

Control Systems

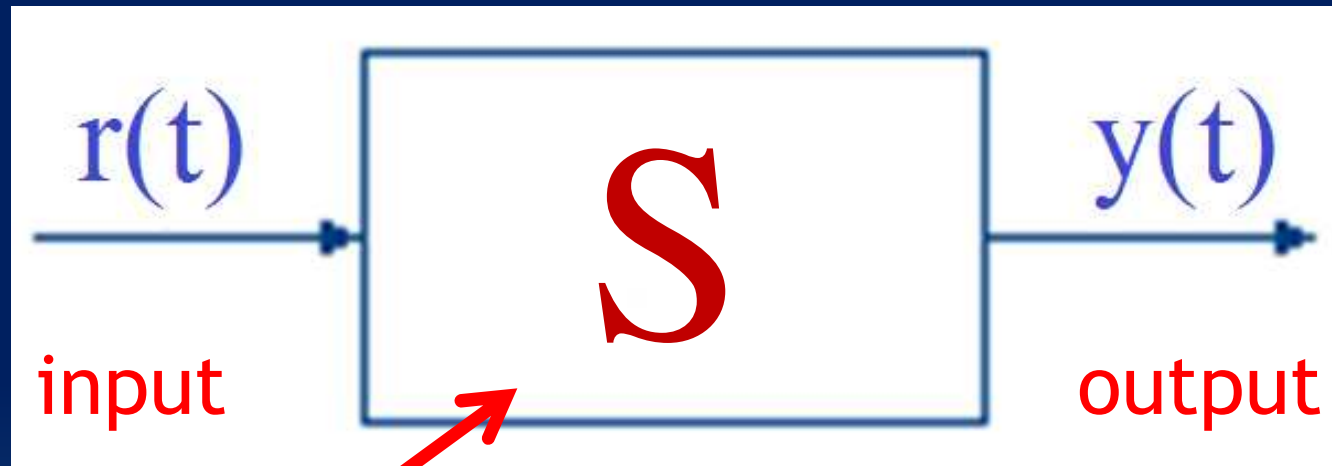
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"Time domain analysis"

part II — 2nd order systems

J. A. M. Felippe de Souza

Time domain analysis - 2nd order systems

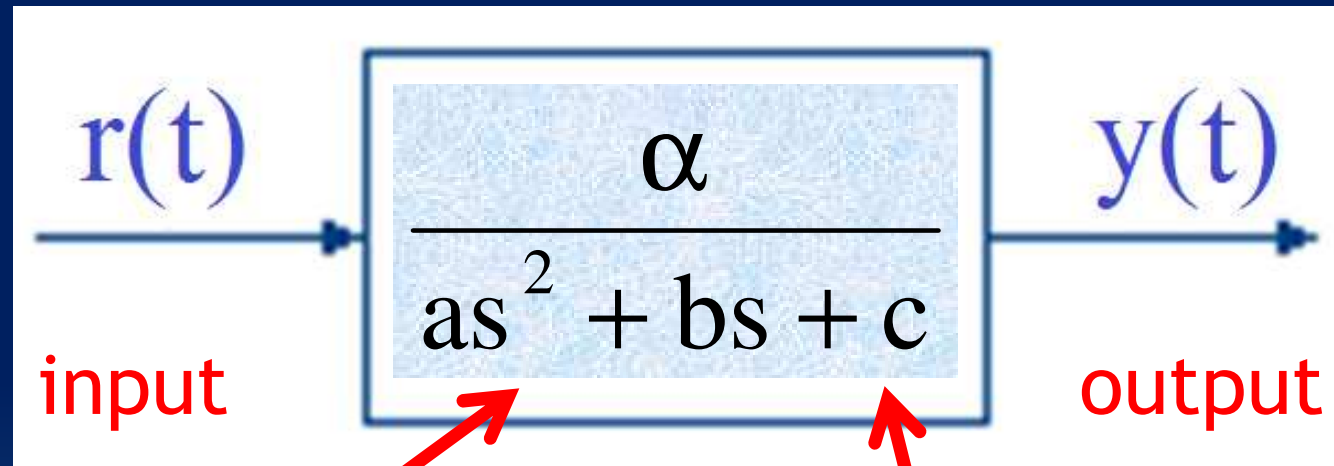


Second order systems

of the type

$$G(s) = \frac{\alpha}{as^2 + bs + c}$$

Time domain analysis - 2nd order systems

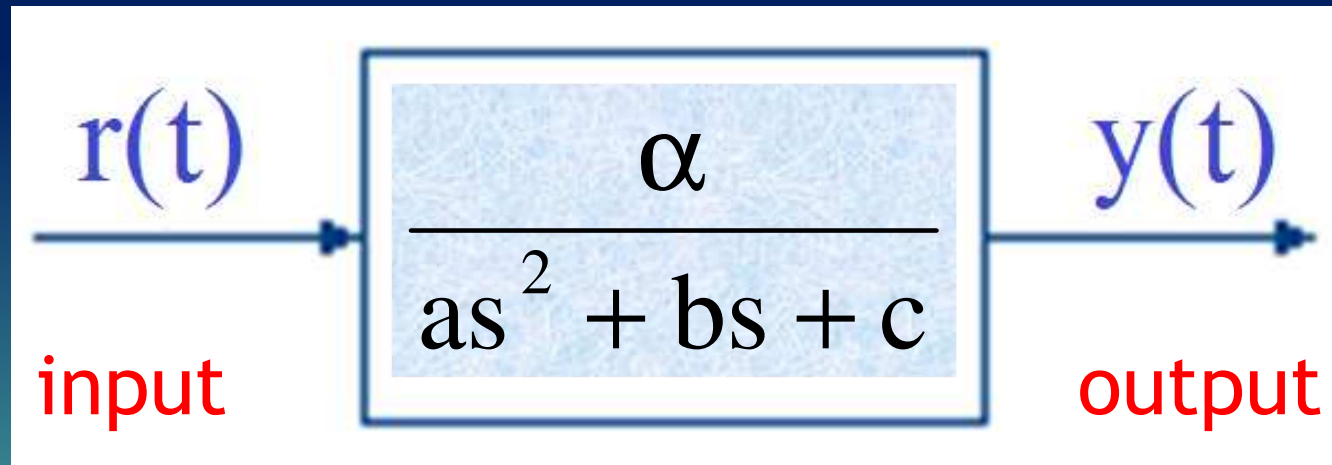


Second order systems

of the type

$$G(s) = \frac{\alpha}{as^2 + bs + c}$$

Second order systems:



that is:

$$\frac{Y(s)}{R(s)} = \frac{\alpha}{as^2 + bs + c}$$

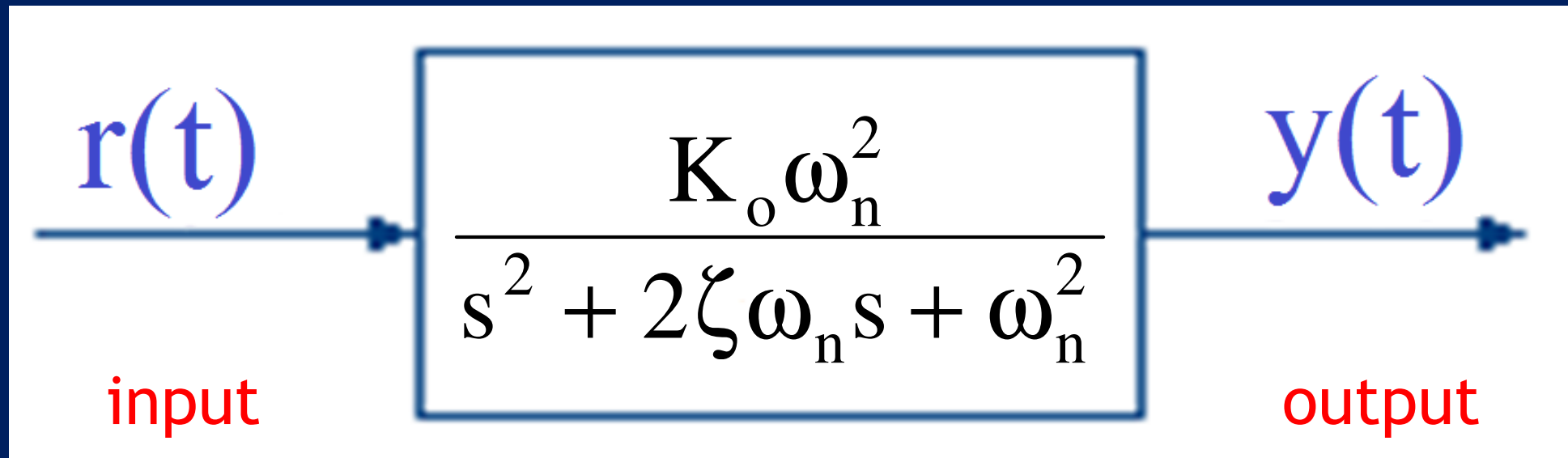


$$\frac{Y(s)}{R(s)} = \frac{\frac{\alpha}{a}}{s^2 + \frac{b}{a}s + \frac{c}{a}}$$

$$K_o \omega_n^2$$

$$2\zeta \omega_n$$

$$\omega_n^2$$



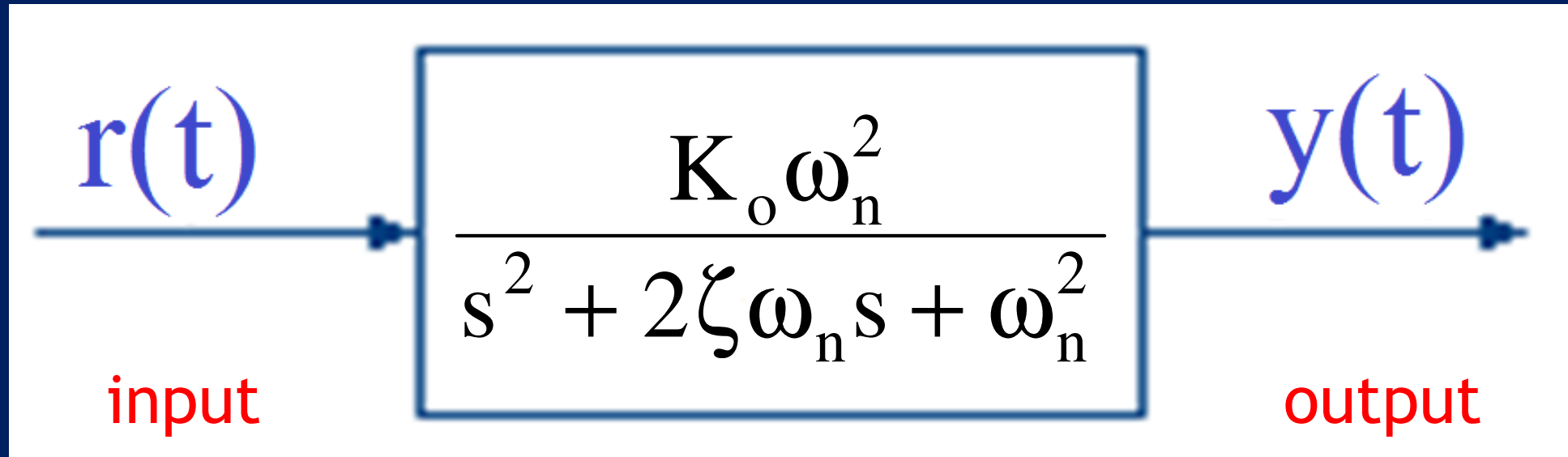
K_o = gain of the system

ζ = damping coefficient

ω_n = natural frequency

the transfer function can be rewritten as:

$$\frac{Y(s)}{R(s)} = \frac{K_o \omega_n^2}{s^2 + 2\zeta \omega_n s + \omega_n^2}$$



K_o = gain of the system

ζ = damping coefficient

ω_n = natural frequency

Besides these 3 above parameters, we also have

ω_d = damping frequency

$$\omega_d = \omega_n \cdot \sqrt{1 - \zeta^2} \quad 0 < \zeta \leq 1$$

Example 1:

$$\frac{Y(s)}{R(s)} = \frac{3}{4s^2 + 12s + 1}$$

poles:

$$s = -2,914$$

$$s = -0,086$$

$$K_o = 3 \quad \zeta = 3 \quad \omega_n = 0,5$$

poles are
real and
distinct

Example 2:

$$\frac{Y(s)}{R(s)} = \frac{3}{s^2 + 2s + 1}$$

poles:

$$s = -1$$

(duple)

$$K_o = 3 \quad \zeta = 1 \quad \omega_n = 1 \quad \omega_d = 0$$

poles are
real and
repeated

Example 3:

$$\frac{Y(s)}{R(s)} = \frac{3}{2s^2 + 2s + 2}$$

poles:
 $s = -0,5 \pm 0,866j$

complex
conjugate
poles

$$K_o = 1,5 \quad \zeta = 0,5 \quad \omega_n = 1 \quad \omega_d = 0,866$$

Example 4:

$$\frac{Y(s)}{R(s)} = \frac{3}{s^2 + 1}$$

poles:
 $s = \pm j$
(pure imaginary)

complex
conjugate
poles

$$K_o = 3 \quad \zeta = 0 \quad \omega_n = \omega_d = 1$$

Characteristic equation:

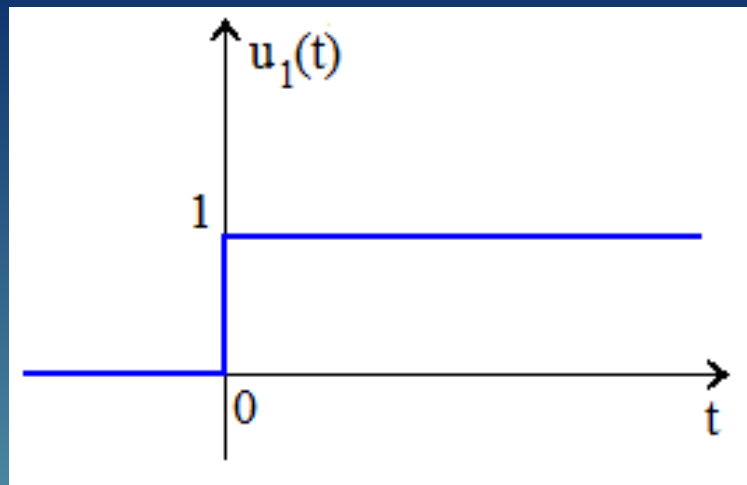
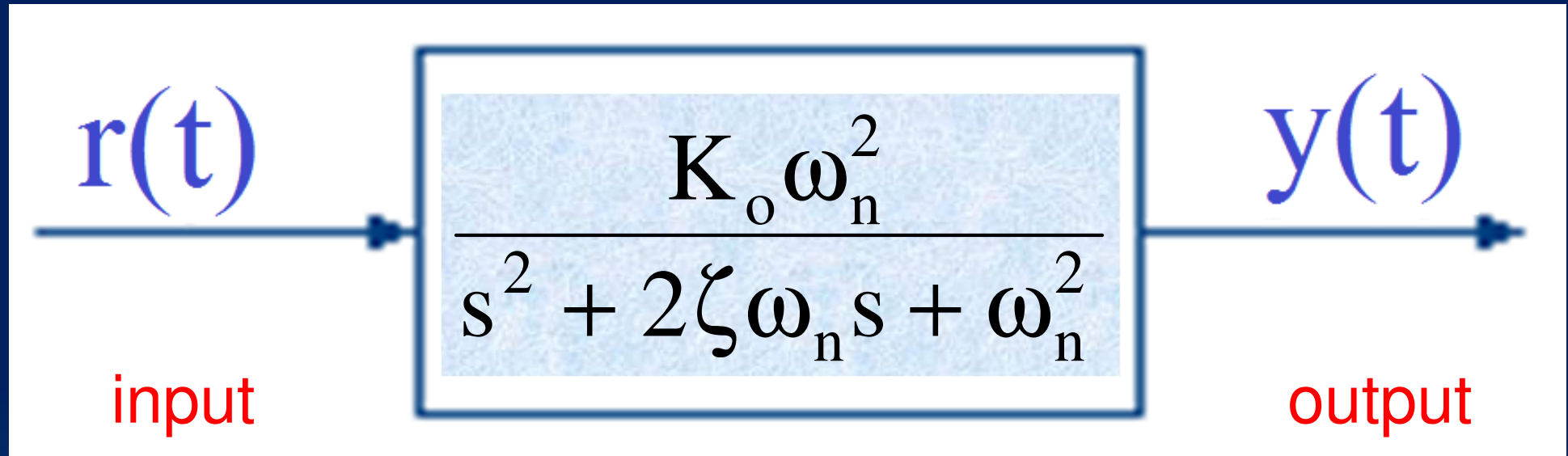
$$p(s) = s^2 + 2\zeta\omega_n s + \omega_n^2$$

$$\begin{aligned}\Delta &= 4\zeta^2\omega_n^2 - 4\omega_n^2 = \\ &= 4\omega_n^2(\zeta^2 - 1)\end{aligned}$$

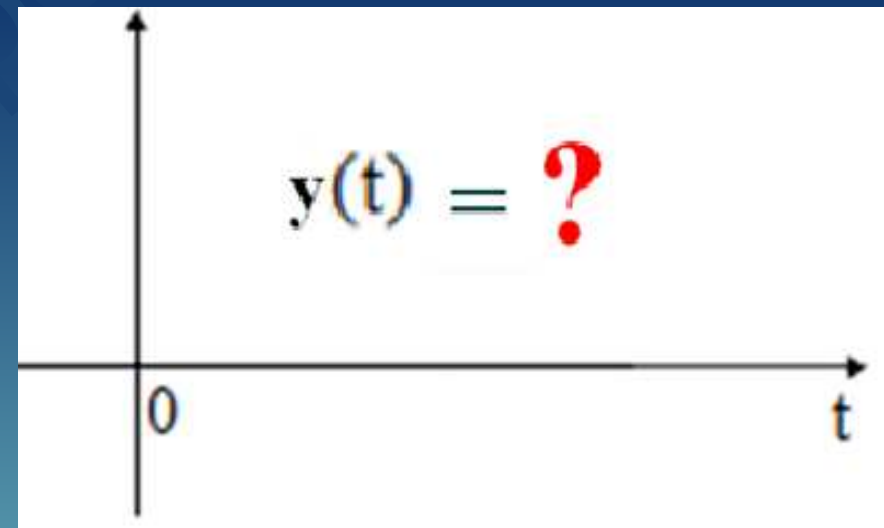
$$\left\{ \begin{array}{l} \Delta > 0 \rightarrow (\zeta^2 - 1) > 0 \rightarrow \zeta^2 > 1 \rightarrow \zeta > 1 \\ \Delta = 0 \rightarrow (\zeta^2 - 1) = 0 \rightarrow \zeta^2 = 1 \rightarrow \zeta = 1 \\ \Delta < 0 \rightarrow (\zeta^2 - 1) < 0 \rightarrow \zeta^2 < 1 \rightarrow \zeta < 1 \end{array} \right.$$

$\zeta > 1 \rightarrow$ poles are real and distinct
 $\zeta = 1 \rightarrow$ poles are real and repeated
 $0 < \zeta < 1 \rightarrow$ poles are complex conjugate

Time domain analysis - 2nd order systems

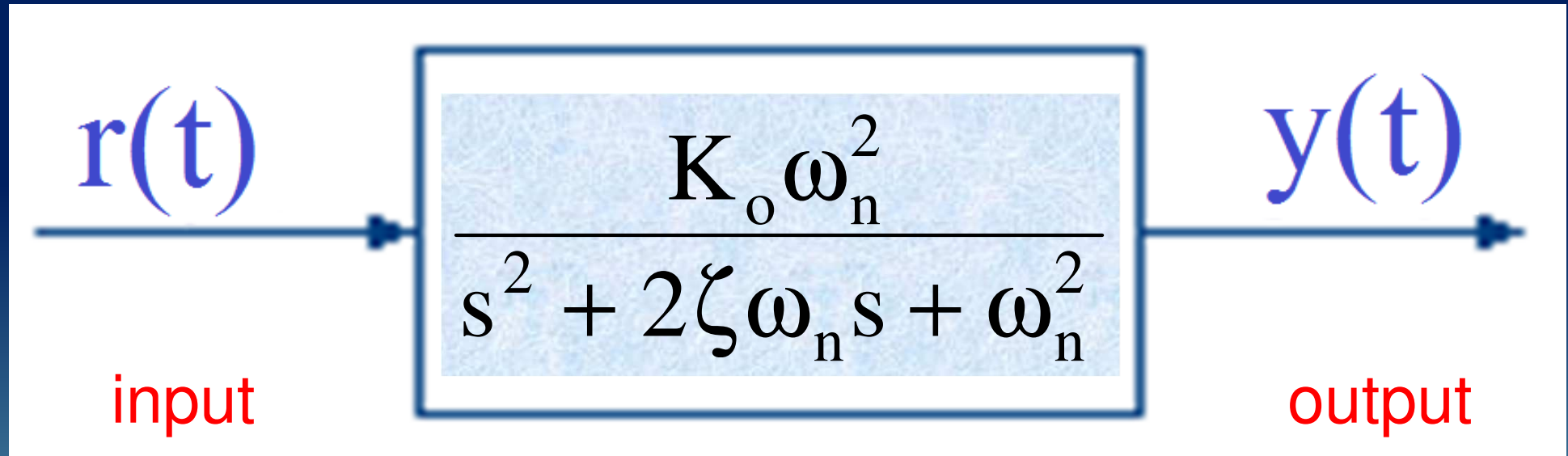


unit step input



What is the output?
(*step response*)

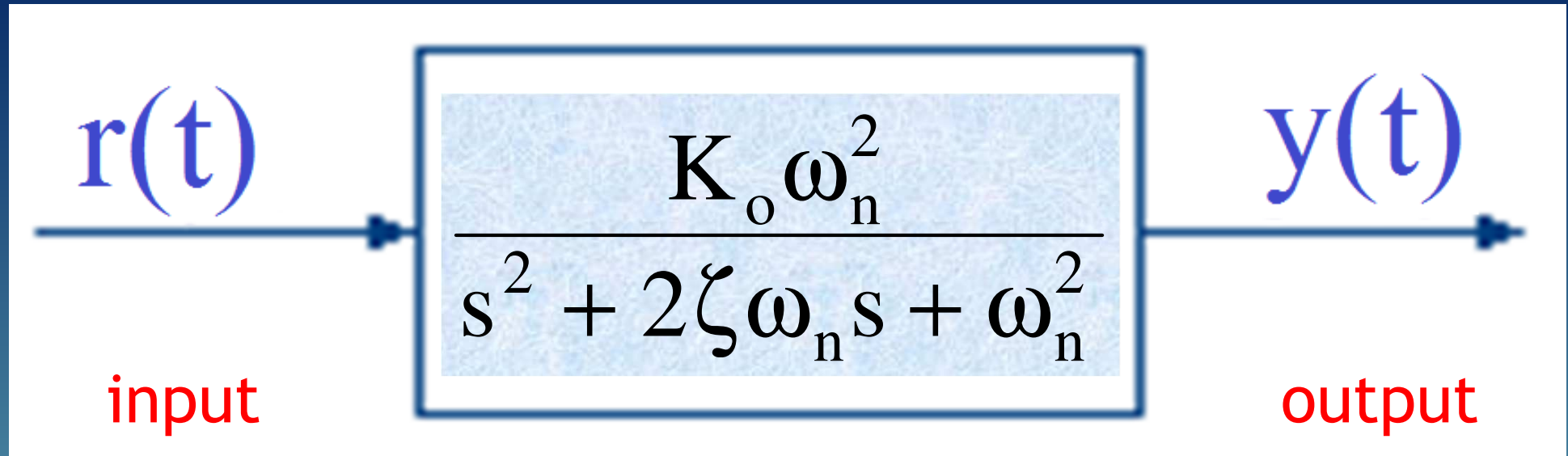
Time domain analysis - 2nd order systems



$$Y(s) = \frac{K_o \omega_n^2}{s^2 + 2\zeta \omega_n s + \omega_n^2} \cdot R(s)$$

and since $r(t)$ = unit step:

