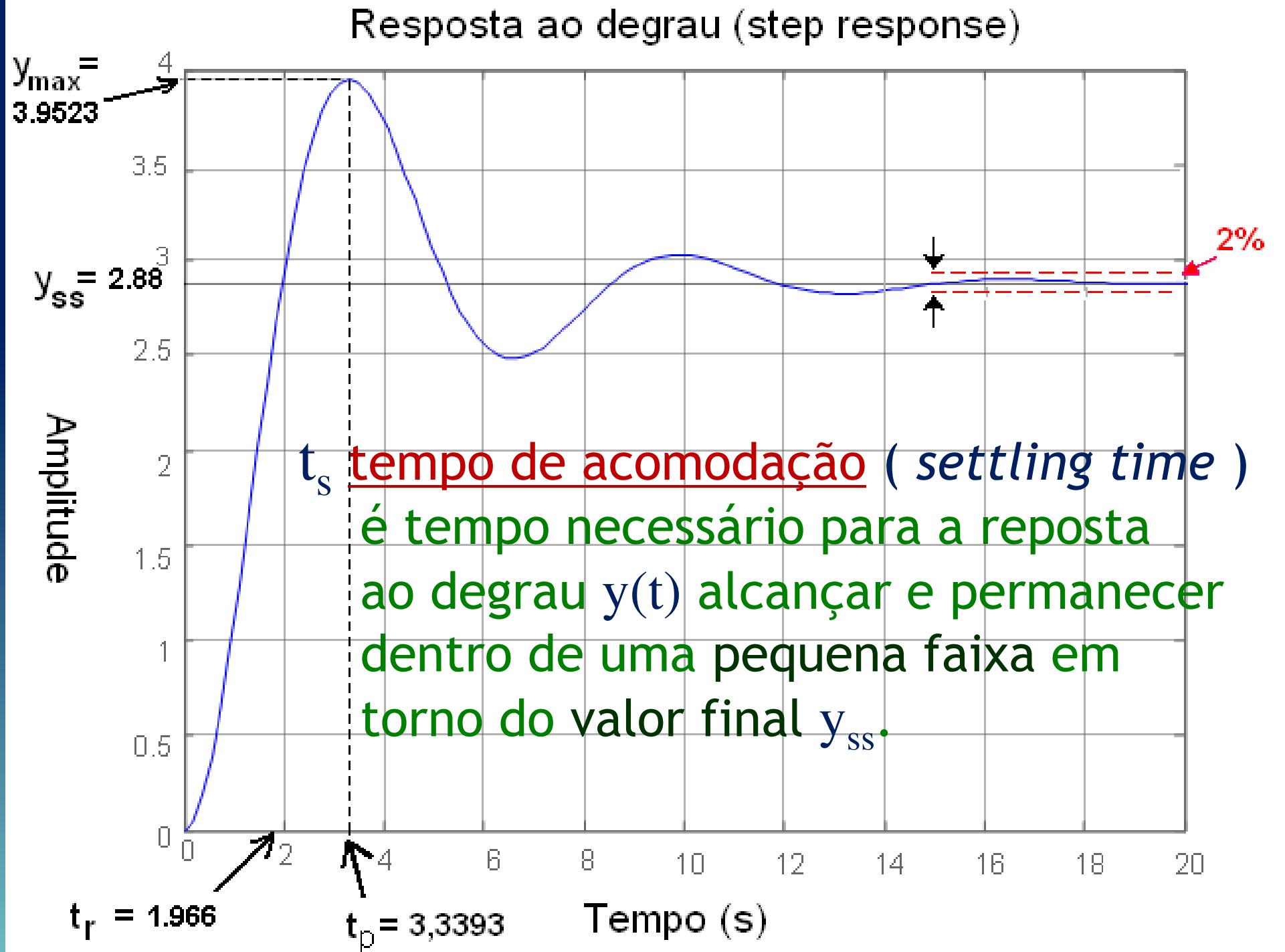
ou

$$M_p = e^{\frac{-\zeta \pi}{\sqrt{1 - \zeta^2}}} \times 