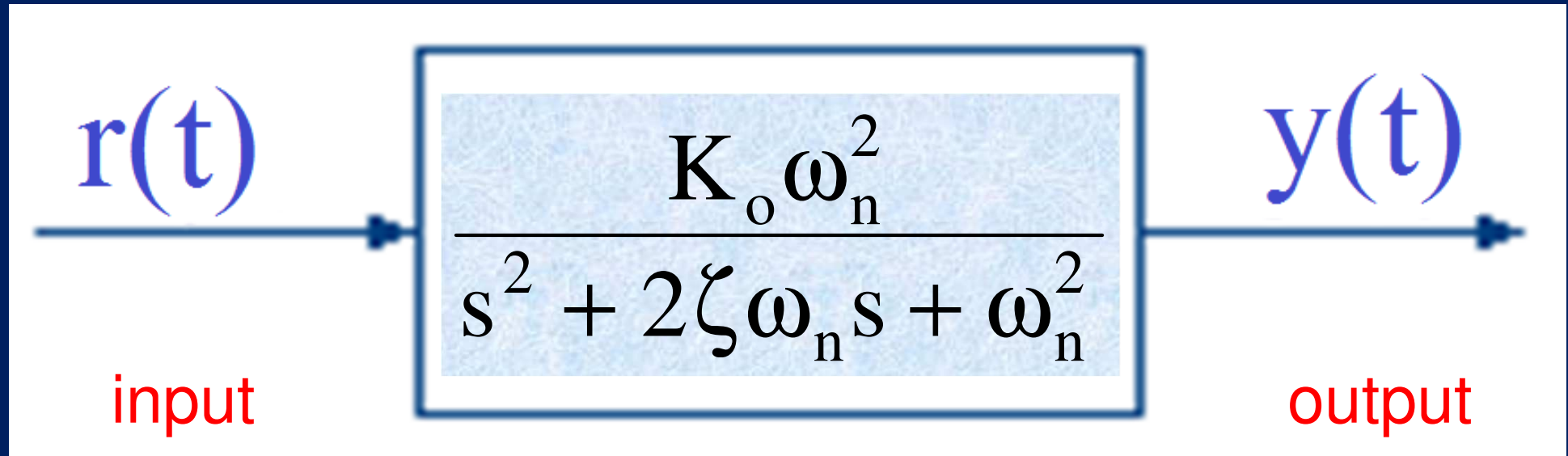
$$Y(s) = \frac{K_o \omega_n^2}{s^2 + 2\zeta \omega_n s + \omega_n^2} \cdot \frac{1}{s}$$



$$y(t) = \mathcal{L}^{-1}[Y(s)]$$

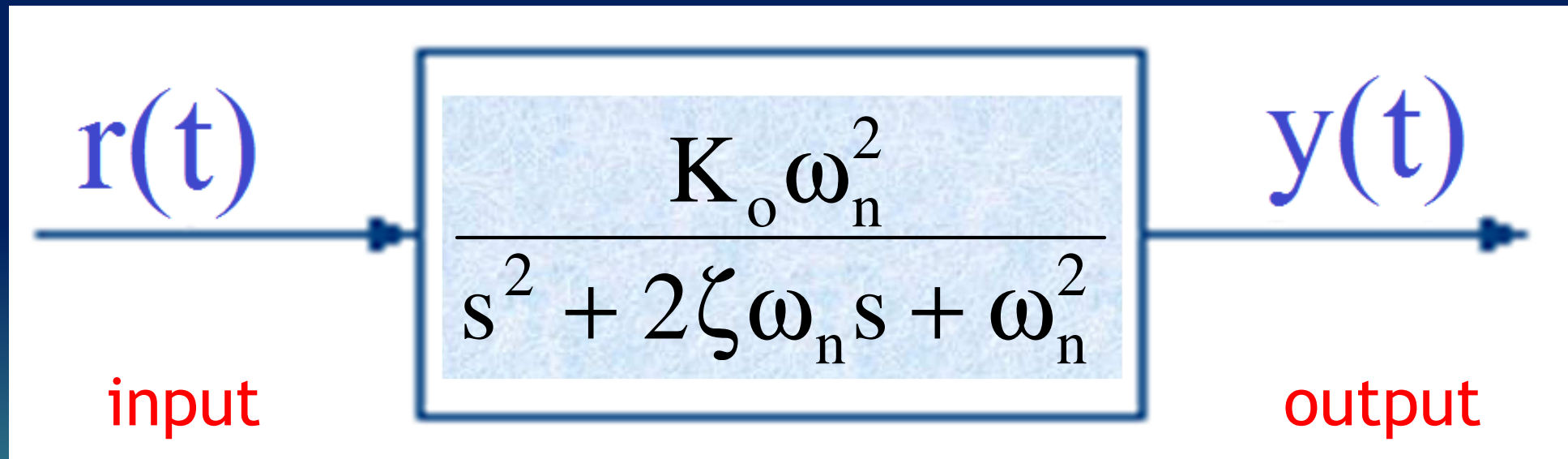
the **unit step** response depends on the value of ζ :

- a) $0 < \zeta < 1$ (*under damping*)
- b) $\zeta = 1$ (*critical damping*)
- c) $\zeta > 1$ (*over damping*)



Let us now see $y(t)$, the outputs to the **unit step** in these **3 cases**, starting with case (a)

a) $0 < \zeta < 1$ (*under damping*)



$$y(t) = \mathcal{L}^{-1}[Y(s)]$$

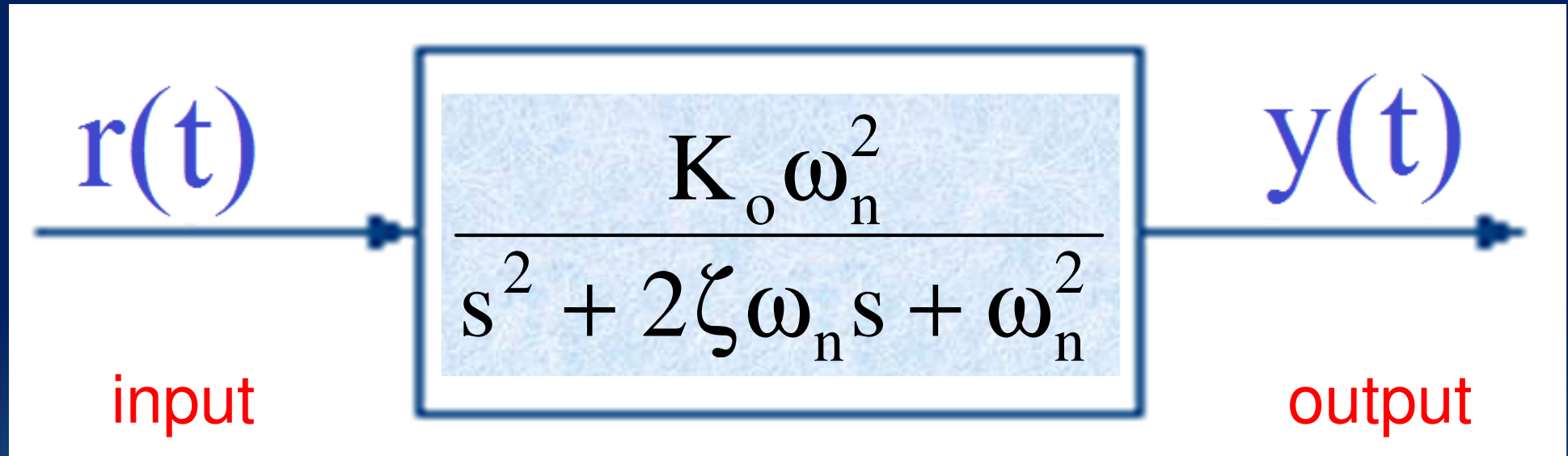
So, in the case $0 < \zeta < 1$ (*under damping*) the **unit step** response is:

$$y(t) = K_o \left[1 - e^{-\zeta \omega_n t} \left(\cos \omega_d t + \frac{\zeta}{\sqrt{1 - \zeta^2}} \cdot \sin \omega_d t \right) \right], \quad t > 0$$

where

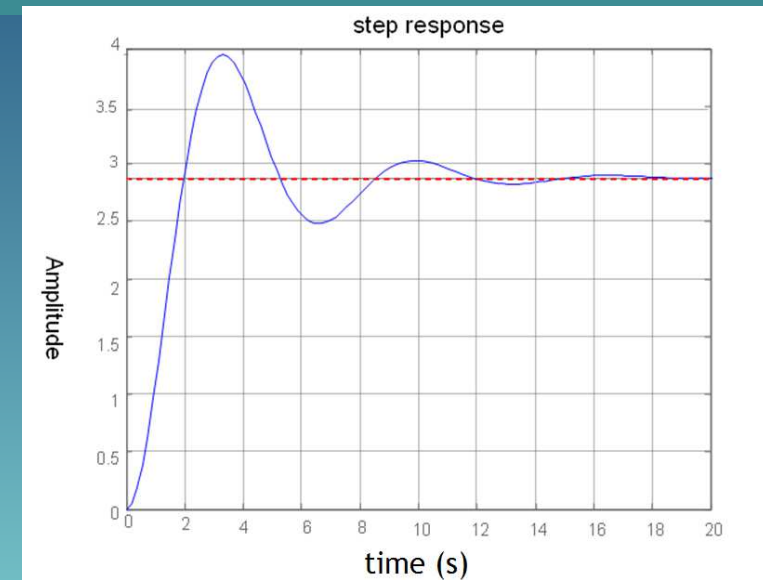
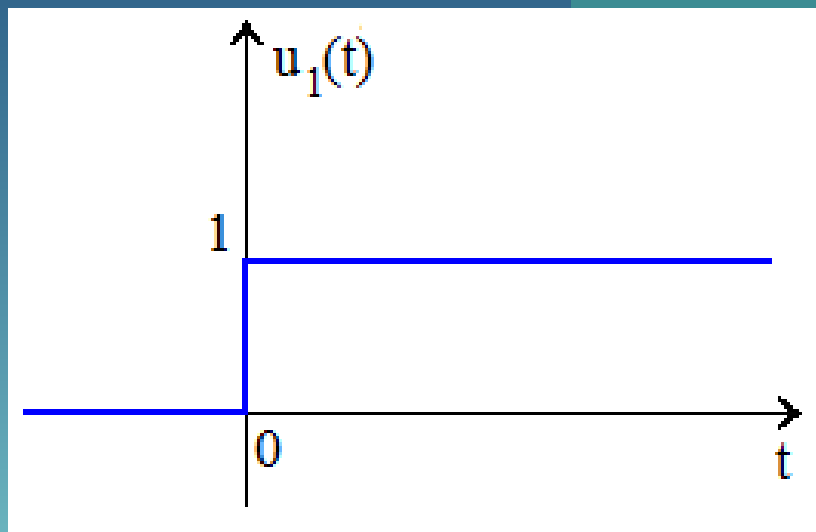
$$\omega_d = \omega_n \cdot \sqrt{1 - \zeta^2} \quad (\text{damping frequency})$$

Time domain analysis - 2nd order systems



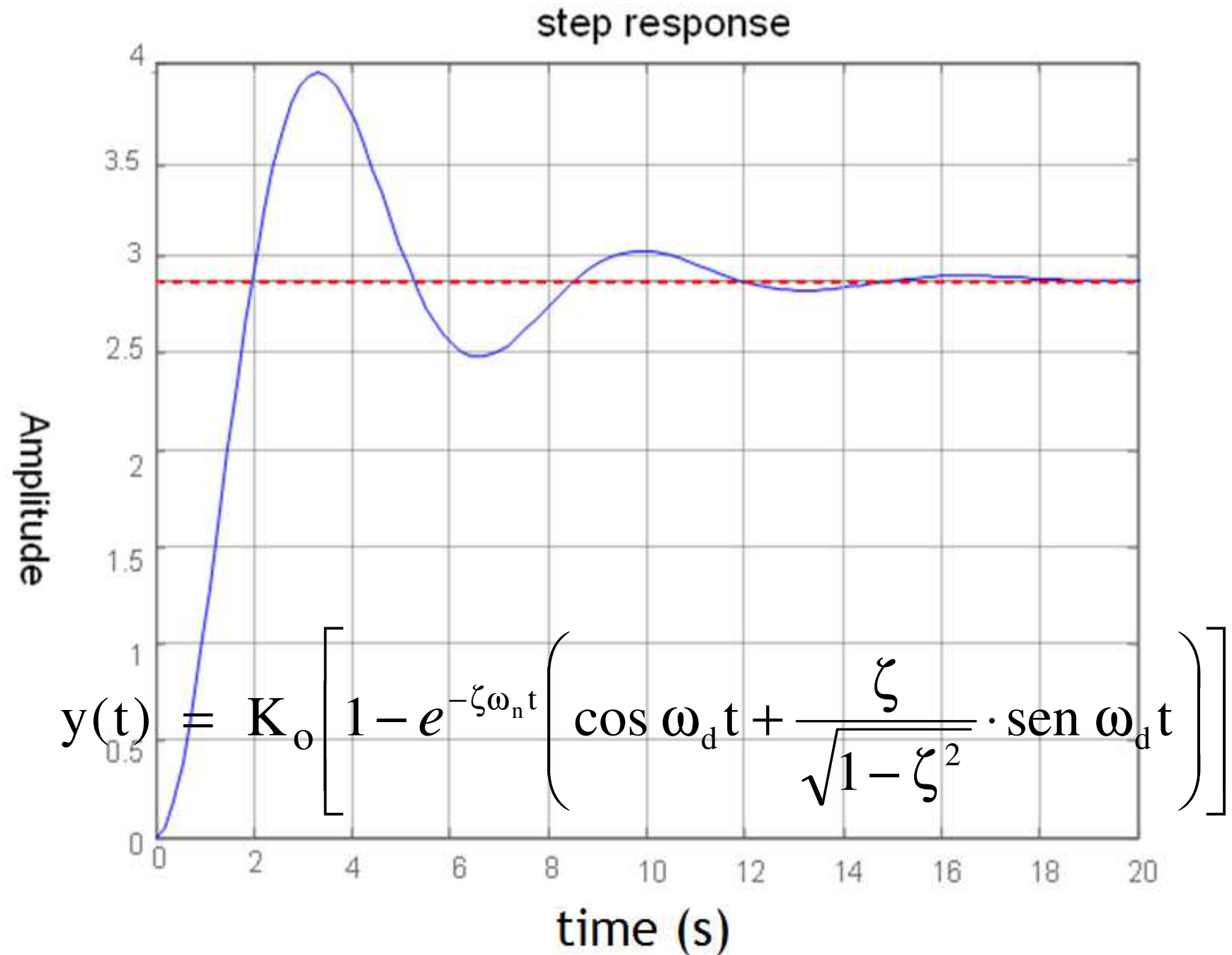
unit step response :

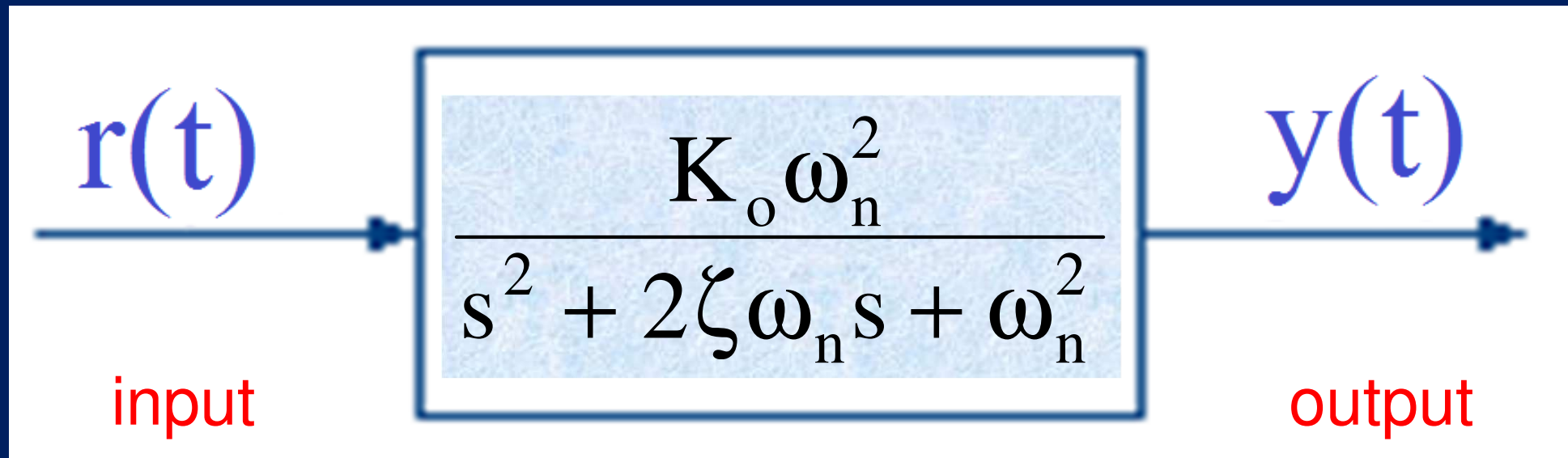
$$y(t) = K_o \left[1 - e^{-\zeta \omega_n t} \left(\cos \omega_d t + \frac{\zeta}{\sqrt{1 - \zeta^2}} \cdot \sin \omega_d t \right) \right]$$



Time domain analysis - 2nd order systems

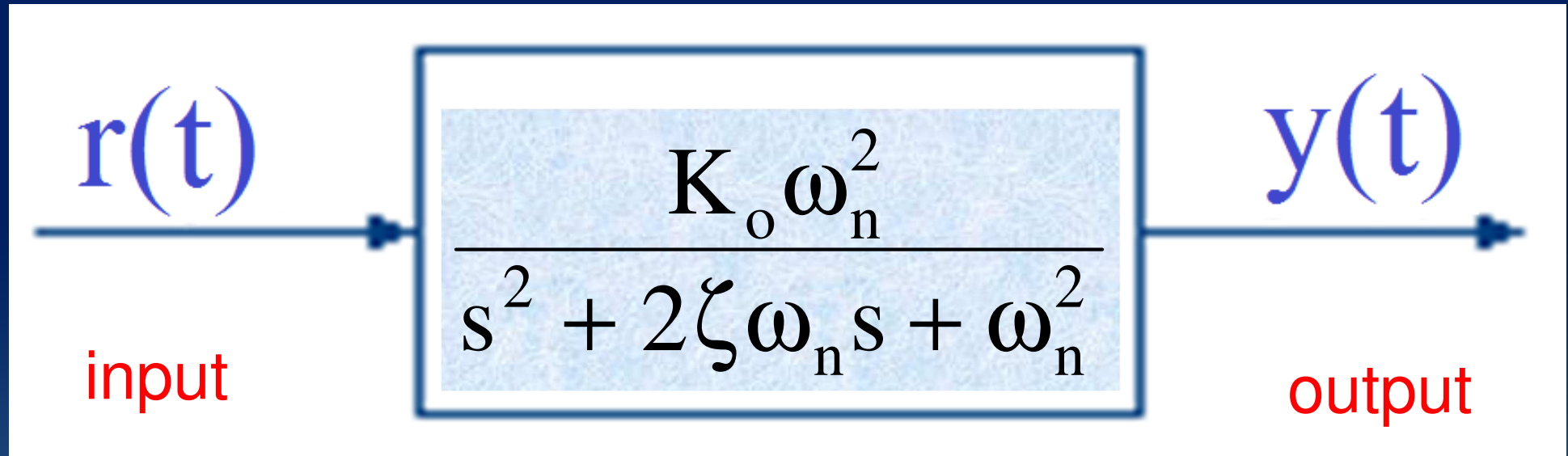
unit step response:





Let us now see $y(t)$, the output to the **unit step** for case (b)

b) $\zeta = 1$ (*critical damping*)

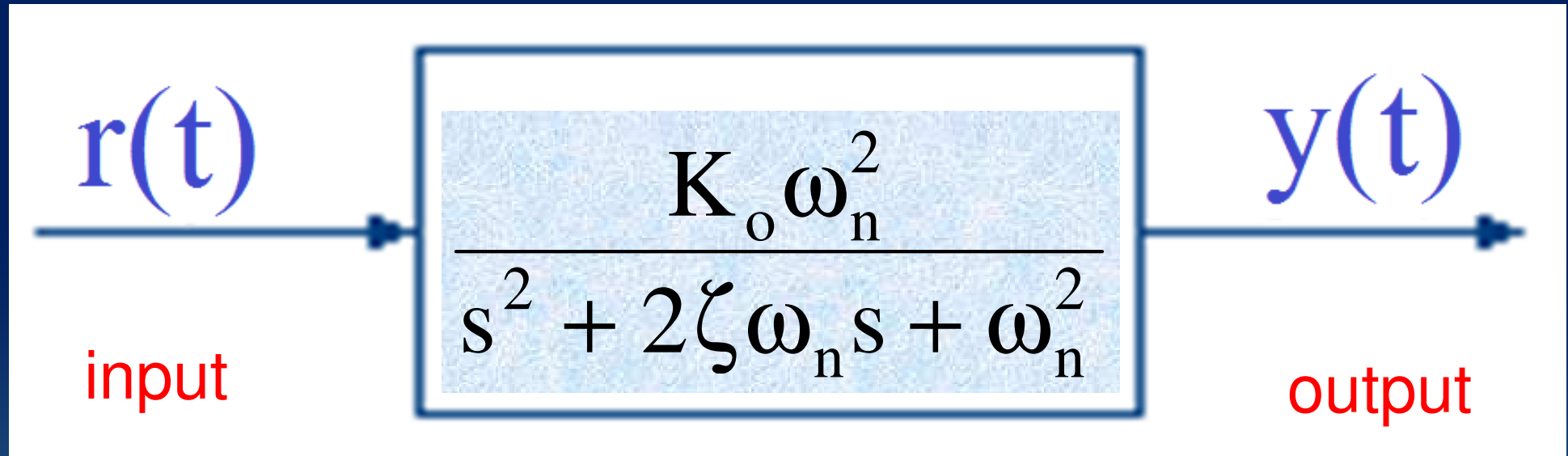


$$y(t) = \mathcal{L}^{-1}[Y(s)]$$

In the case $\zeta = 1$ (*critical damping*) the **unit step** response is:

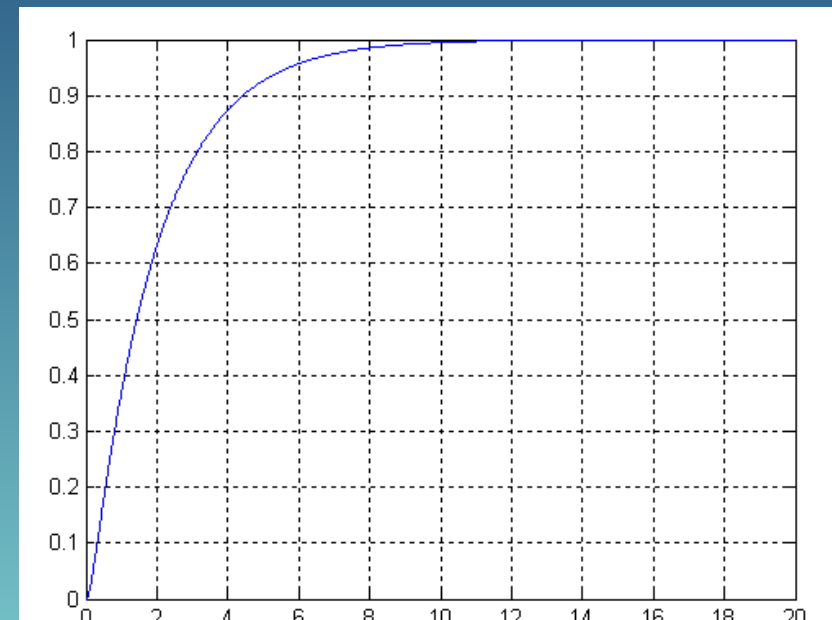
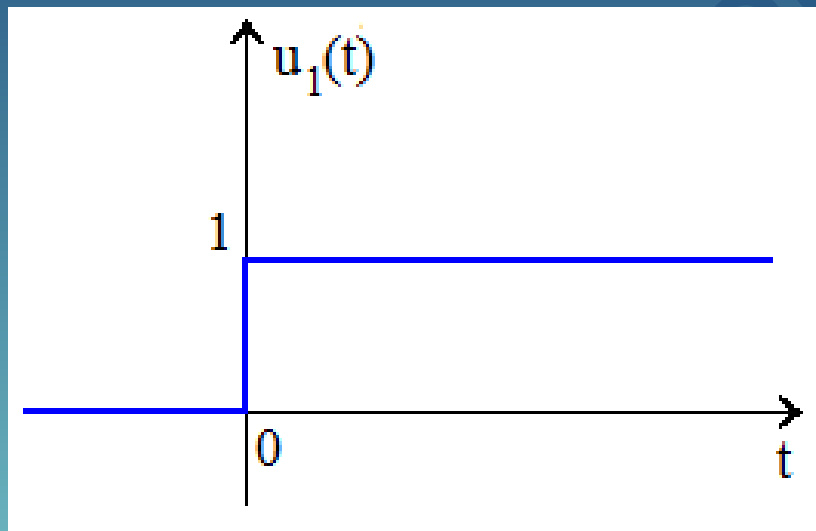
$$y(t) = K_o \left[1 - e^{-\zeta \omega_n t} \cdot (1 + \omega_n t) \right], \quad t > 0$$

Time domain analysis - 2nd order systems



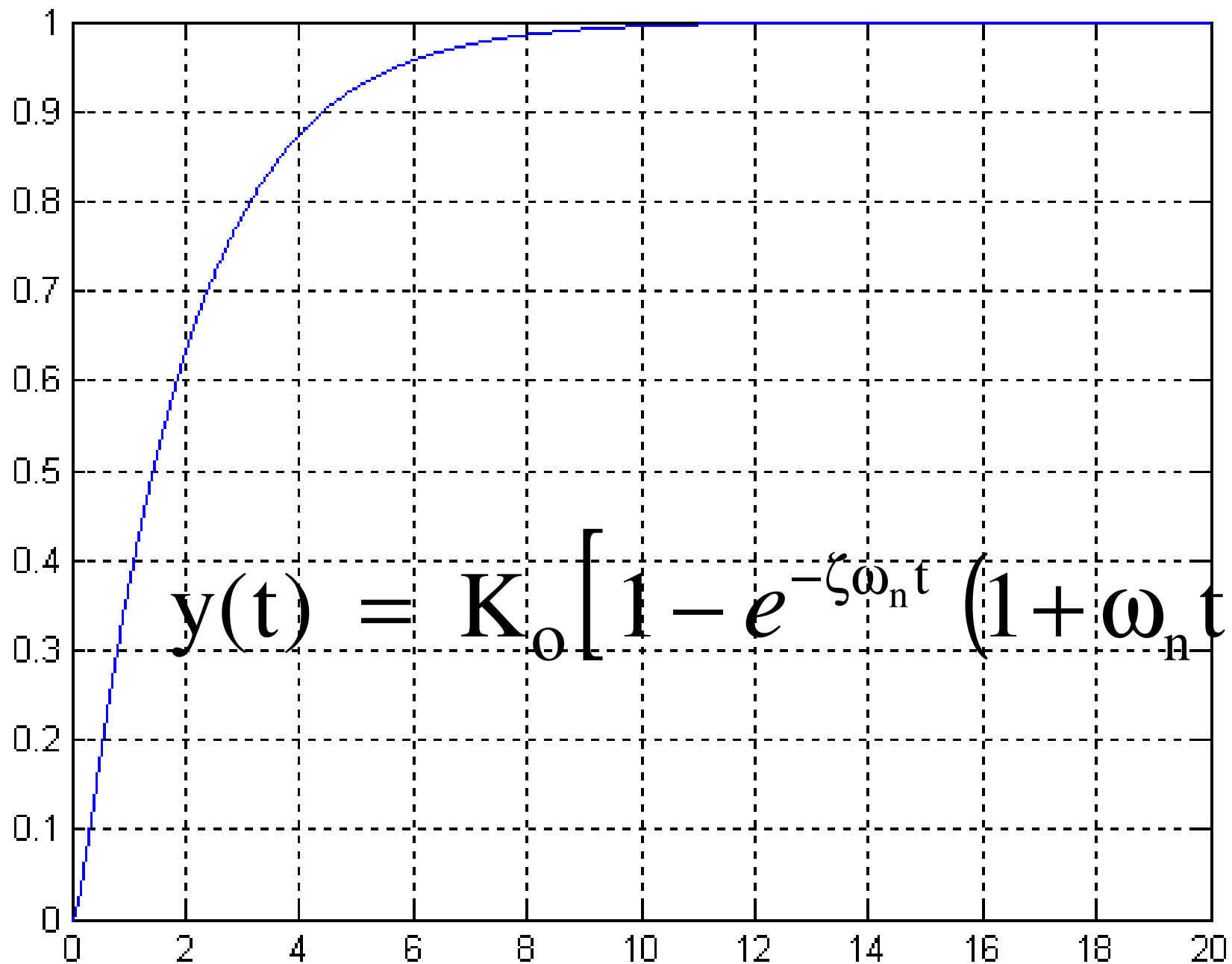
unit step response :

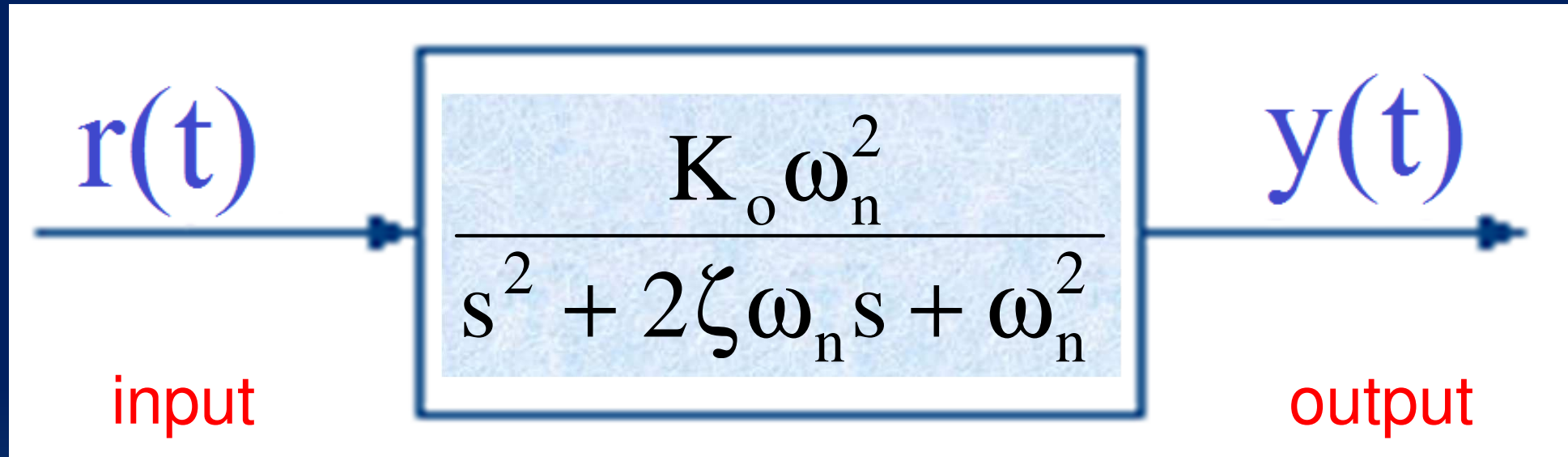
$$y(t) = K_o \left[1 - e^{-\zeta \omega_n t} (1 + \omega_n t) \right]$$



Time domain analysis - 2nd order systems

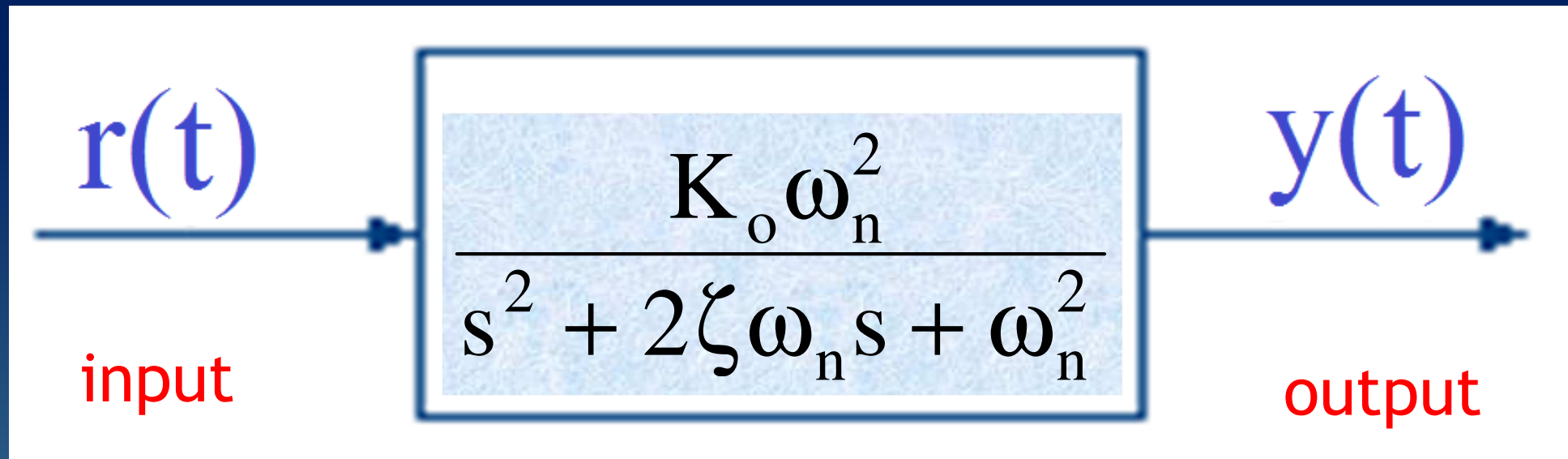
unit step response :





Finally, let us now see $y(t)$, the output to the **unit step** for case (c)

c) $\zeta > 1$ (*over damping*)



$$y(t) = \mathcal{L}^{-1}[Y(s)]$$

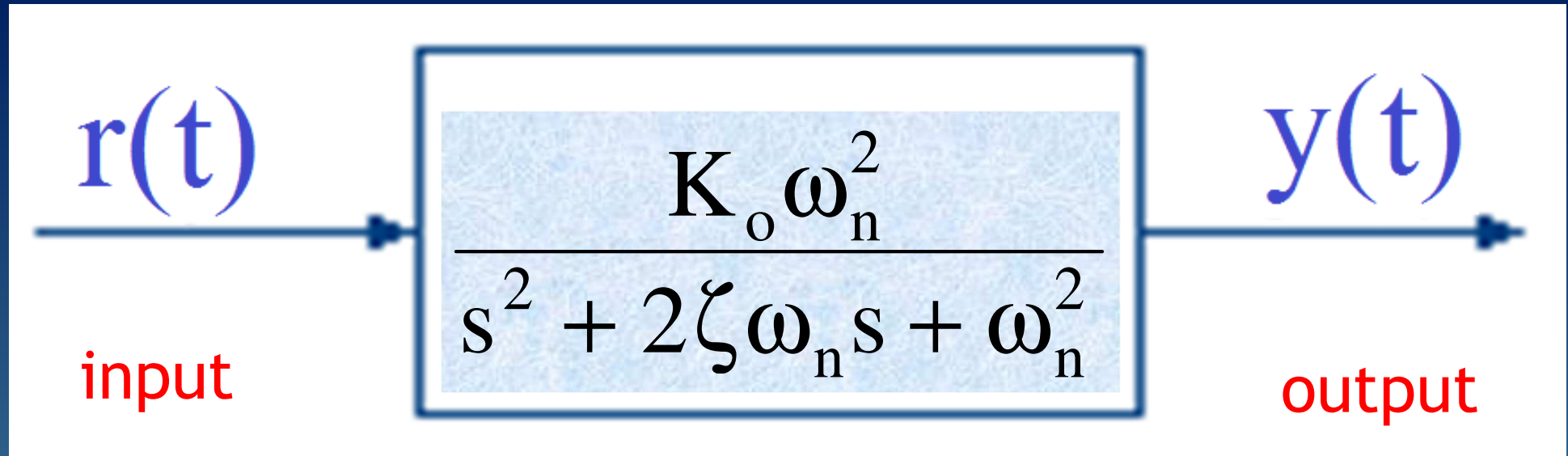
In the case $\zeta > 1$ (*over damping*) the **unit step** response is:

$$y(t) = K_o \left[1 + \frac{\omega_n}{2\sqrt{\zeta^2 - 1}} \cdot \left(\frac{e^{p_1 t}}{p_1} - \frac{e^{p_2 t}}{p_2} \right) \right], \quad t > 0$$

where

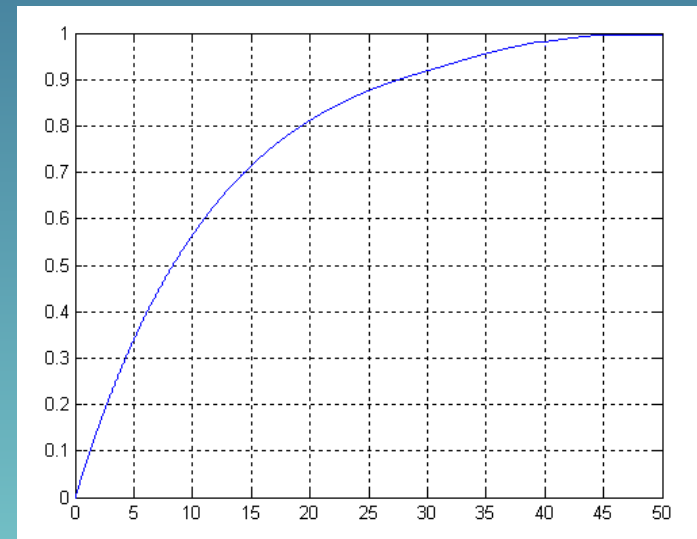
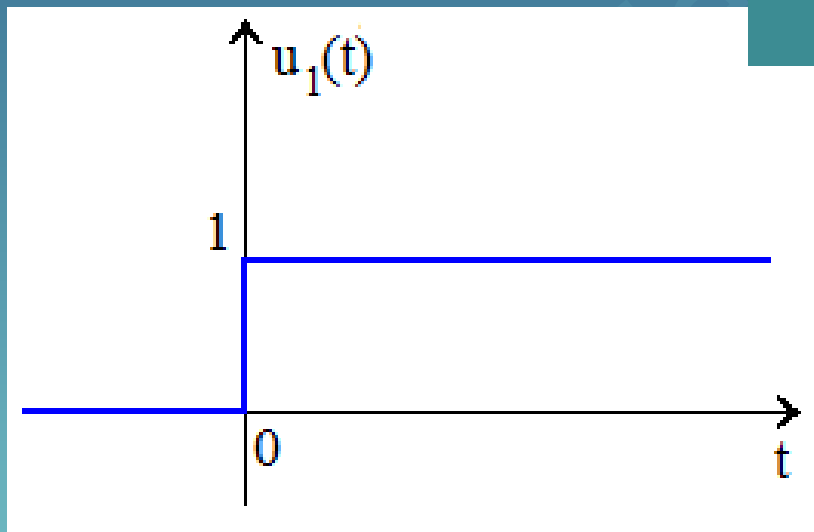
$$p_{1,2} = -\zeta \omega_n \mp \omega_n \sqrt{\zeta^2 - 1} = -\omega_n \left(\zeta \pm \sqrt{\zeta^2 - 1} \right) \text{ System has real poles}$$

Time domain analysis - 2nd order systems



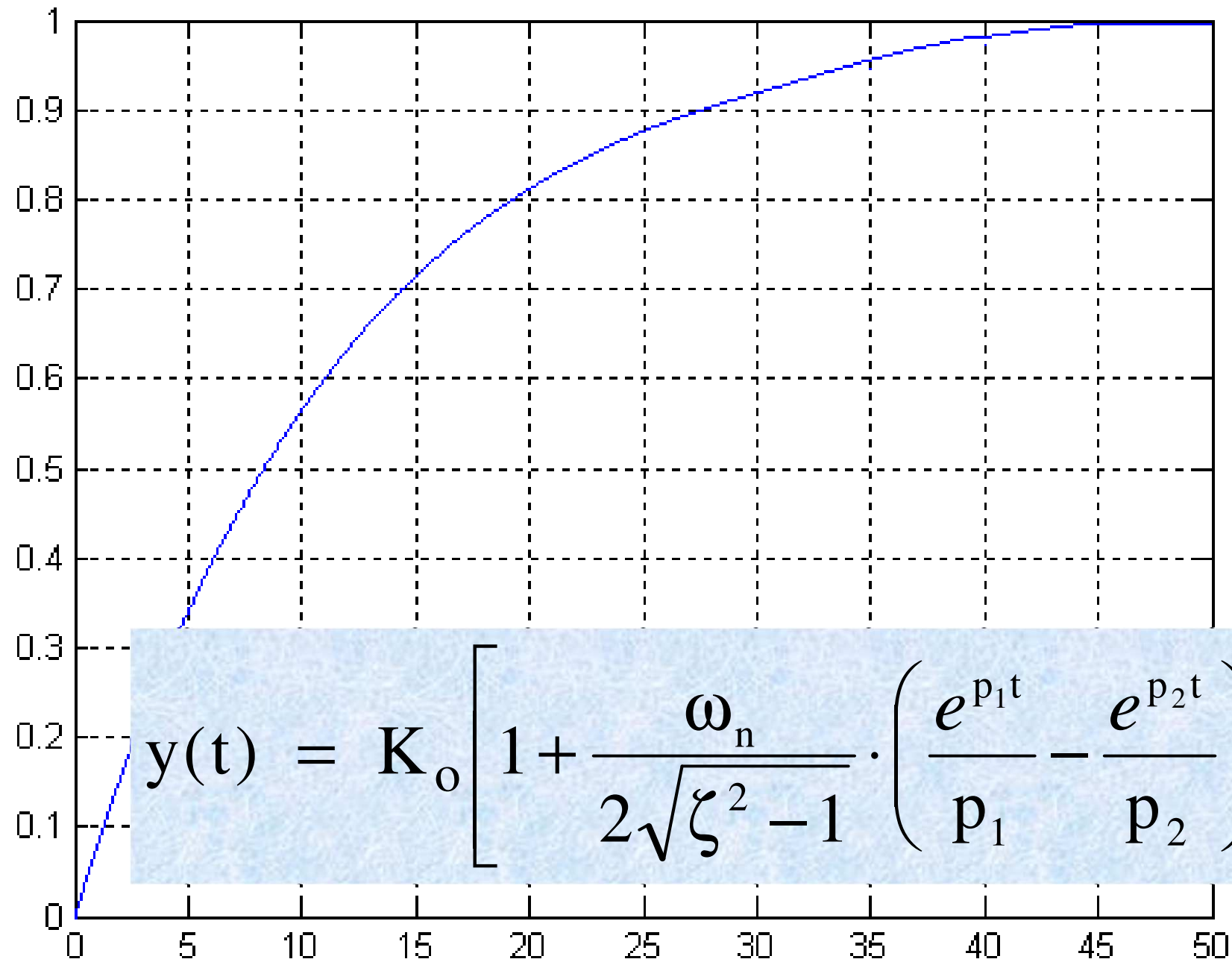
unit step response •

$$y(t) = K_o \left[1 + \frac{\omega_n}{2\sqrt{\zeta^2 - 1}} \cdot \left(\frac{e^{p_1 t}}{p_1} - \frac{e^{p_2 t}}{p_2} \right) \right]$$

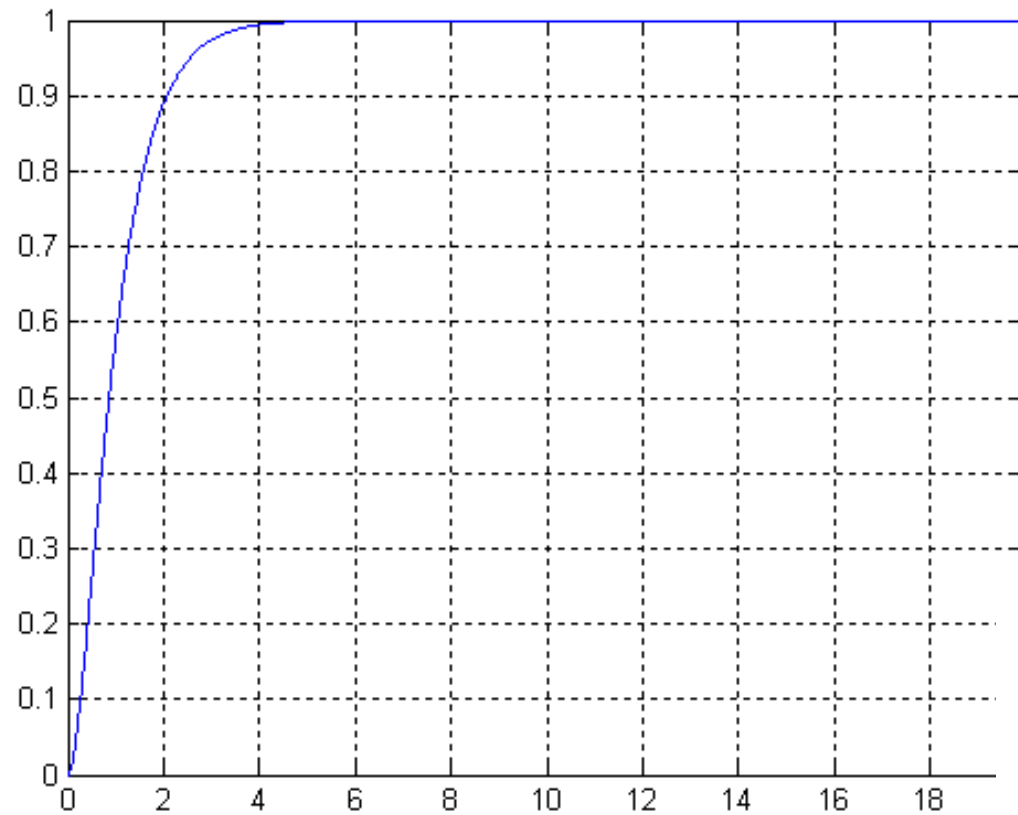


Time domain analysis - 2nd order systems

unit step response:



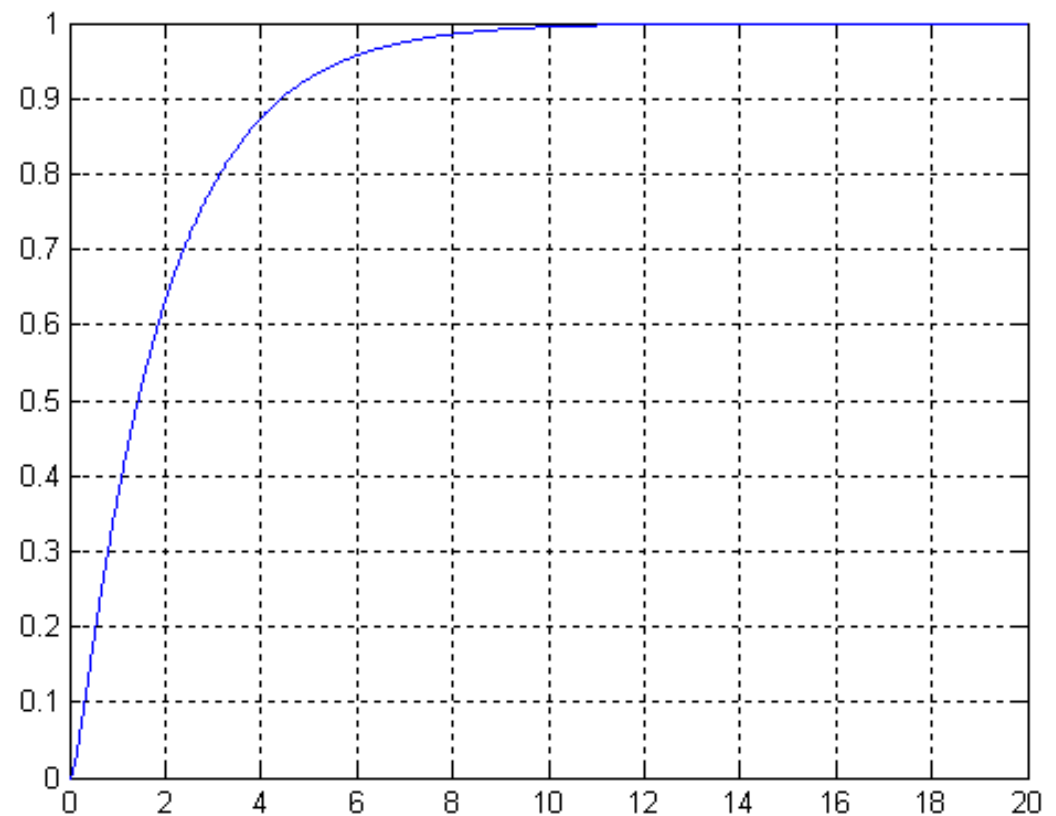
Time domain analysis - 2nd order systems



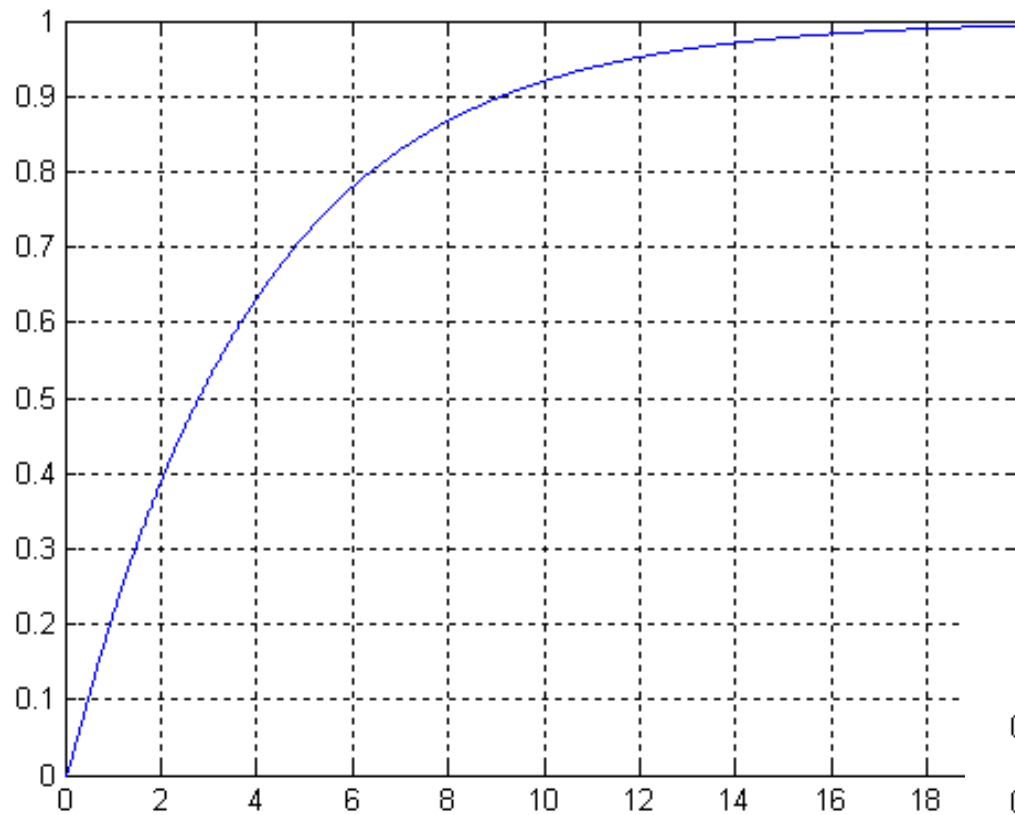
unit step
response

$\zeta = 1$

$\zeta = 2$



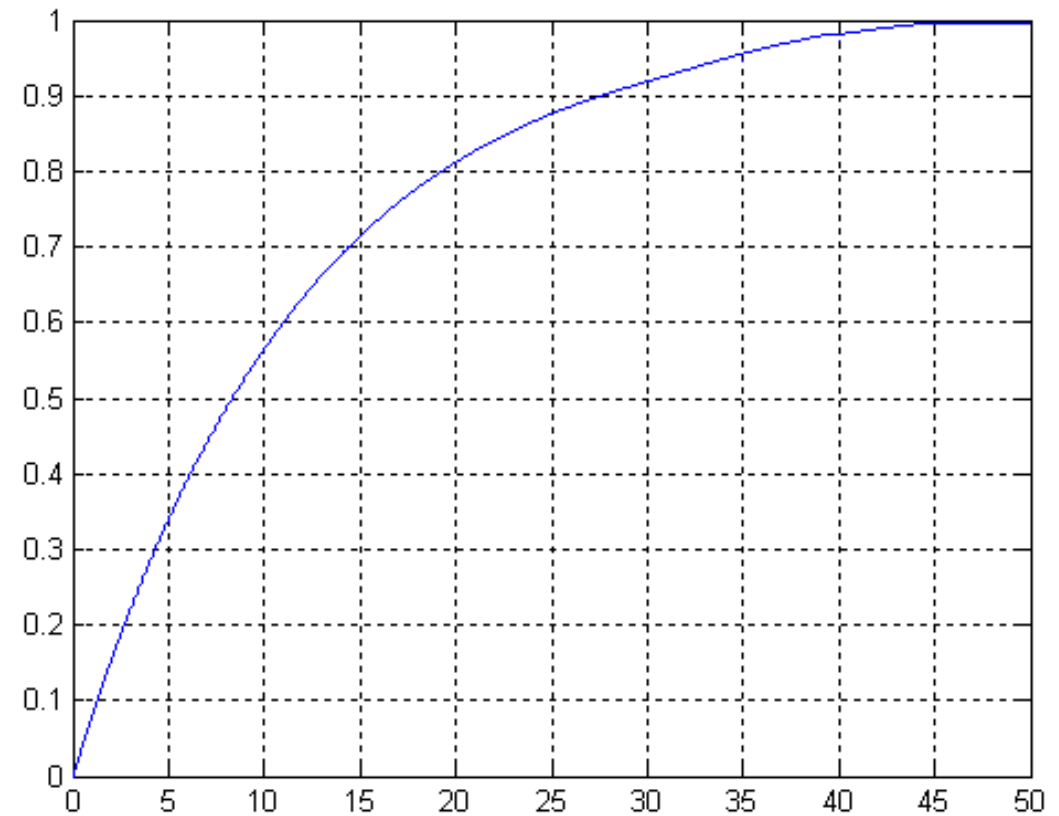
Time domain analysis - 2nd order systems



unit step
response

$$\zeta = 4$$

$$\zeta = 12$$



Let us now analyse some parameters associated with the under damping case

$$0 < \zeta < 1 \quad (\text{under damping})$$

In the case $0 < \zeta < 1$,
the unit step response

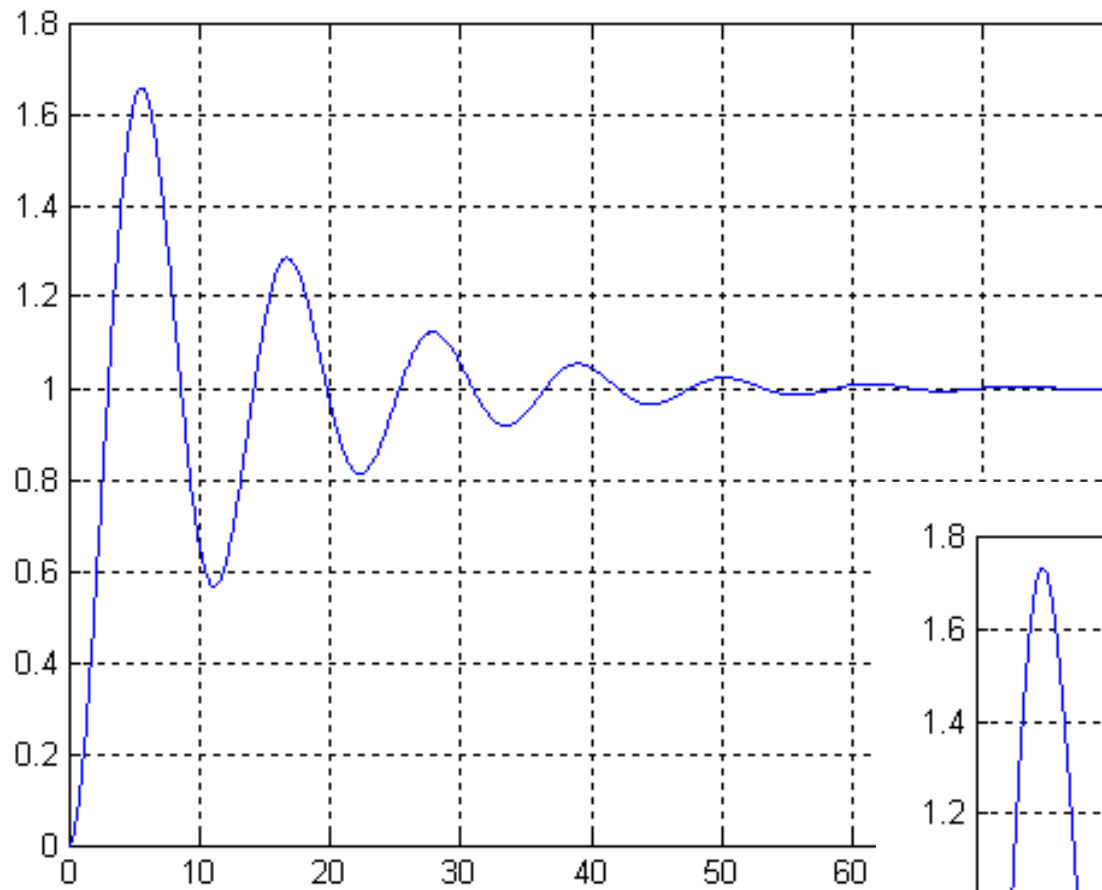
$$y(t) = K_o \left[1 - e^{-\zeta \omega_n t} \left(\cos \omega_d t + \frac{\zeta}{\sqrt{1 - \zeta^2}} \cdot \sin \omega_d t \right) \right], \quad t > 0$$

can have many different forms, depending on the
values of ζ (*damping coefficient*),
 ω_n (*natural frequency*) e K_o (*gain*)

Observe that ω_d depends on ζ and ω_n

$$\omega_d = \omega_n \cdot \sqrt{1 - \zeta^2} \quad (\text{damping frequency})$$

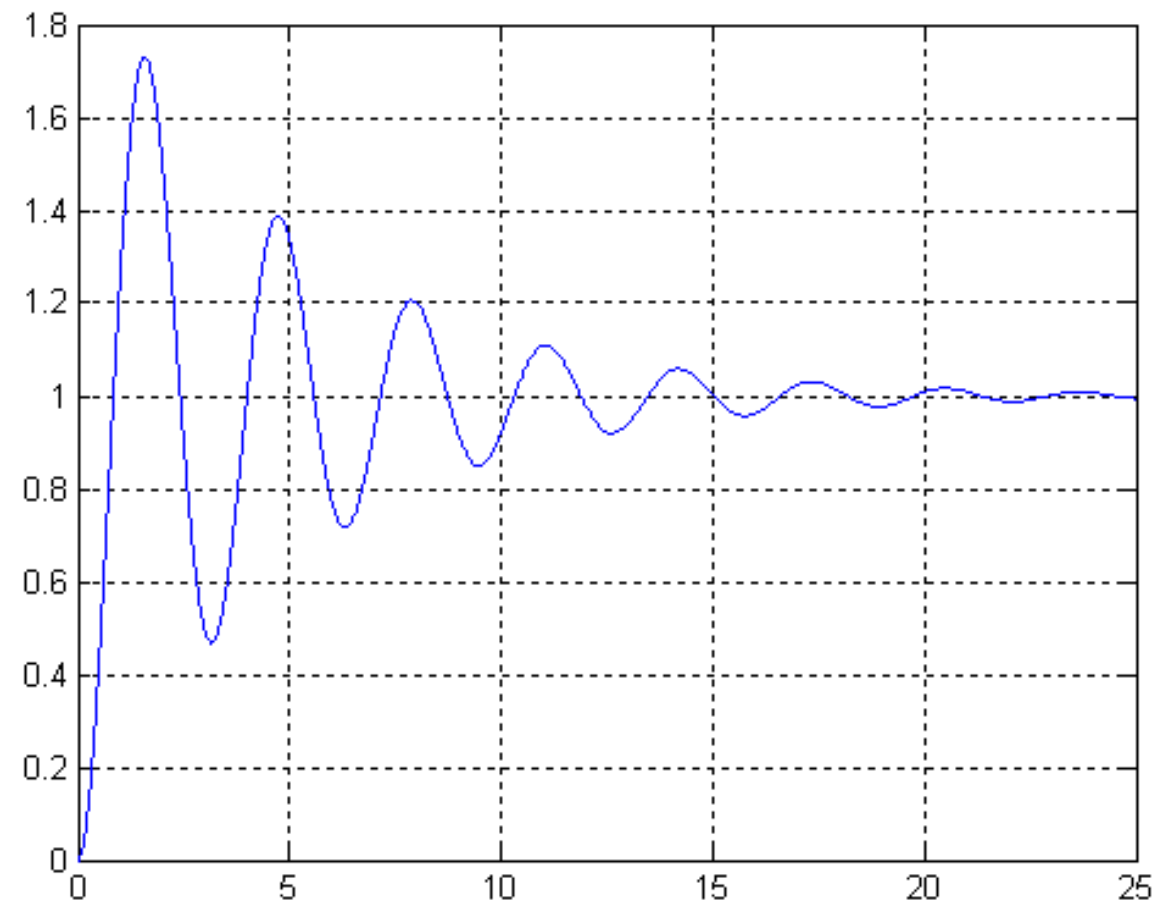
Time domain analysis - 2nd order systems



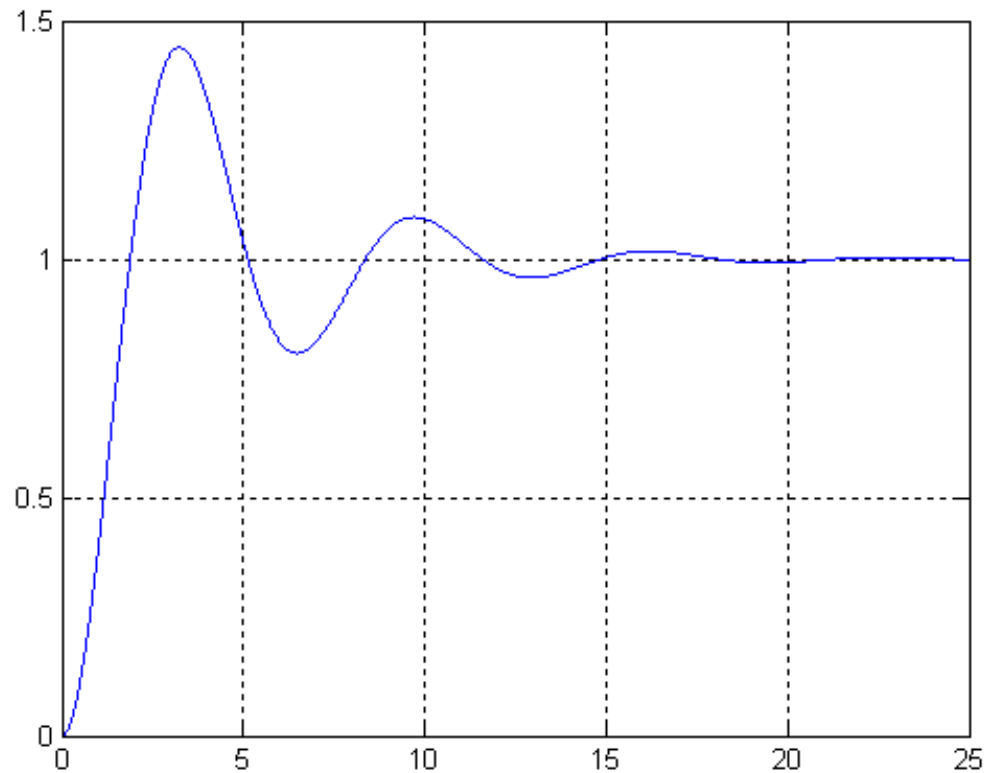
unit step
response

$$\zeta = 0.132$$
$$\omega_n = 0.57$$

$$\zeta = 0.1$$
$$\omega_n = 2$$



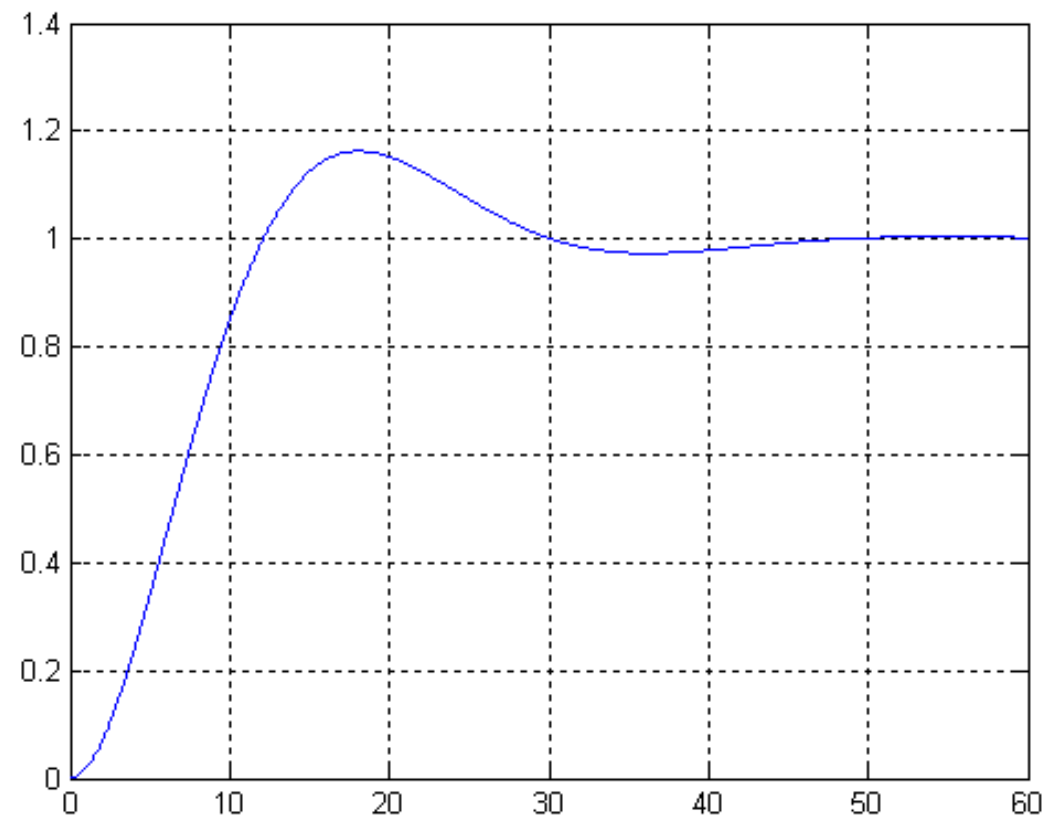
Time domain analysis - 2nd order systems