100\%$$

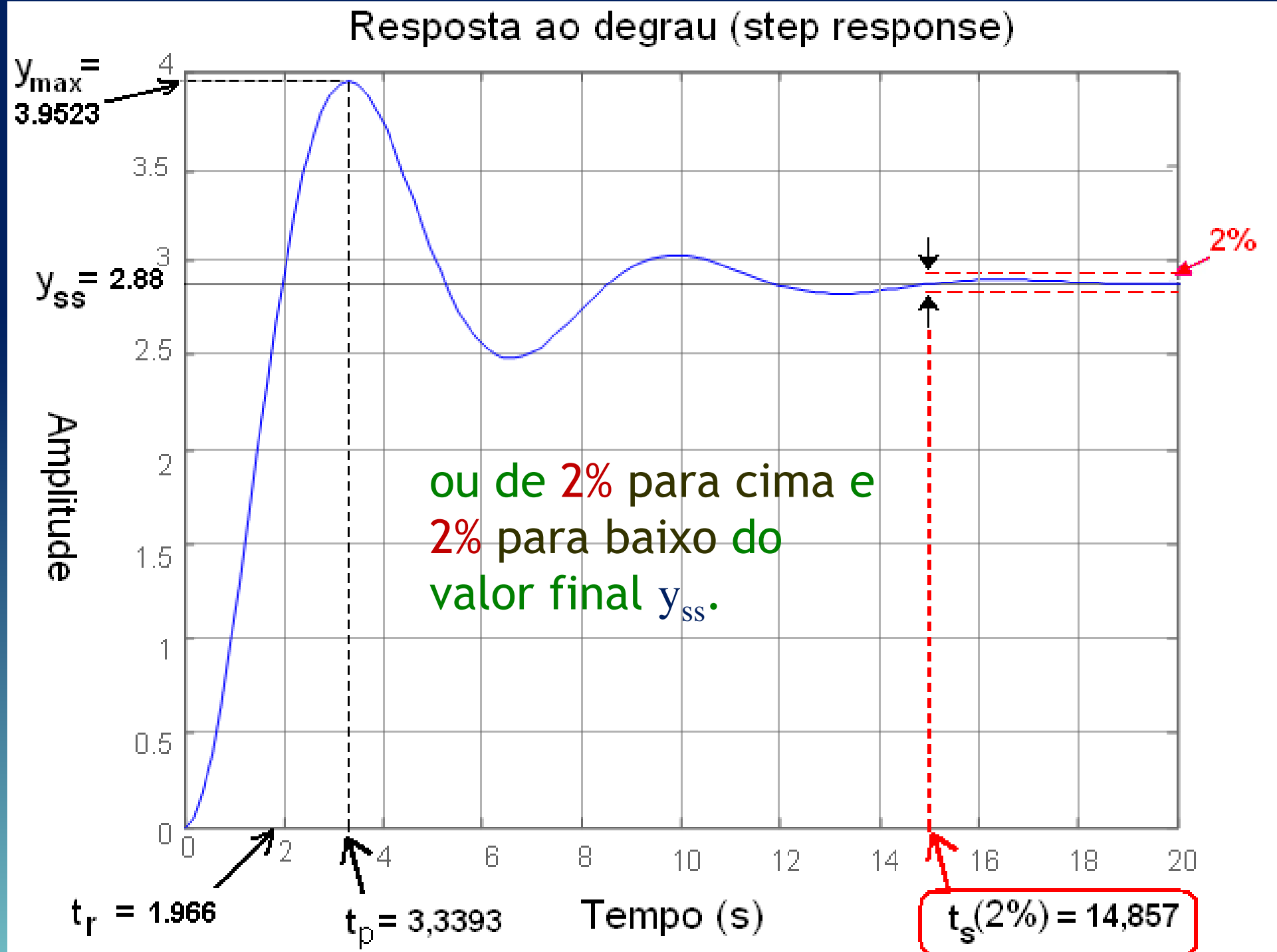


tempo de acomodação
(*settling time*)