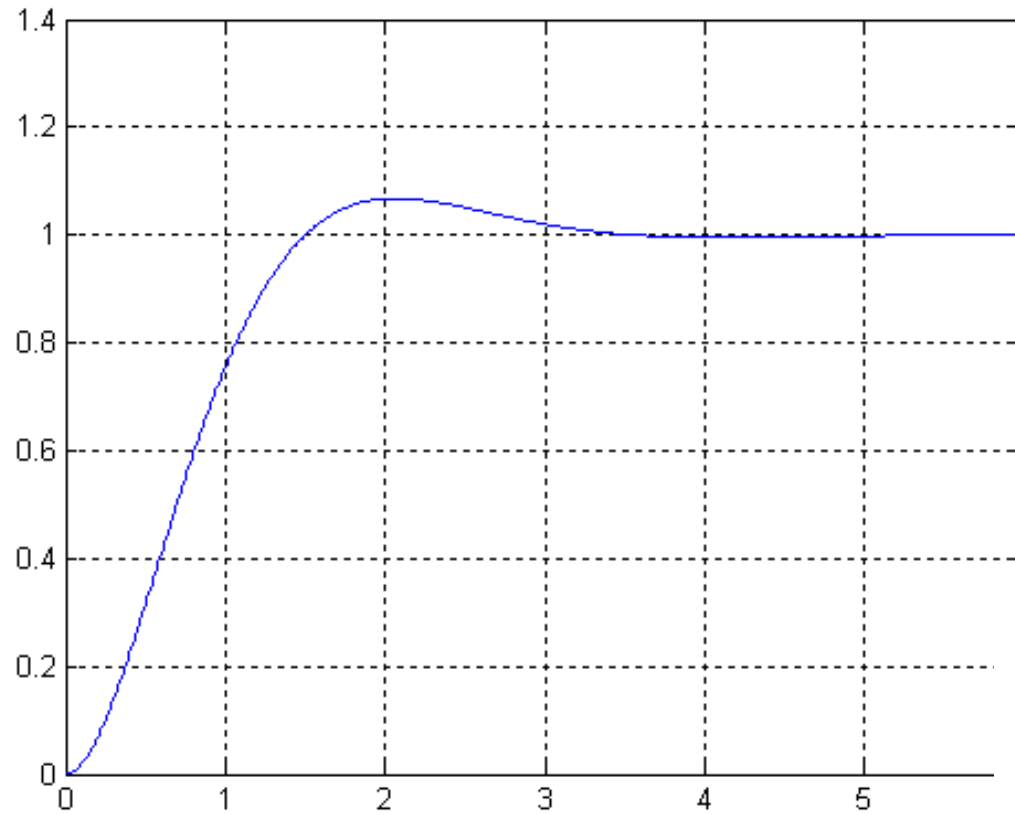
$$\zeta = 0,25$$
$$\omega_n = 1$$

$$\zeta = 0,5$$
$$\omega_n = 0,2$$

unit step
response



Time domain analysis - 2nd order systems



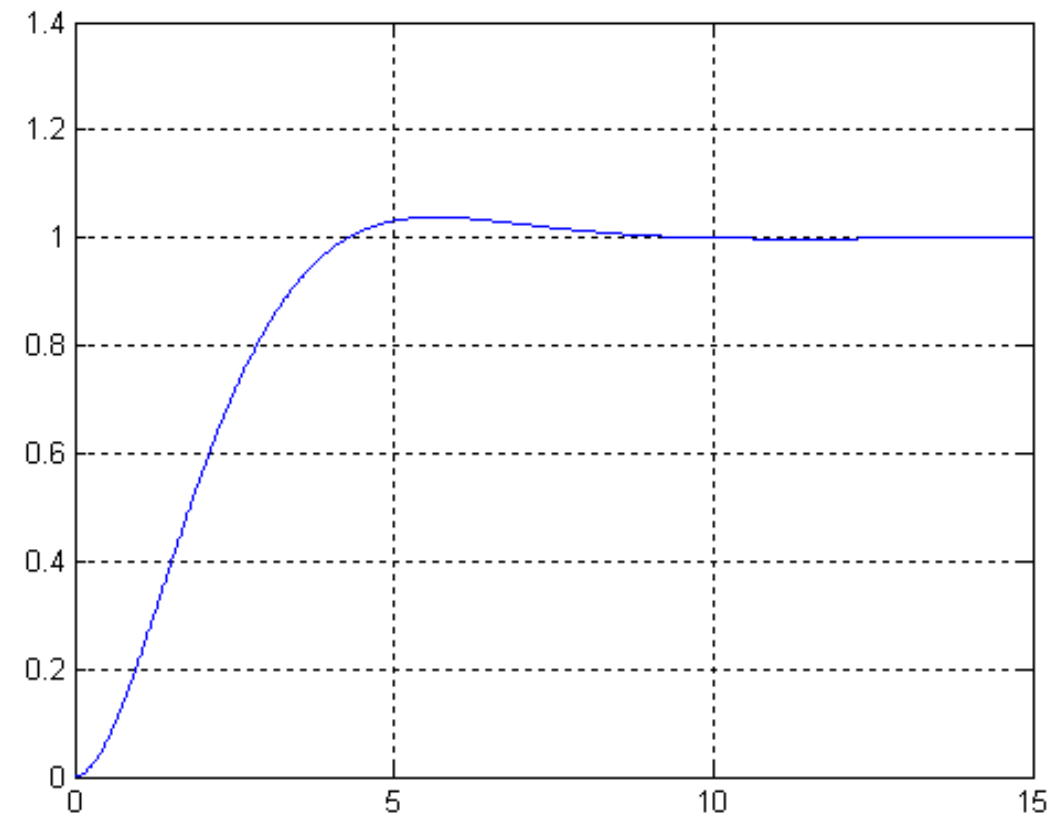
unit step
response

$$\zeta = 0,65$$

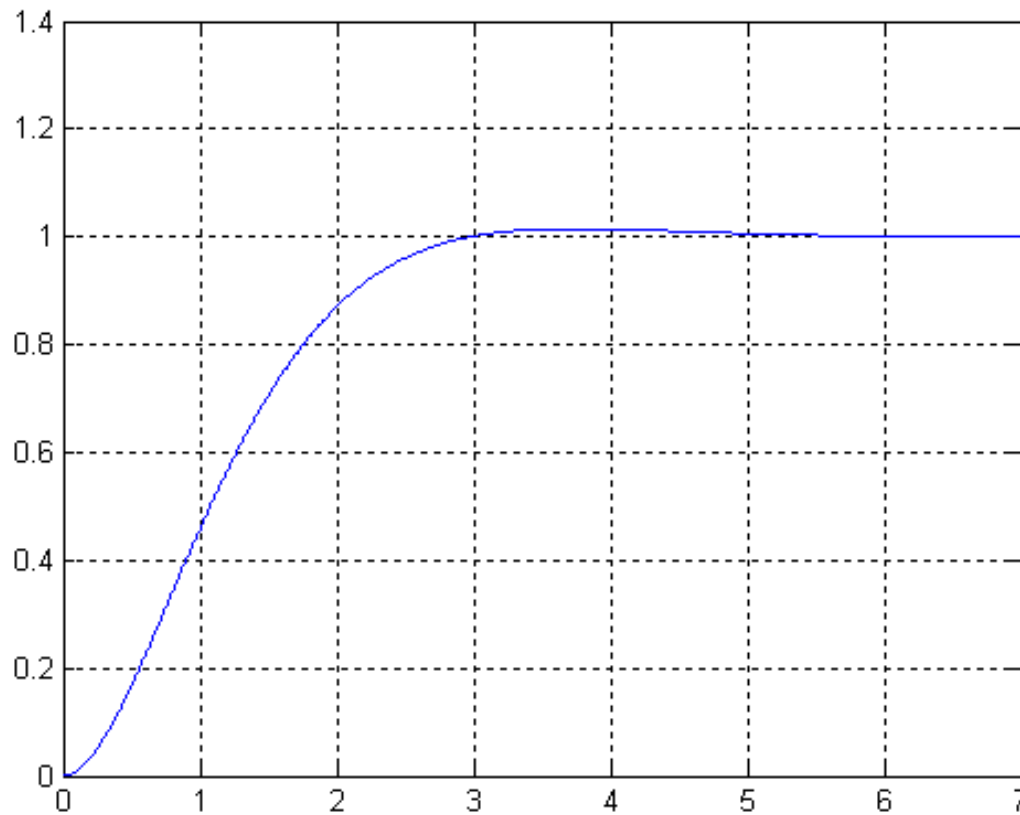
$$\omega_n = 2$$

$$\zeta = 0,72$$

$$\omega_n = 0,8$$



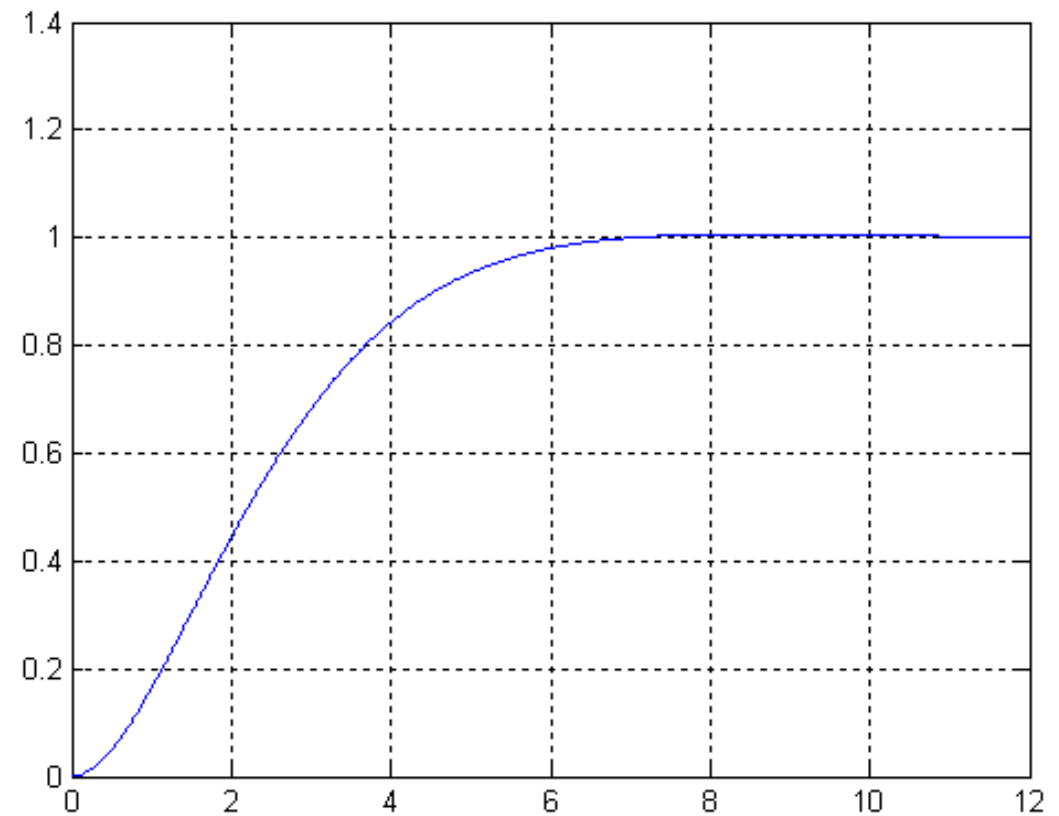
Time domain analysis - 2nd order systems



unit step
response

$$\zeta = 0,8$$
$$\omega_n = 1,4$$

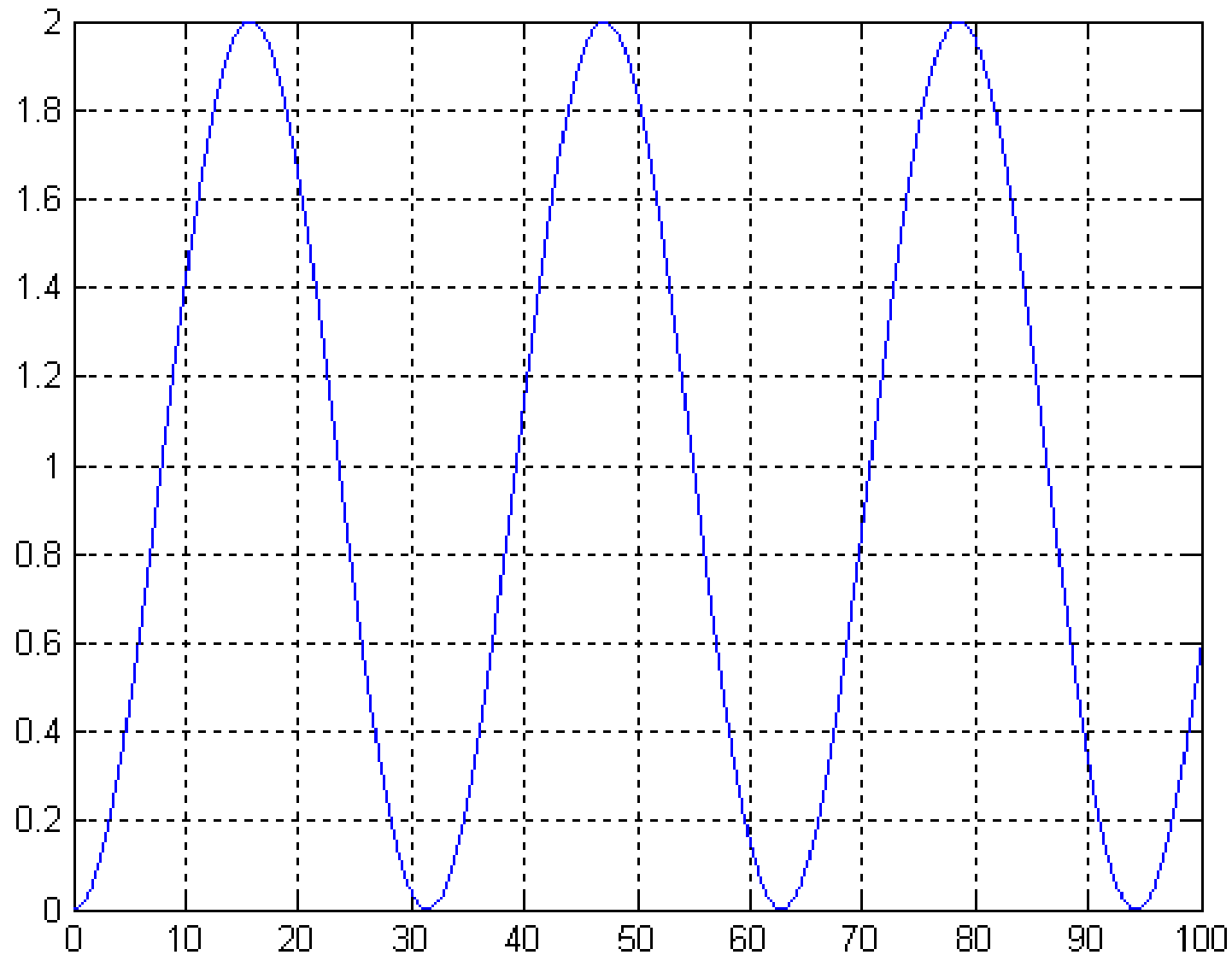
$$\zeta = 0,85$$
$$\omega_n = 0,7$$



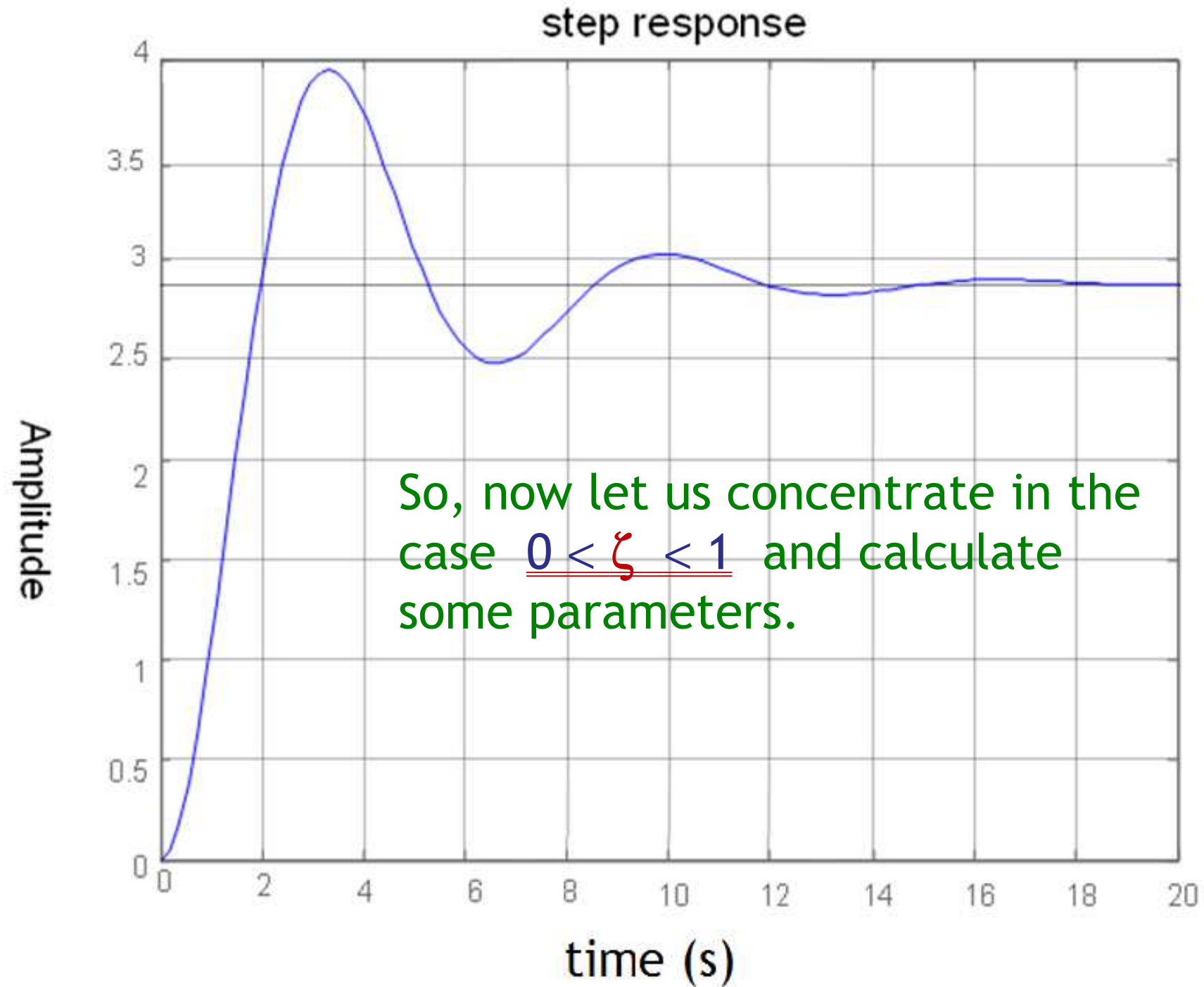
Time domain analysis - 2nd order systems

unit step
response

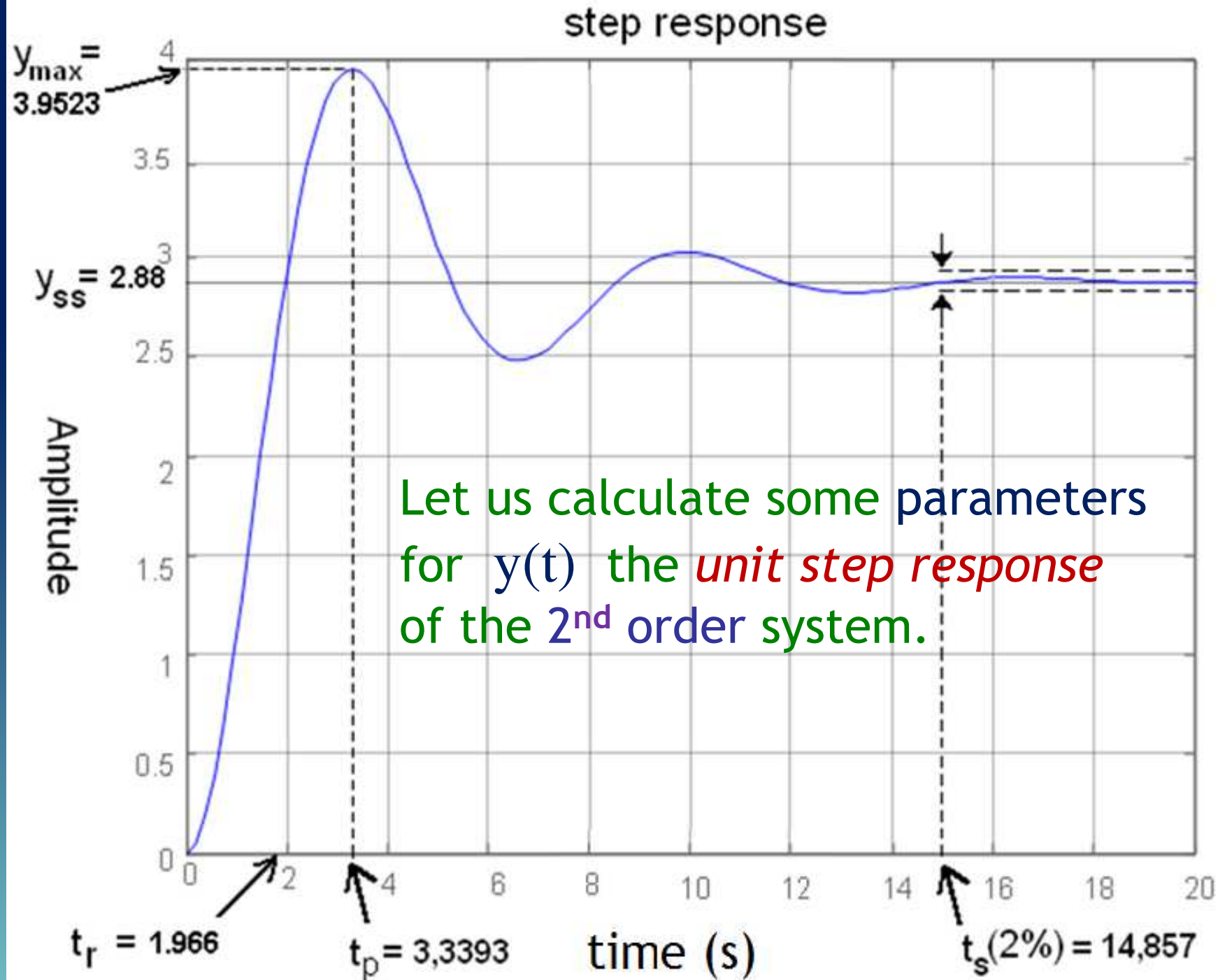
$$\zeta = 0$$
$$\omega_n = 0,2$$



Time domain analysis - 2nd order systems



Time domain analysis - 2nd order systems



steady state output

y_{ss}

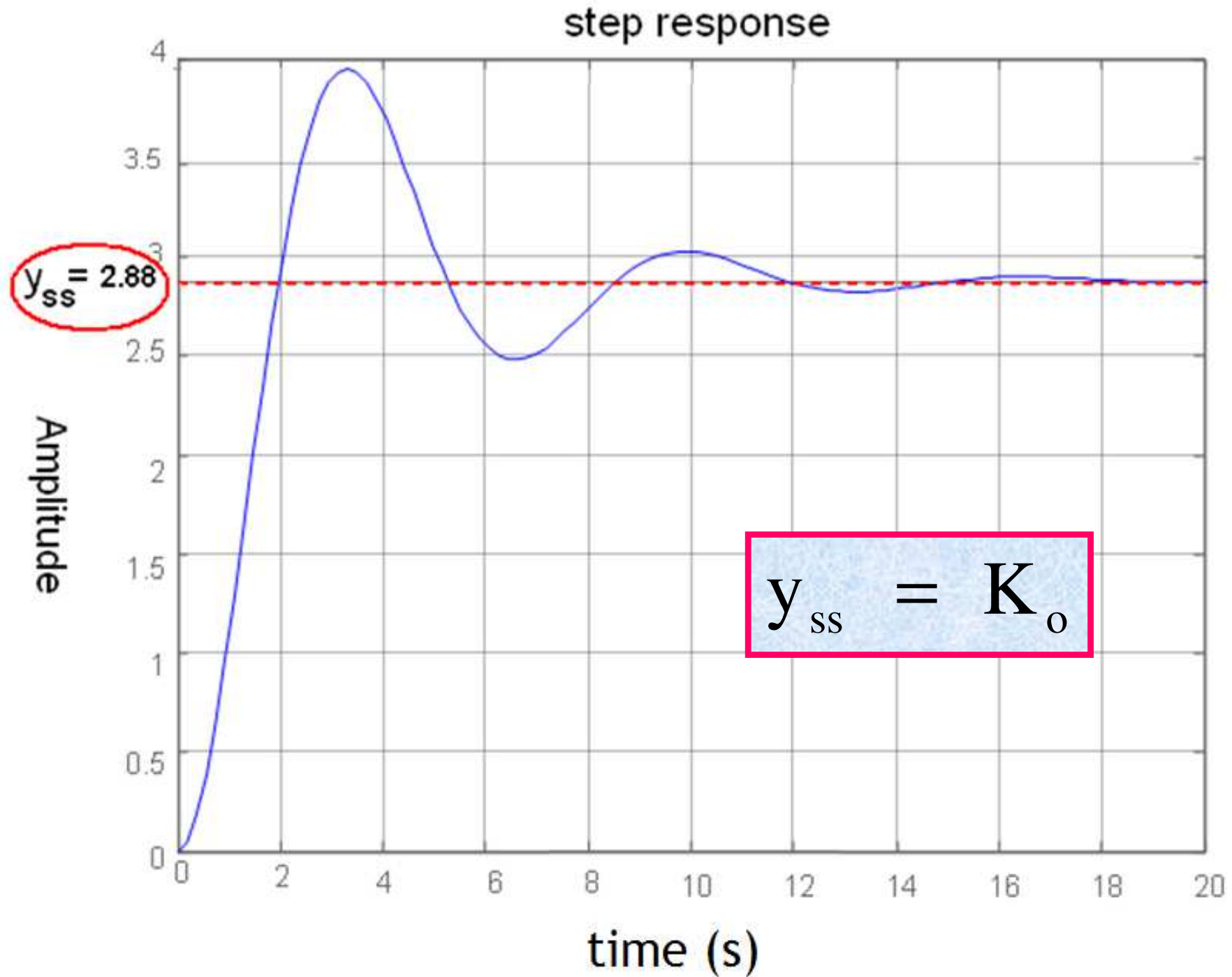
y_{ss} = steady state response
(steady state output)