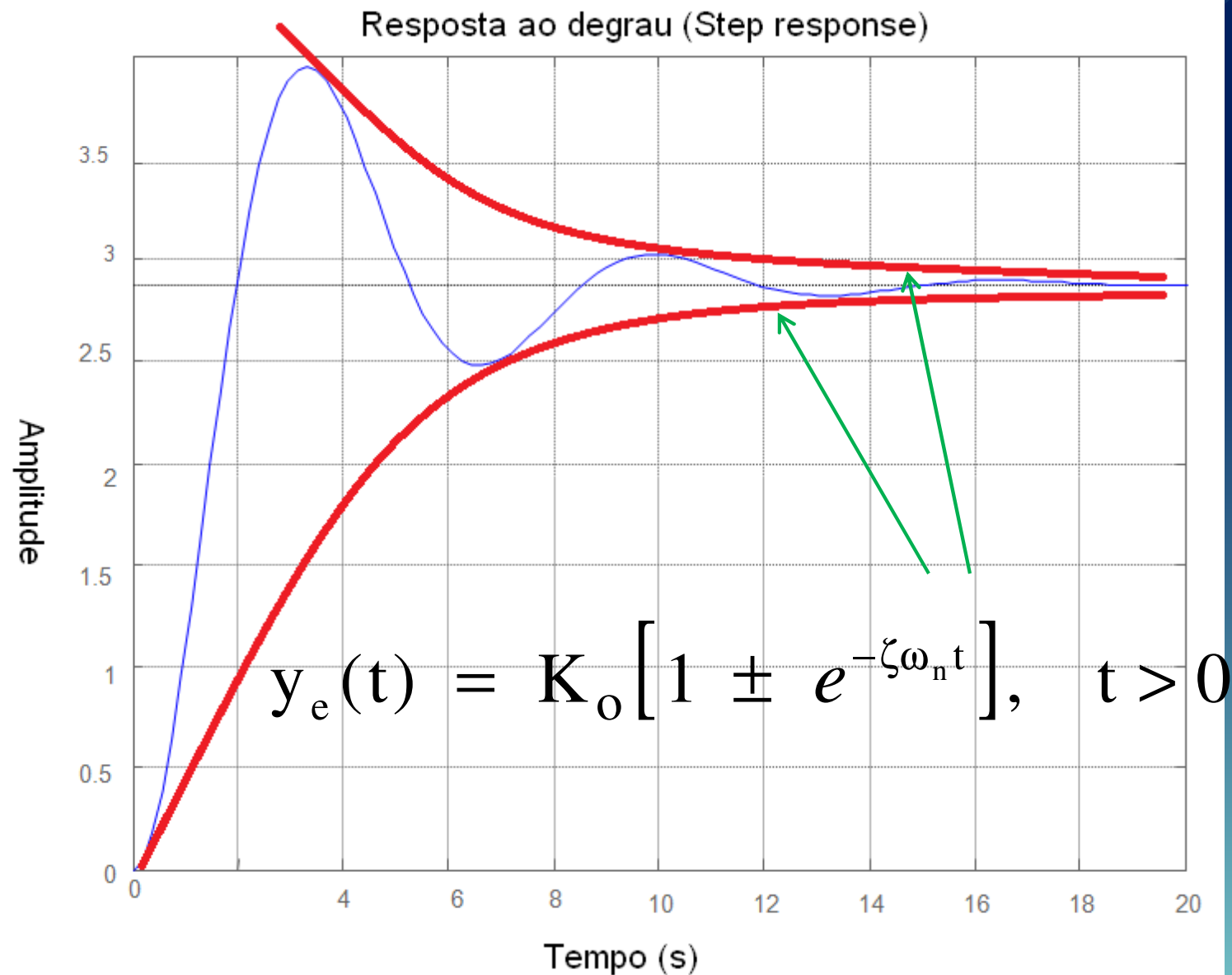
t_s







O tempo de acomodação (*settling time*) é obtido a partir das equações de $y_e(t)$, as curvas envoltórias de $y(t)$.