$$Y(s) = \frac{K_o \omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2} \cdot R(s) \quad \text{with a red arrow pointing to } R(s) = \frac{1}{s}$$

$$\begin{aligned} y_{ss} &= \lim_{t \rightarrow \infty} y(t) = \lim_{s \rightarrow 0} s \cdot Y(s) = \\ &= \lim_{s \rightarrow 0} \frac{K_o \omega_n^2 s}{s^2 + 2\zeta\omega_n s + \omega_n^2} \cdot \frac{1}{s} = \\ &= K_o \end{aligned}$$

$$y_{ss} = K_o$$

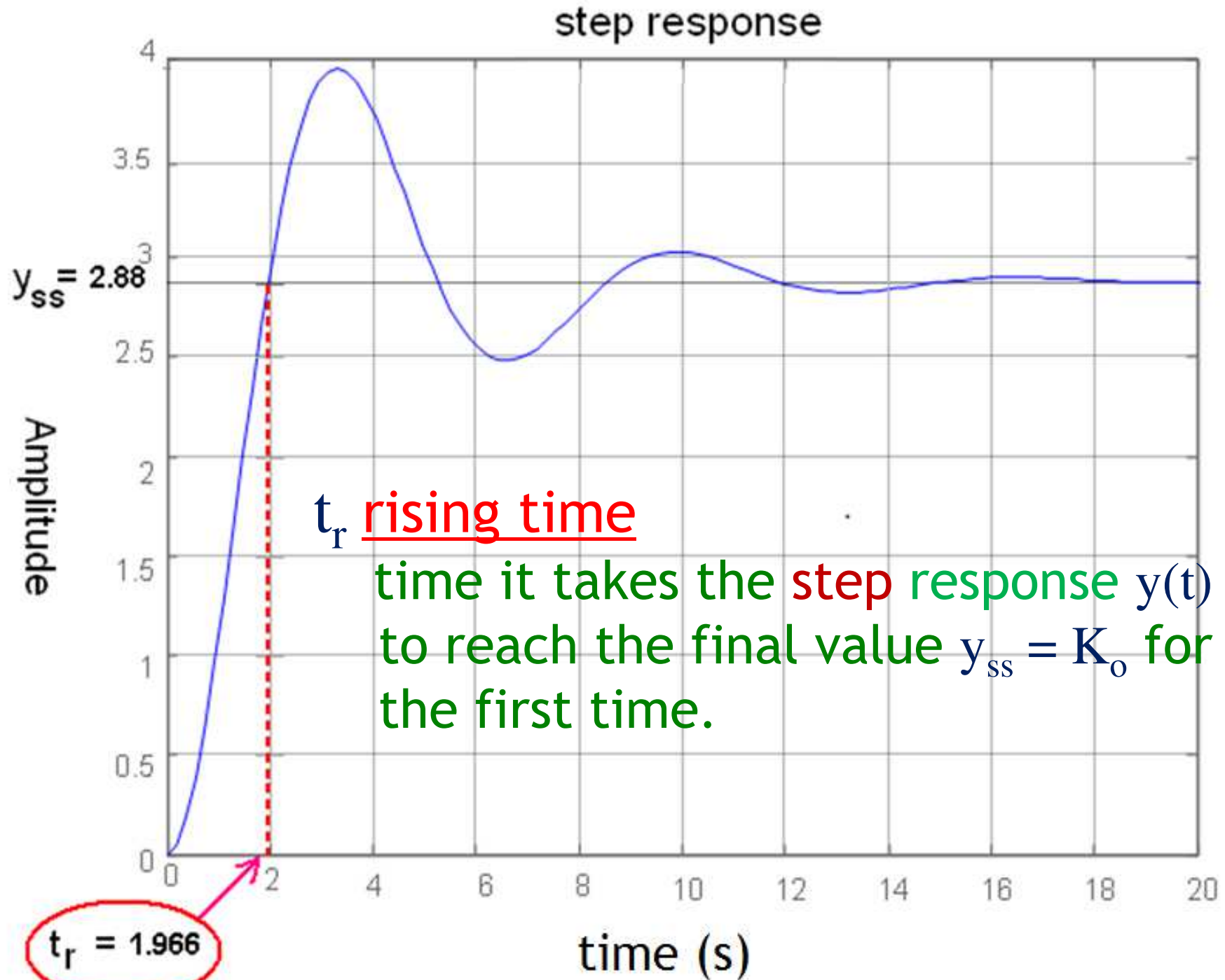
Time domain analysis - 2nd order systems



rising time

t_r

Time domain analysis - 2nd order systems



t_r = rising time

Is the instant of time that $y(t)$ reaches the final value K_o for the first time.

$$y(t_r) = K_o \left[1 - e^{-\zeta \omega_n t_r} \left(\cos \omega_d t_r + \frac{\zeta}{\sqrt{1-\zeta^2}} \cdot \sin \omega_d t_r \right) \right] = K_o$$

$$e^{-\zeta \omega_n t_r} \left(\cos \omega_d t_r + \frac{\zeta}{\sqrt{1-\zeta^2}} \cdot \sin \omega_d t_r \right) = 0$$

$$\operatorname{tg}(\omega_d t_r) = \frac{-\sqrt{1-\zeta^2}}{\zeta} = \frac{-\omega_d}{\zeta \omega_n}$$

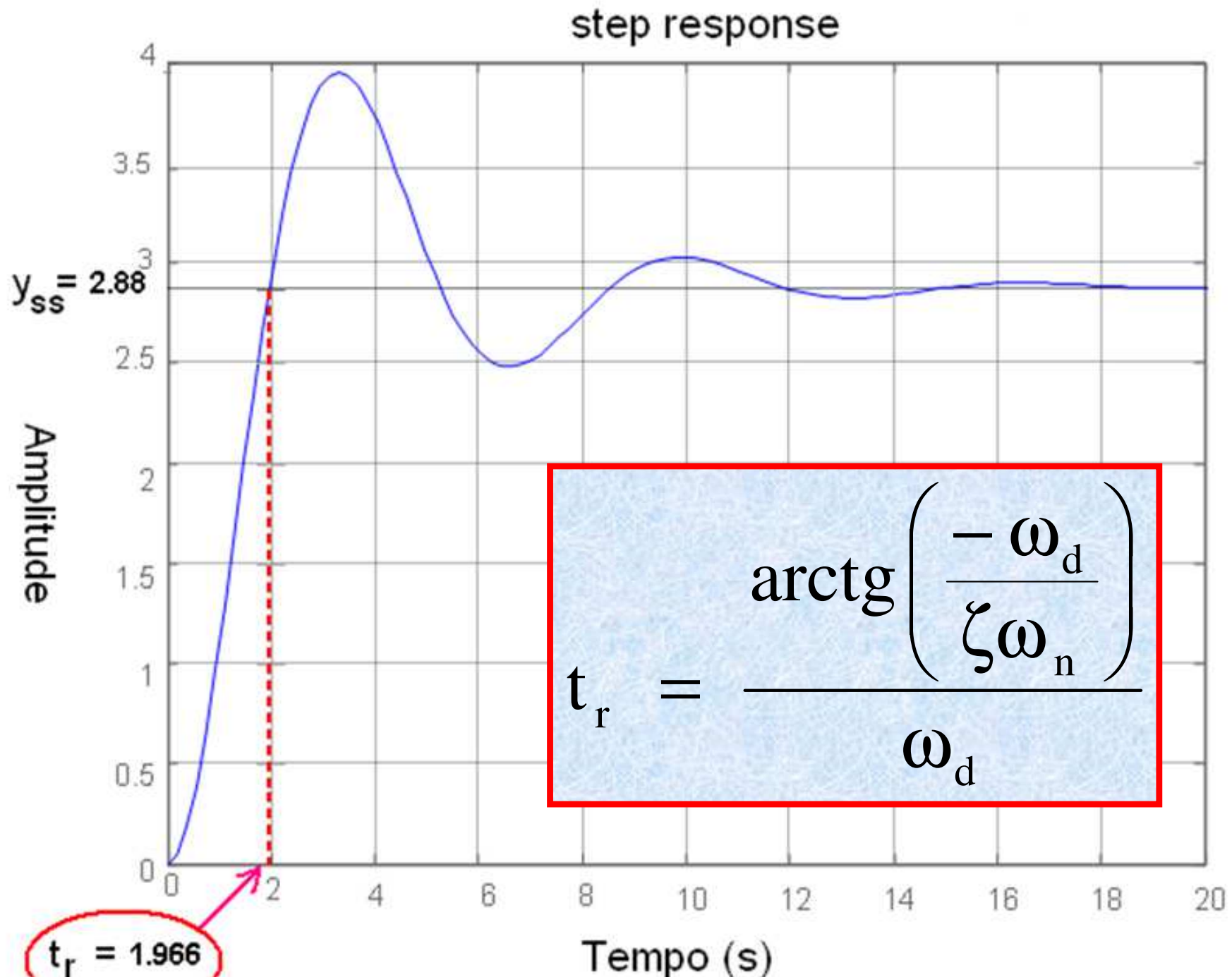
t_r = rising time

Depends on the values of ζ (*damping coefficient*),
and of ω_n (*natural frequency*)

$$t_r = \frac{\arctg\left(\frac{-\omega_d}{\zeta\omega_n}\right)}{\omega_d} = \frac{\arctg\left(\frac{-\sqrt{1-\zeta^2}}{\zeta}\right)}{\omega_d}$$

$$t_r = \arctg(-\omega_d / \zeta\omega_n) / \omega_d$$

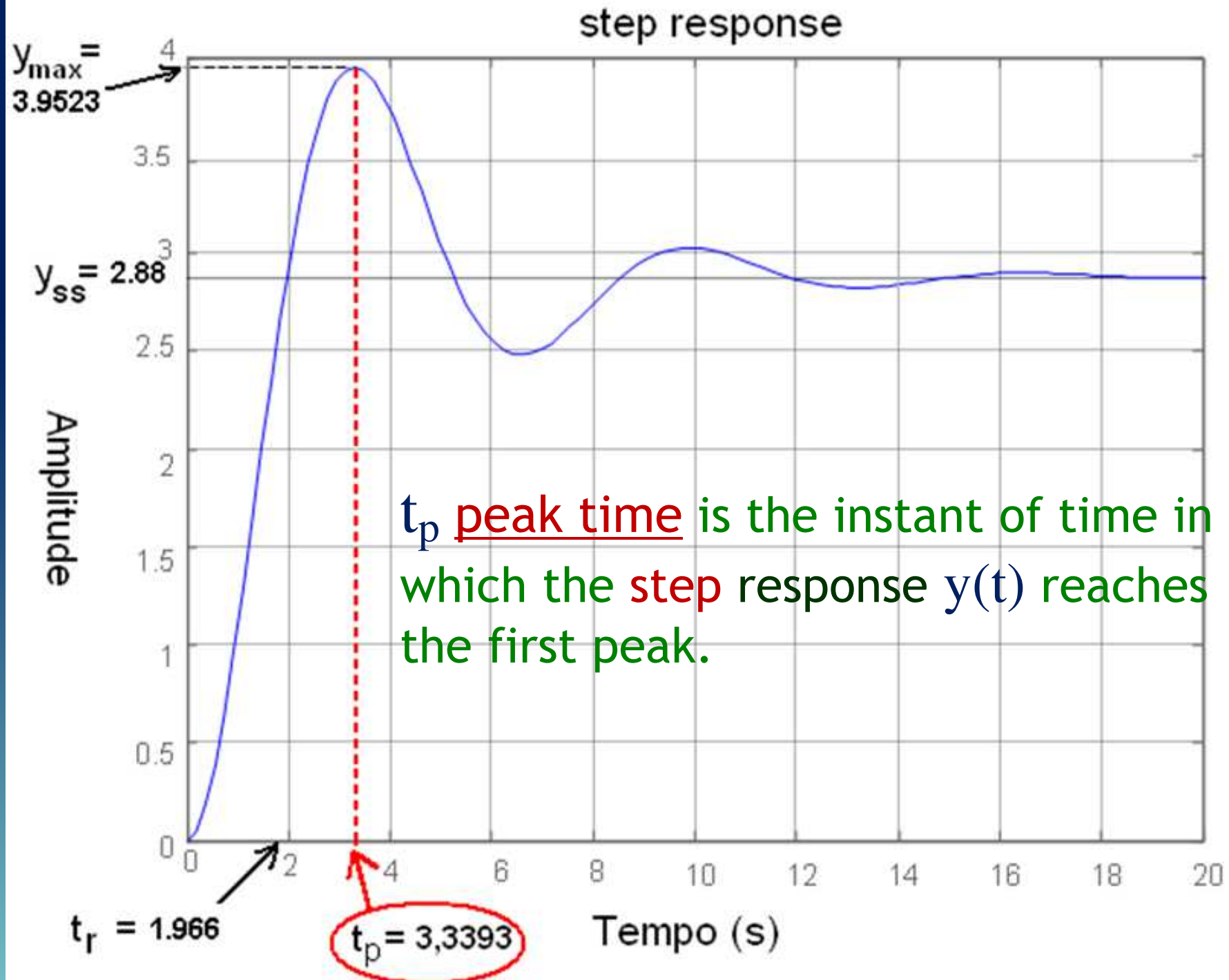
Time domain analysis - 2nd order systems



peak time

t_p

Time domain analysis - 2nd order systems



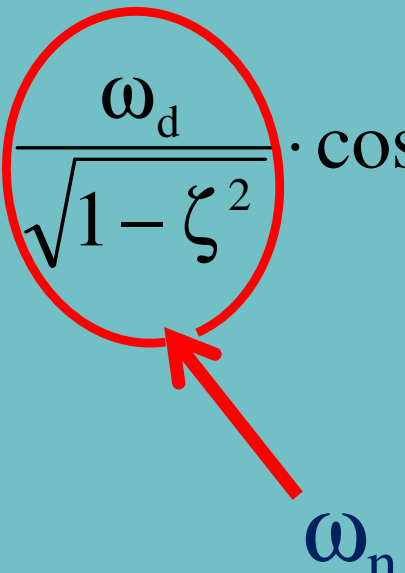
Time domain analysis - 2nd order systems

peak time

$$y_{ss} = K_o \text{ (gain)}$$

ζ (damping coefficient),

ω_n (natural frequency)

$$y' = \frac{dy}{dt} = K_o \left[\zeta \omega_n \cdot e^{-\zeta \omega_n t} \left(\cos \omega_d t_r + \frac{\zeta}{\sqrt{1 - \zeta^2}} \cdot \text{sen } \omega_d t_r \right) + \right. \\ \left. - e^{-\zeta \omega_n t} \left(-\omega_d \text{sen } \omega_d t_r + \zeta \frac{\omega_d}{\sqrt{1 - \zeta^2}} \cdot \cos \omega_d t_r \right) \right]$$


peak time

$$\begin{aligned}
 \frac{dy}{dt} &= K_o \cdot e^{-\zeta \omega_n t} \left(\cancel{\zeta \omega_n \cos \omega_d t} + \frac{\zeta^2 \omega_n}{\sqrt{1 - \zeta^2}} \cdot \text{sen } \omega_d t + \right. \\
 &\quad \left. + \omega_d \text{sen } \omega_d t - \cancel{\zeta \omega_n \cdot \cos \omega_d t} \right) \\
 &= K_o \cdot e^{-\zeta \omega_n t} \cdot \text{sen } \omega_d t \cdot \left(\frac{\zeta^2 \omega_n}{\sqrt{1 - \zeta^2}} + \frac{\omega_n (1 - \zeta^2)}{\sqrt{1 - \zeta^2}} \right) \\
 &= \cancel{K_o} \cdot \cancel{e^{-\zeta \omega_n t}} \cdot \text{sen } \omega_d t \cdot \frac{\cancel{\omega_n}}{\cancel{\sqrt{1 - \zeta^2}}} = 0
 \end{aligned}$$

peak time

$$\frac{dy}{dt} = 0$$



$$\sin \omega_d t = 0$$



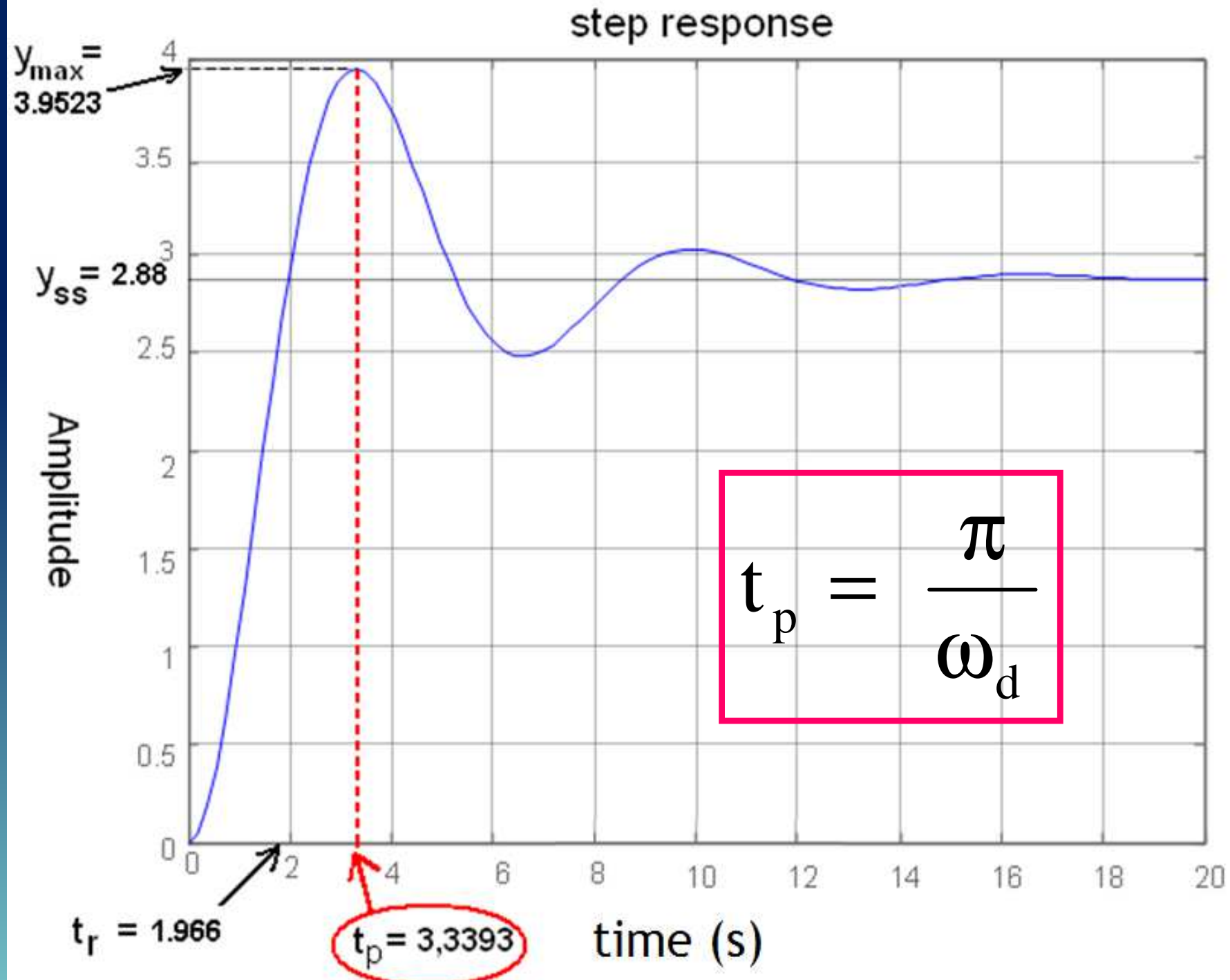
$$\omega_d t = 0, \pi, 2\pi, 3\pi, \dots$$



$$t_p = \frac{\pi}{\omega_d}$$

$$t_p = \pi / \omega_d$$

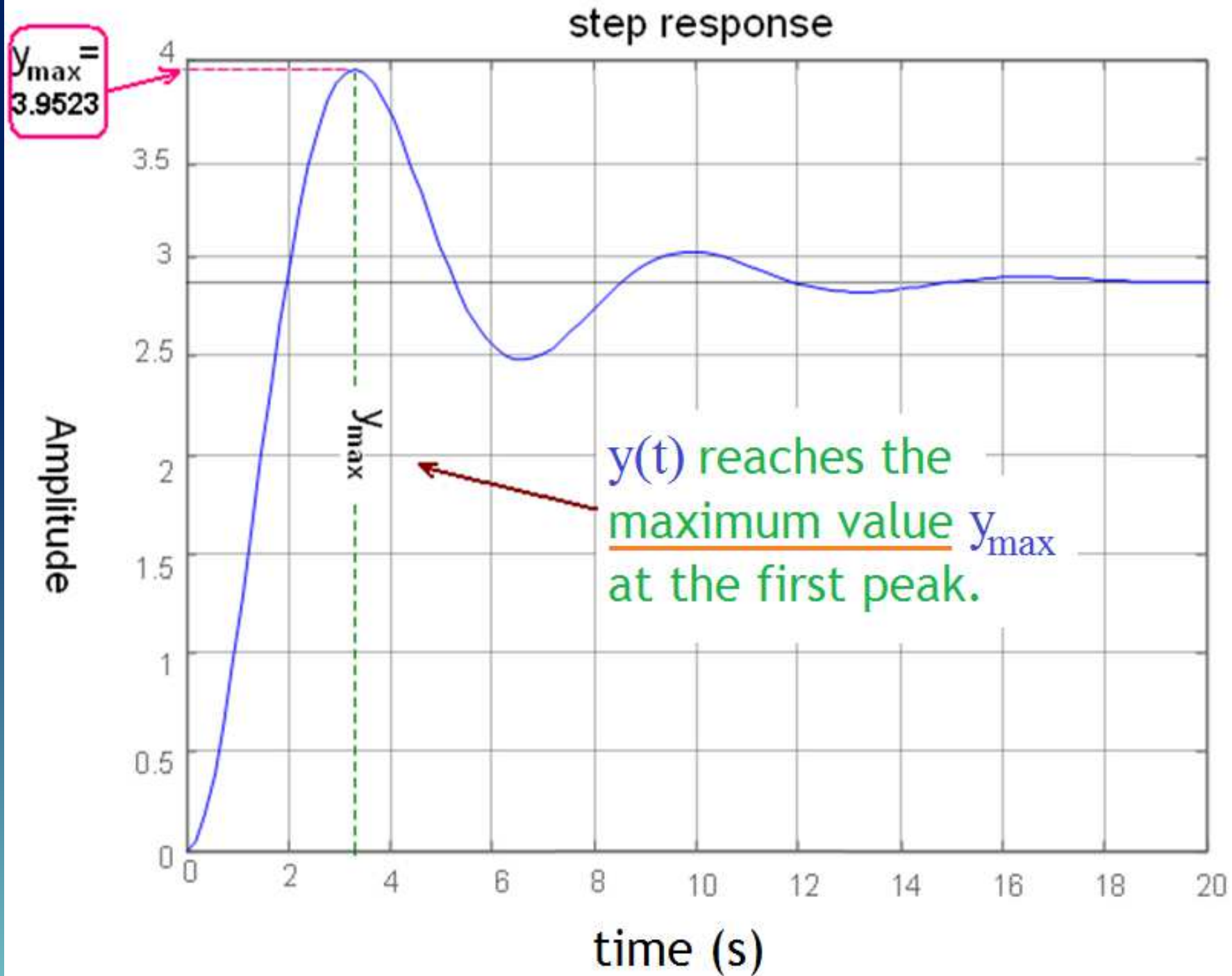
Time domain analysis - 2nd order systems