O tempo de acomodação (*settling time*) t_s é obtido fazendo

$$y_e(t_s) \approx 1,05 K_o$$

para o caso de t_s com 5% de tolerância, e

$$y_e(t_s) \approx 1,02 K_o$$

para o caso de t_s com 2% de tolerância.

Os valores que se obtém são:

$$t_s(5\%) = \frac{3}{\zeta\omega_n}$$

$$t_s(2\%) = \frac{4}{\zeta\omega_n}$$

tempo de acomodação (*settling time*)

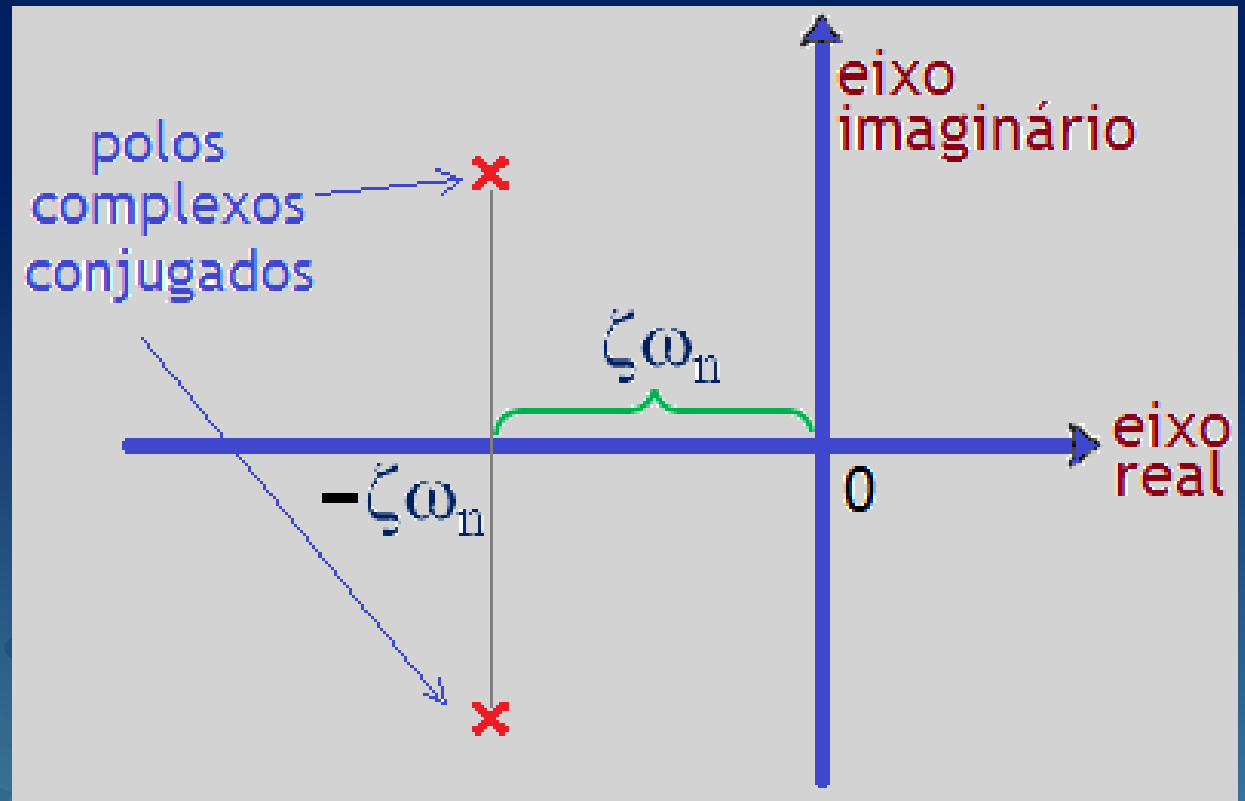
Note que o tempo de acomodação t_r é inversamente proporcional a $\zeta\omega_n$, que é a distância da parte real dos polos à origem.