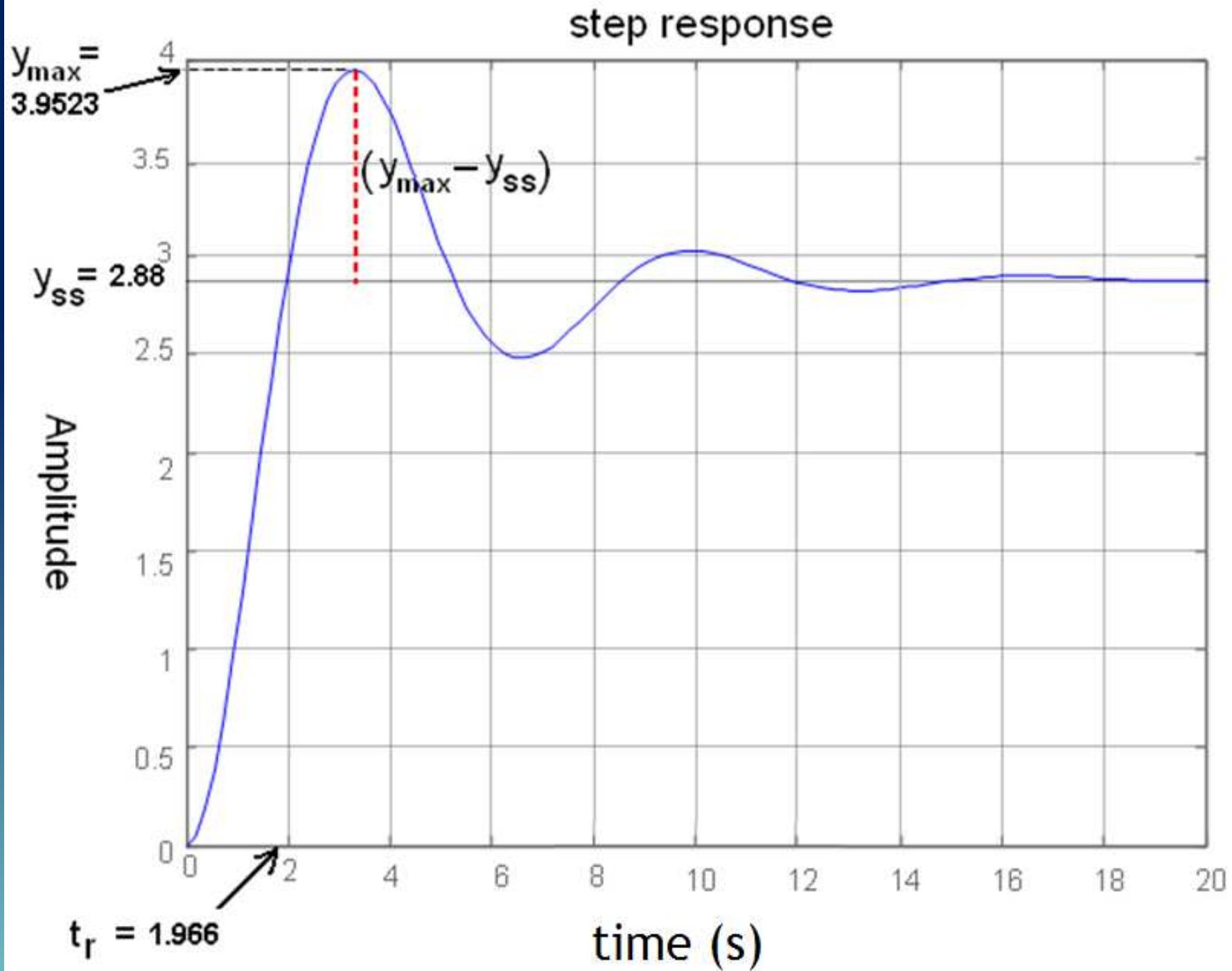
overshoot

M_p

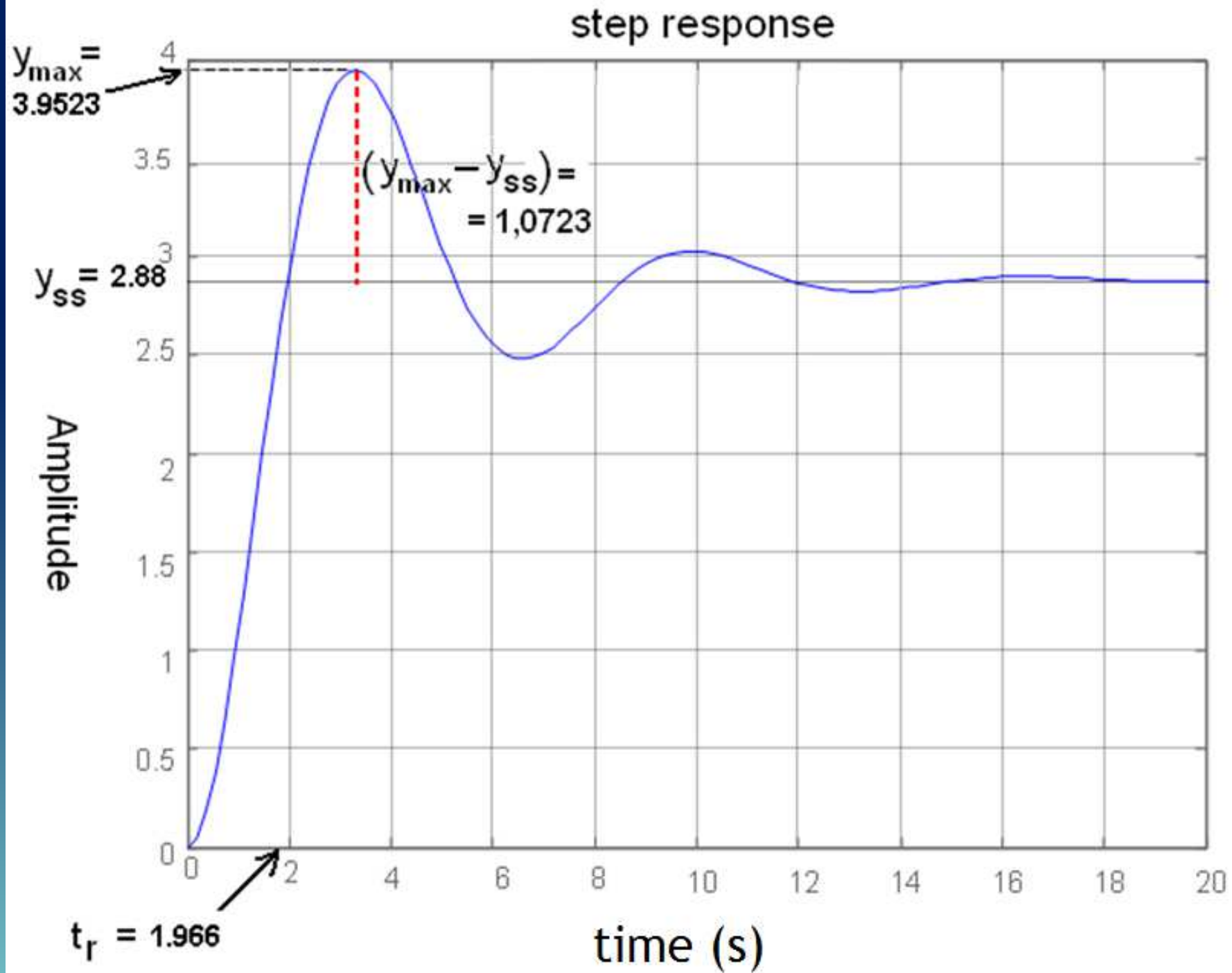
Time domain analysis - 2nd order systems



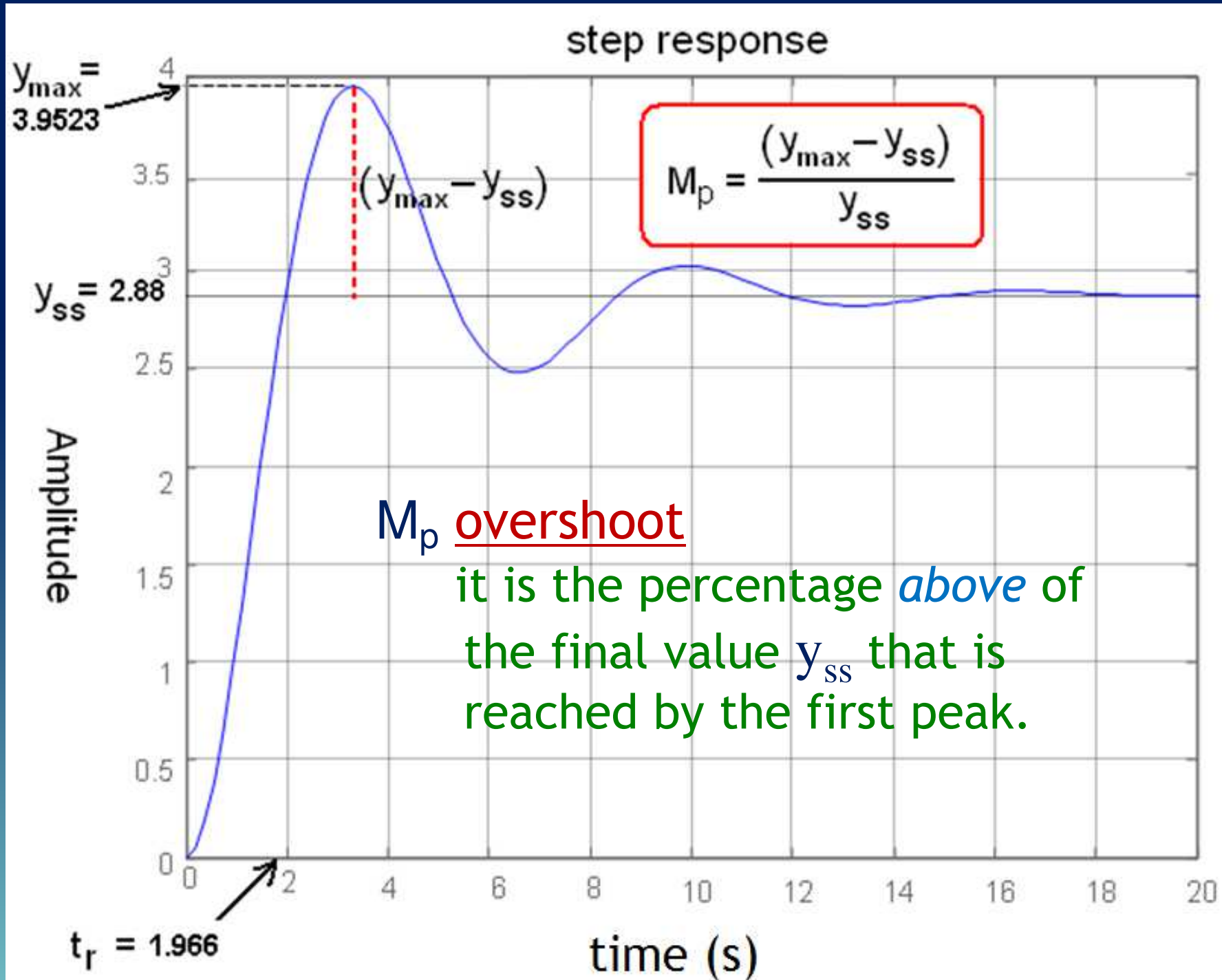
Time domain analysis - 2nd order systems



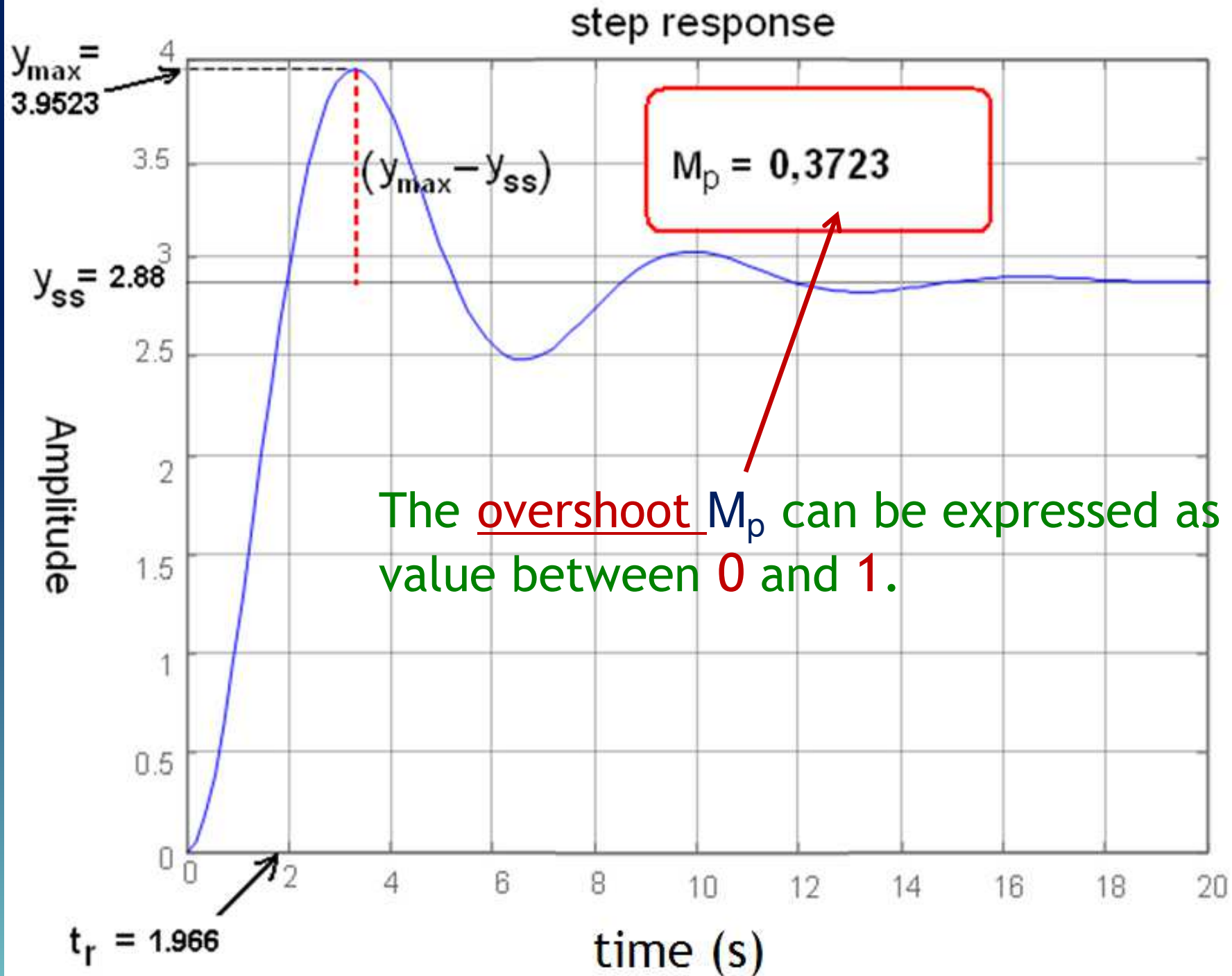
Time domain analysis - 2nd order systems



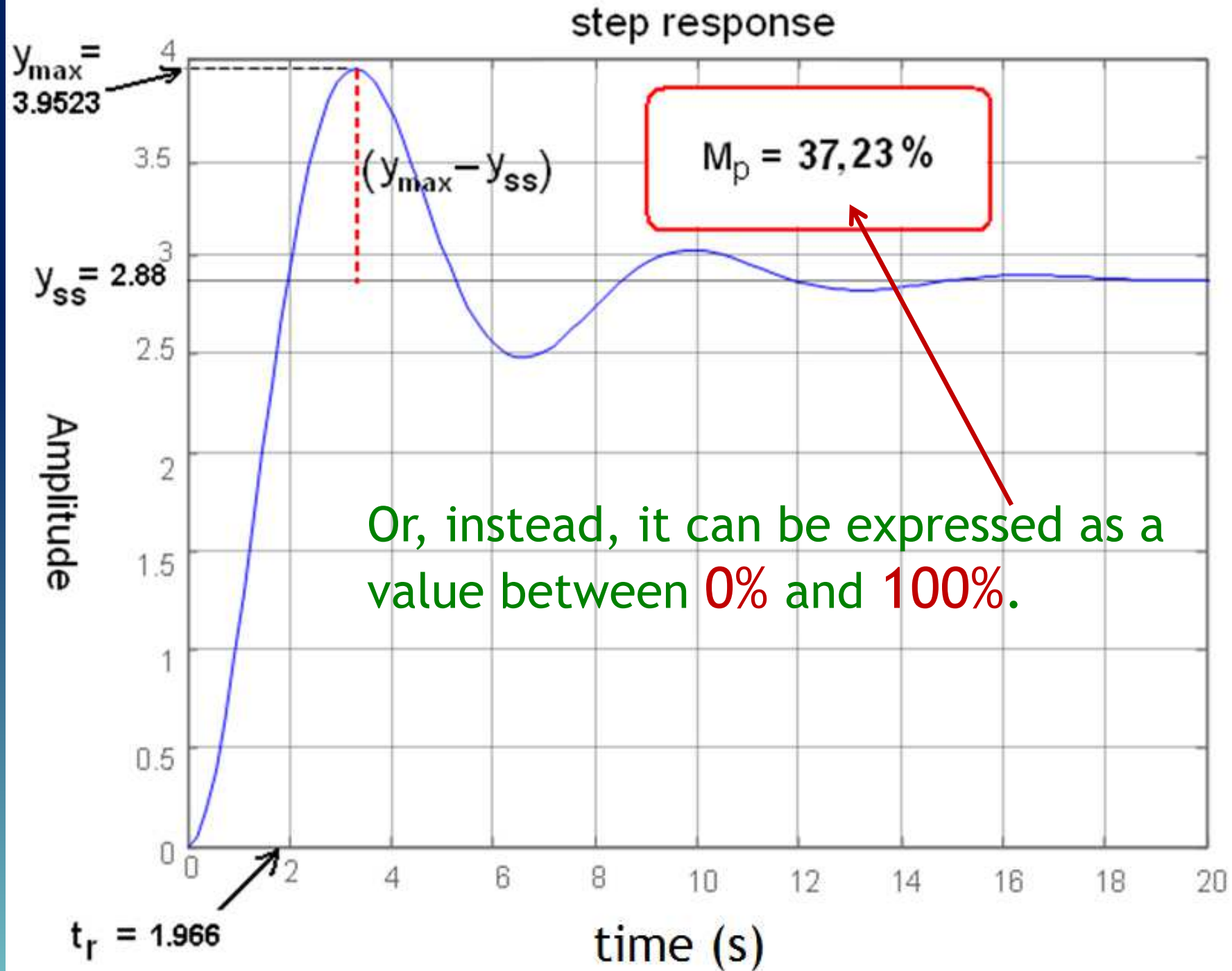
Time domain analysis - 2nd order systems