portanto:

$$t_s(5\%) = \frac{3}{\zeta\omega_n}$$

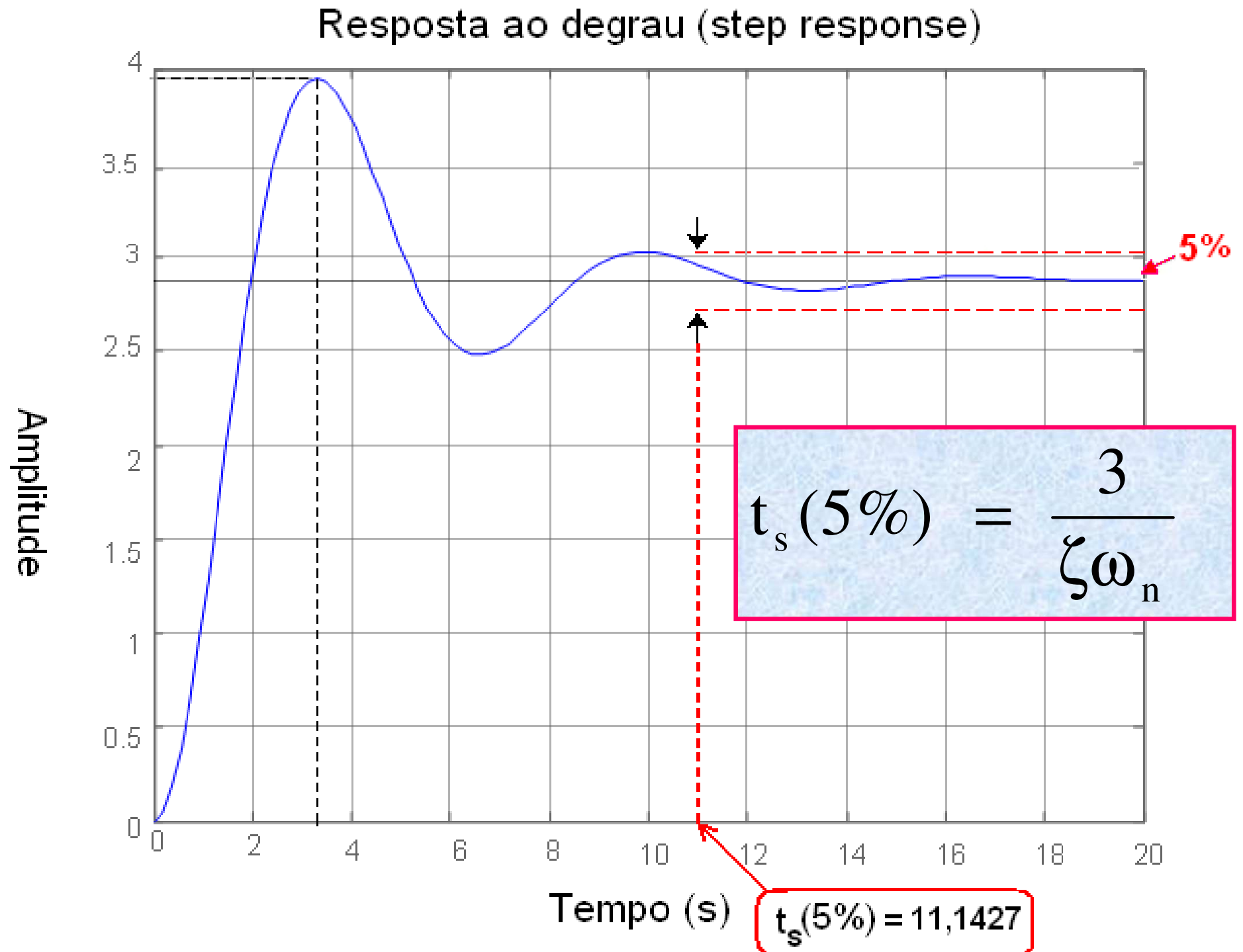
e

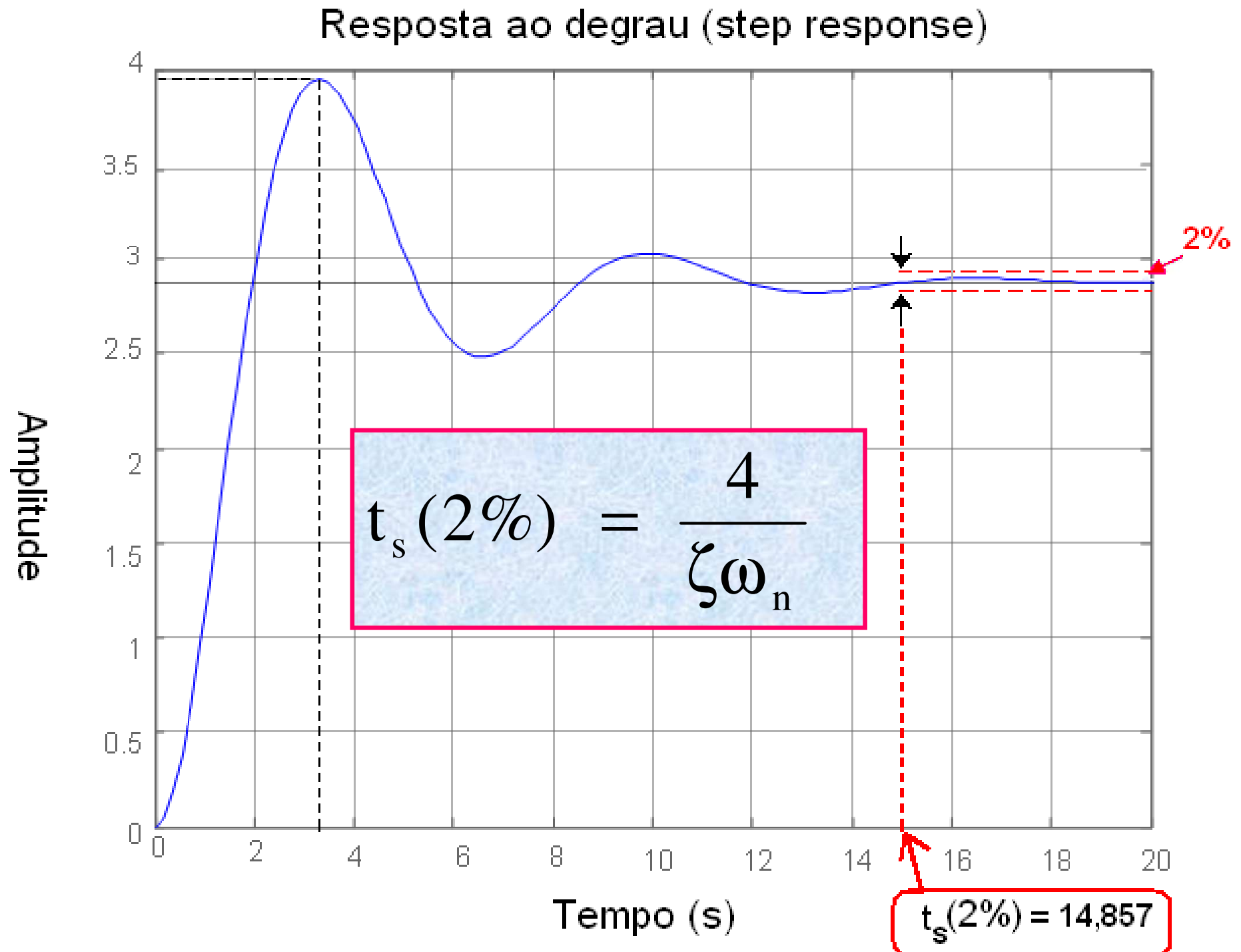
$$t_s(2\%) = \frac{4}{\zeta\omega_n}$$



$$t_s(5\%) = 3 / \zeta\omega_n$$

$$t_s(2\%) = 4 / \zeta\omega_n$$





Observe que vimos aqui 3 casos

$$0 < \zeta < 1$$

$$\zeta = 1$$

$$\zeta > 1$$

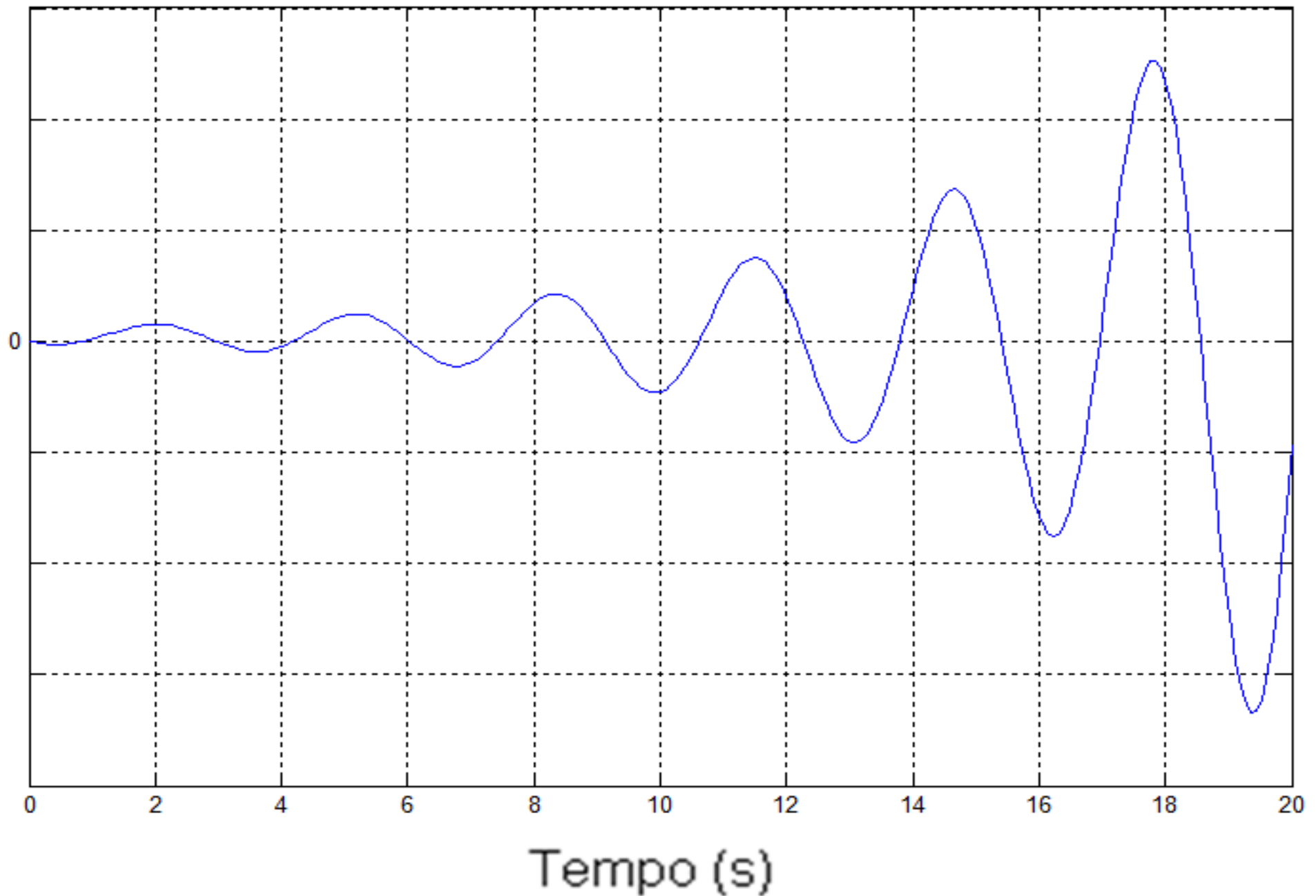
ou seja:

$$\zeta > 0$$

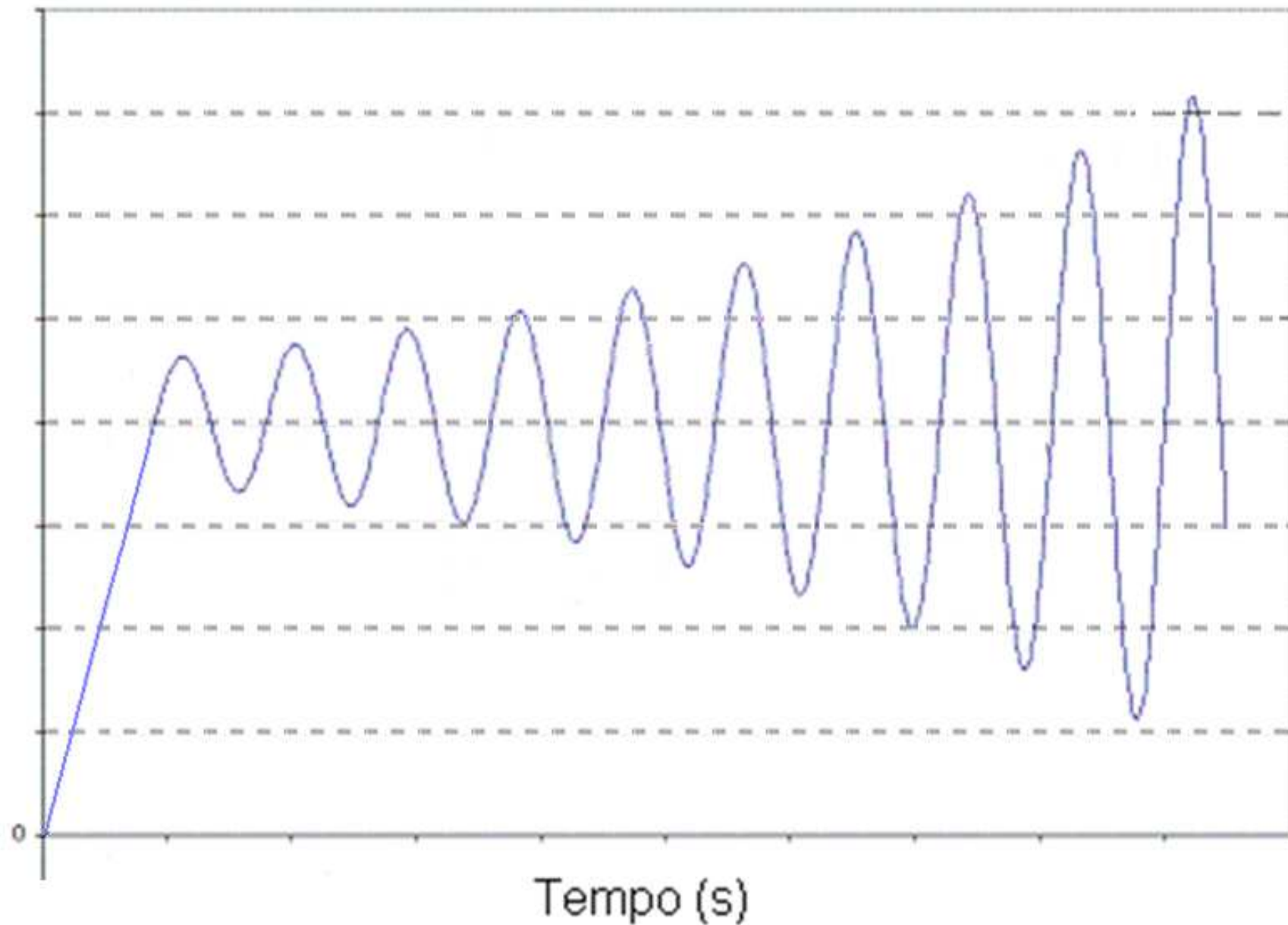
Entretanto, se $\zeta < 0$ então:

o sistema é instável

$\zeta < 0 \rightarrow$ sistema instável (um exemplo)



$\zeta < 0 \rightarrow$ sistema instável (outro exemplo)





Departamento de
Engenharia Eletromecânica

Obrigado!

Felippe de Souza

felippe@ubi.pt