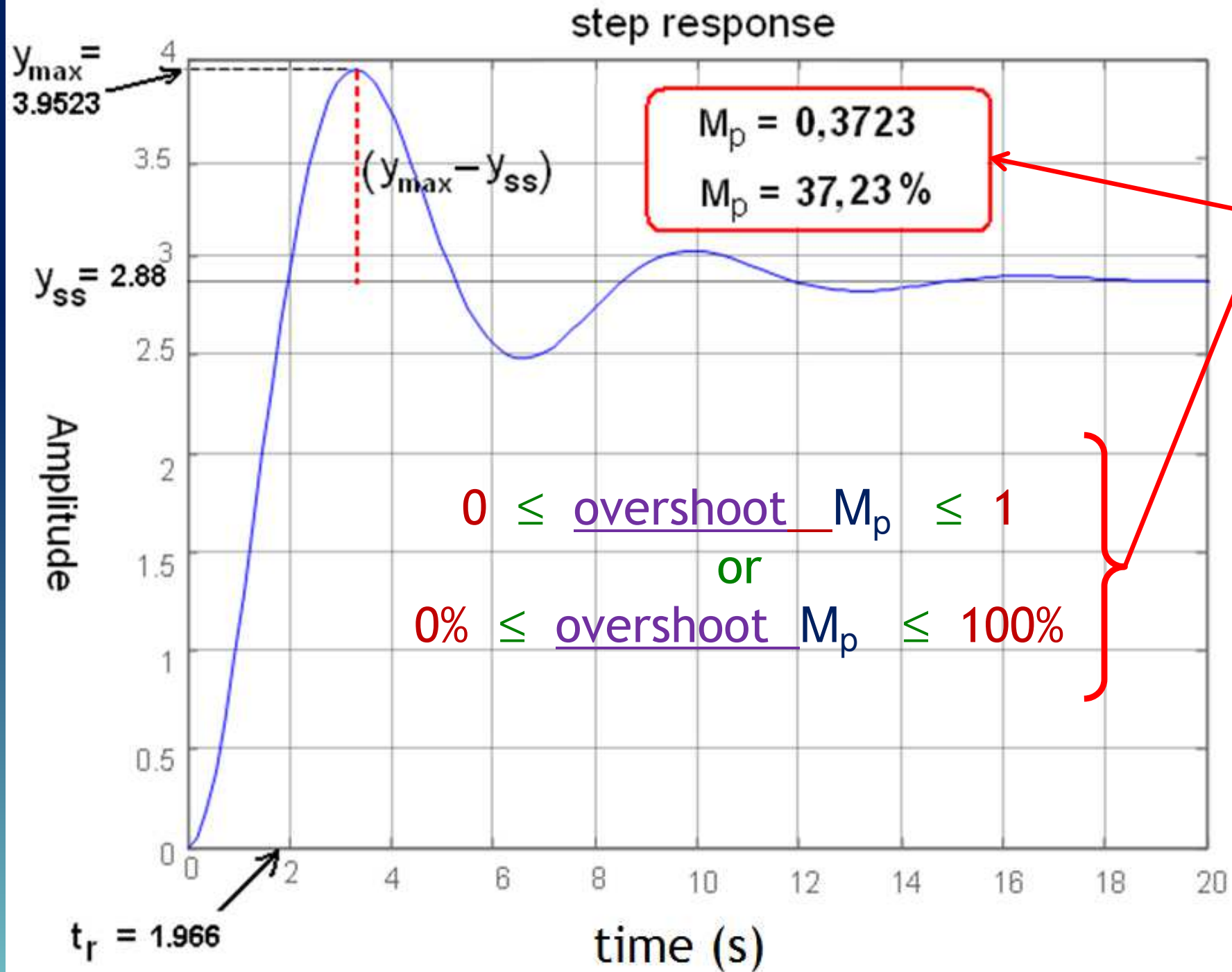
Time domain analysis - 2nd order systems



Time domain analysis - 2nd order systems



Time domain analysis - 2nd order systems



overshoot

$$y_{ss} = K_o \text{ (gain)}$$

$$\zeta \text{ (damping coefficient),}$$

$$\omega_n \text{ (natural frequency)}$$

$$M_p = \frac{y_{\max} - y_{ss}}{y_{ss}} \quad \text{ou} \quad M_p = \frac{y(t_p) - K_o}{K_o}$$

$$M_p = \frac{K_o \left[1 - e^{-\zeta \omega_n t_p} \left(\overbrace{\cos(\pi)}^{-1} - \frac{\zeta}{\sqrt{1-\zeta^2}} \overbrace{\sin(\pi)}^0 \right) \right] - K_o}{K_o}$$

$$M_p = \frac{\cancel{K_o} + K_o e^{-\zeta \omega_n (\pi / \omega_d)} - \cancel{K_o}}{K_o}$$

overshoot

$$M_p = \frac{K_o e^{\frac{-\zeta \pi}{\sqrt{1 - \zeta^2}}}}{K_o}$$


$$M_p = e^{\frac{-\zeta \pi}{\sqrt{1 - \zeta^2}}}$$

M_p depends only on ζ (*damping coefficient*)

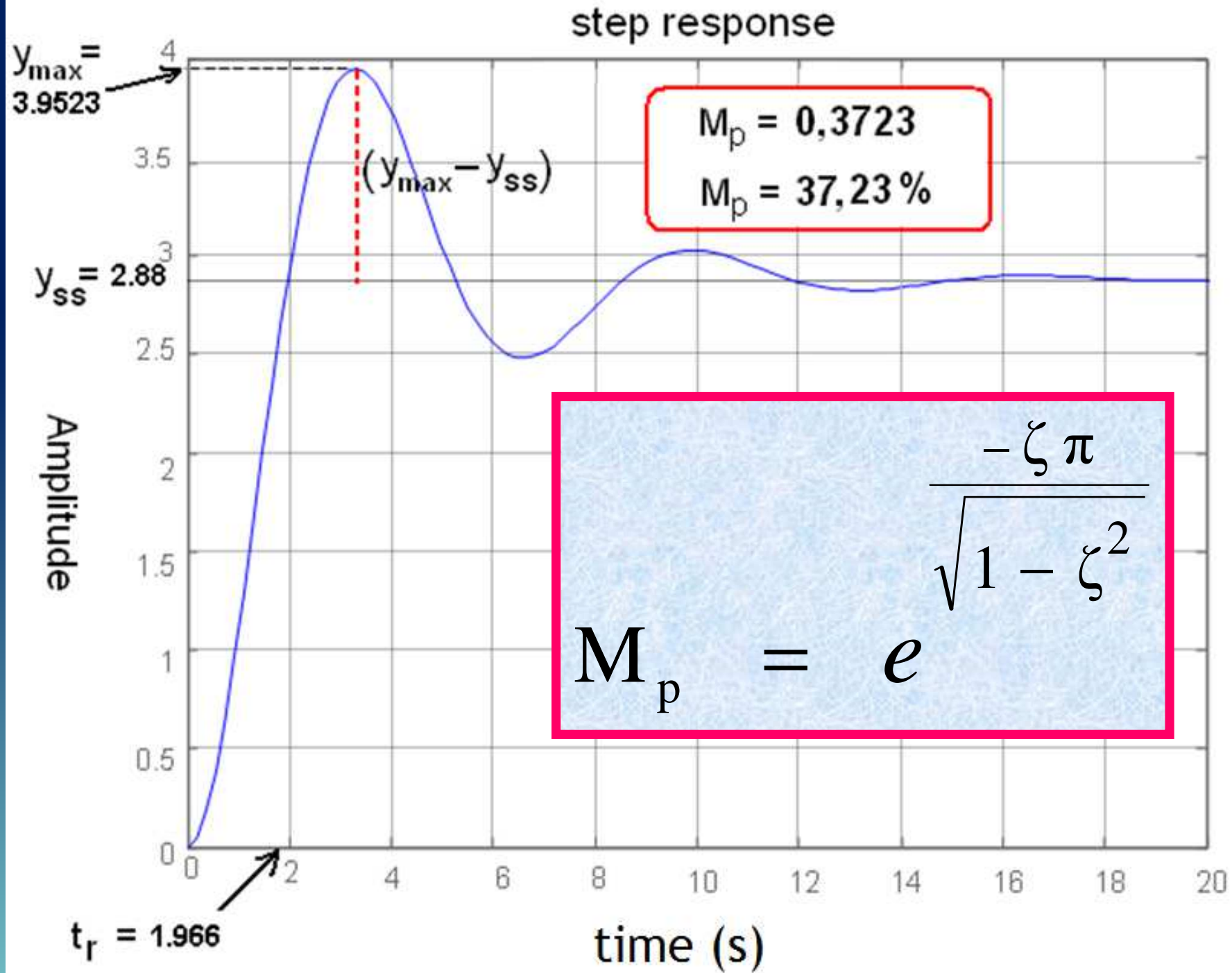
overshoot

M_p depends only on ζ (*damping coefficient*)

$$M_p = e^{\frac{-\zeta \pi}{\sqrt{1 - \zeta^2}}} \quad \text{or}$$

$$M_p = e^{\frac{-\zeta \pi}{\sqrt{1 - \zeta^2}}} \times 100\%$$

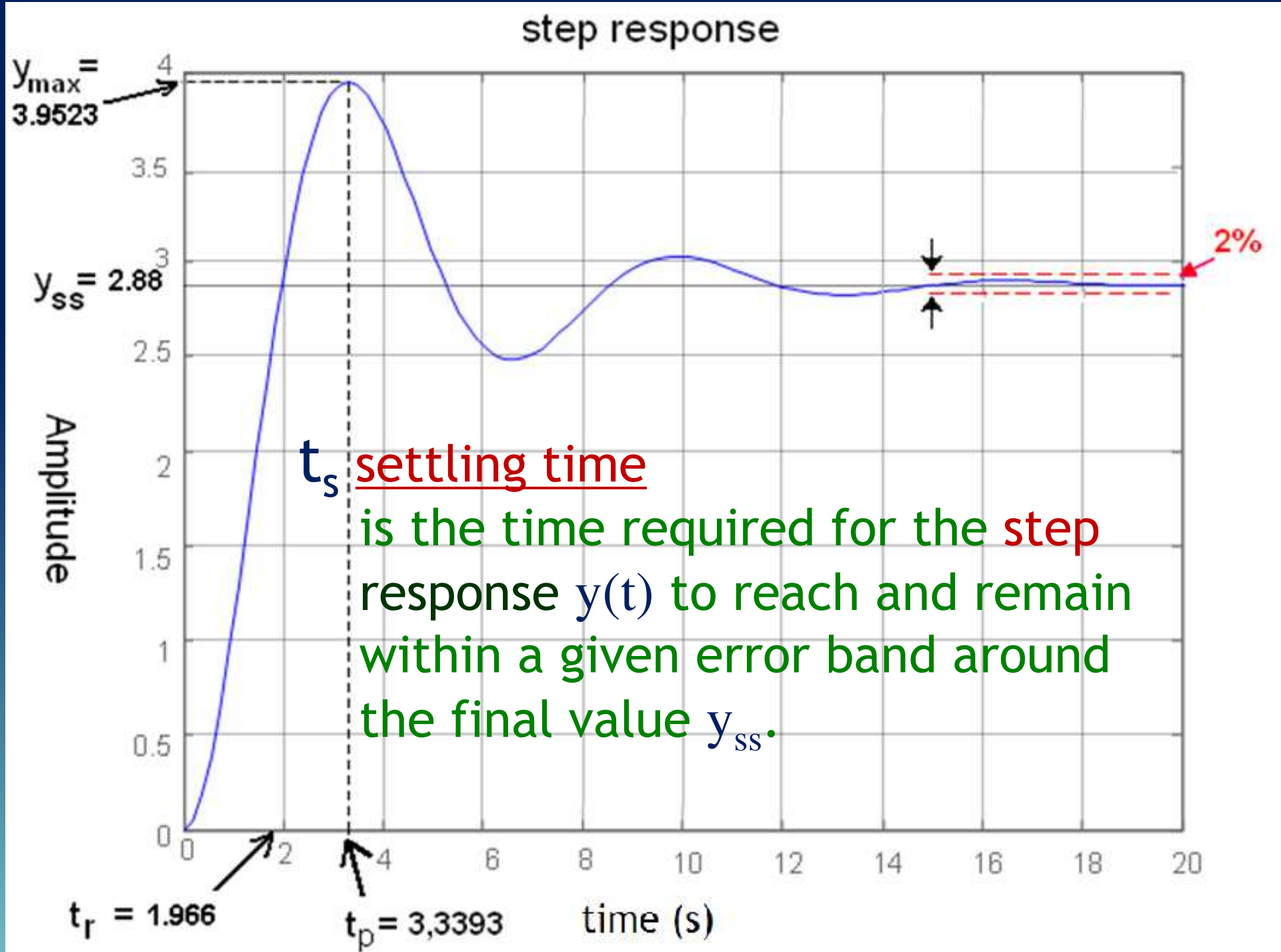
Time domain analysis - 2nd order systems



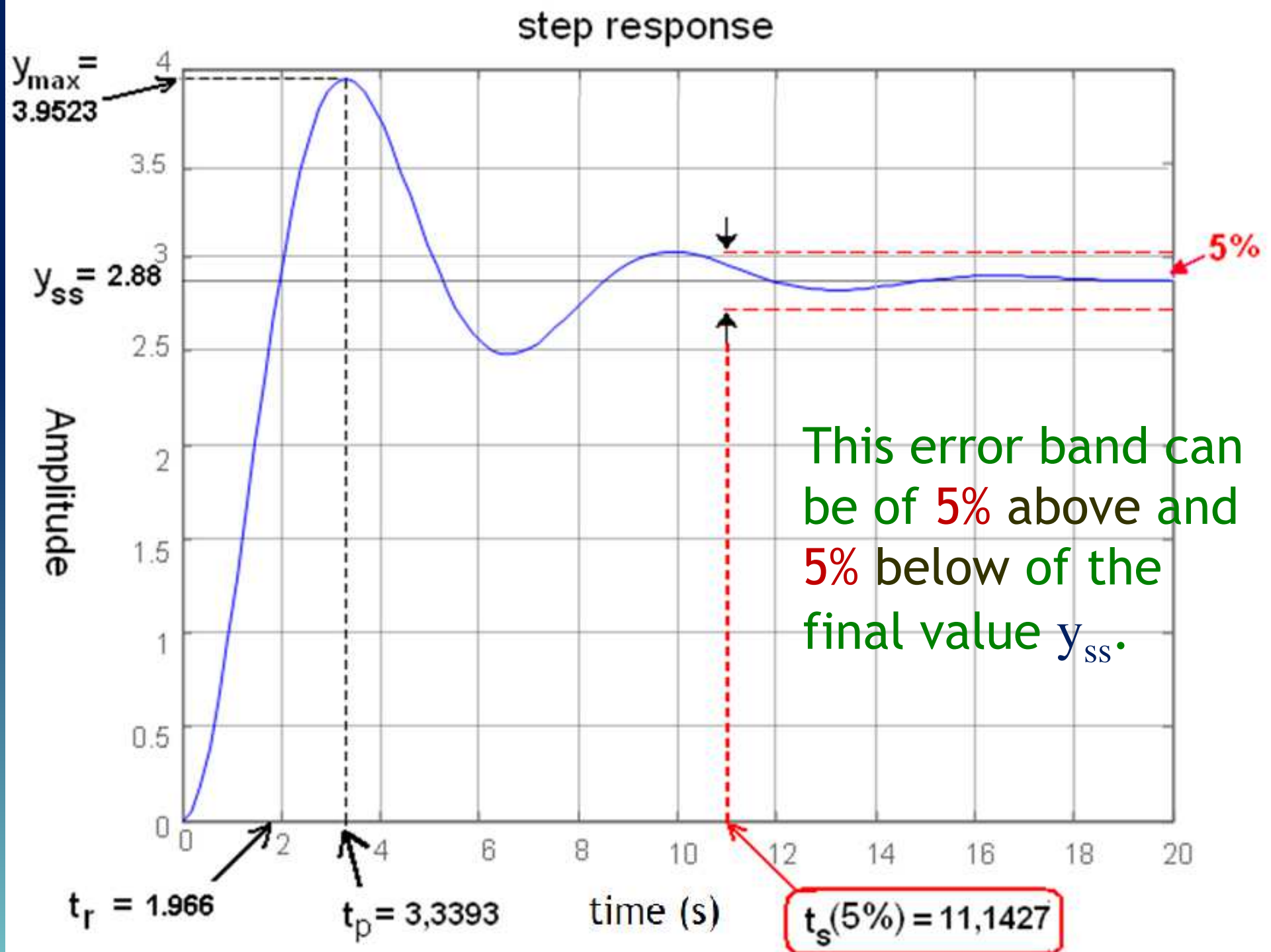
settling time

t_s

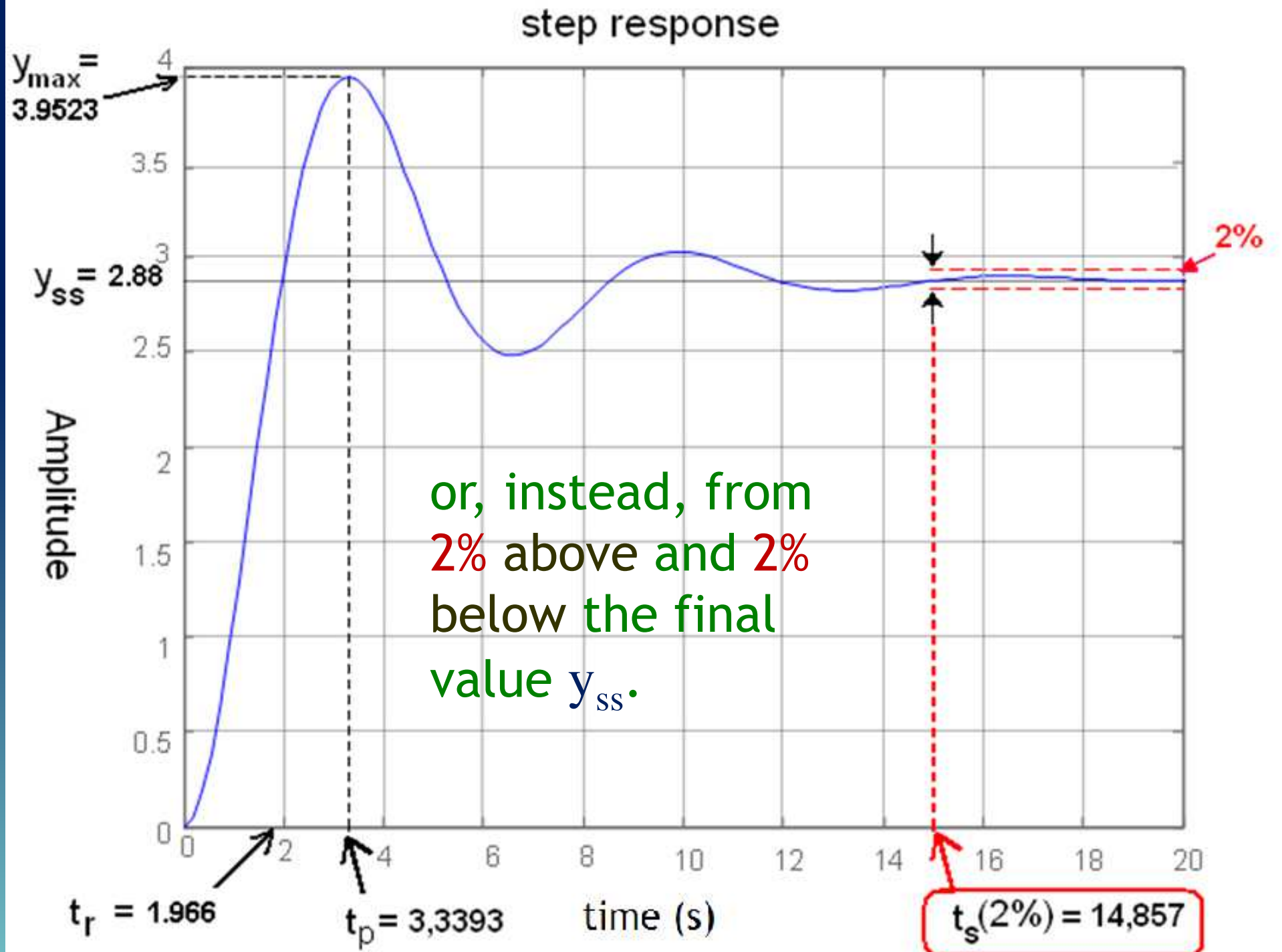
Time domain analysis - 2nd order systems



Time domain analysis - 2nd order systems

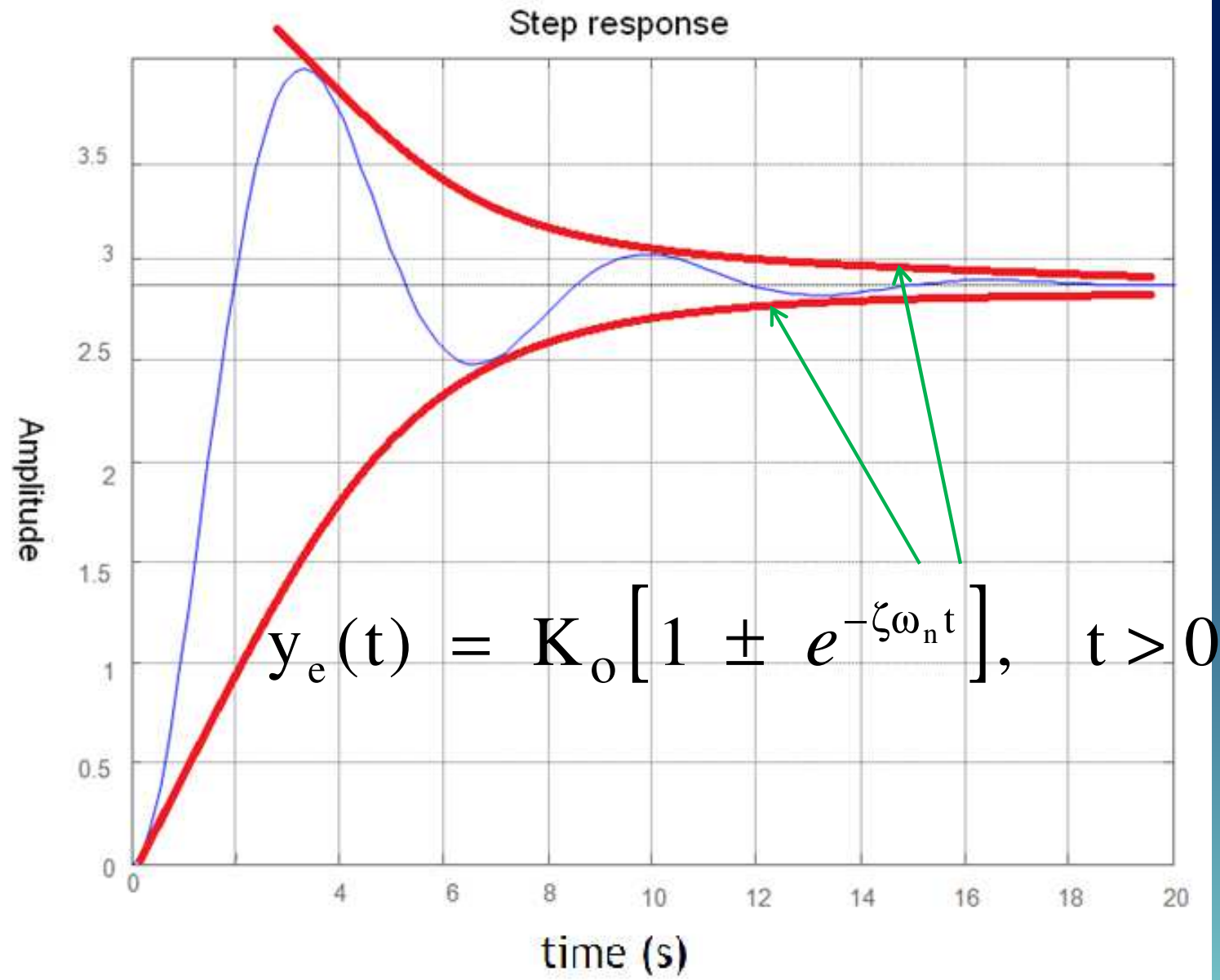


Time domain analysis - 2nd order systems



Time domain analysis - 2nd order systems

The settling time is obtained from the equations of $y_e(t)$, the curves that encompass $y(t)$.



That is, the *settling time* t_s is obtained by calculating

$$y_e(t_s) \approx 1,05 K_o$$

for the case of t_s with 5% tolerance, and

$$y_e(t_s) \approx 1,02 K_o$$

for the case of t_s with 2% tolerance,

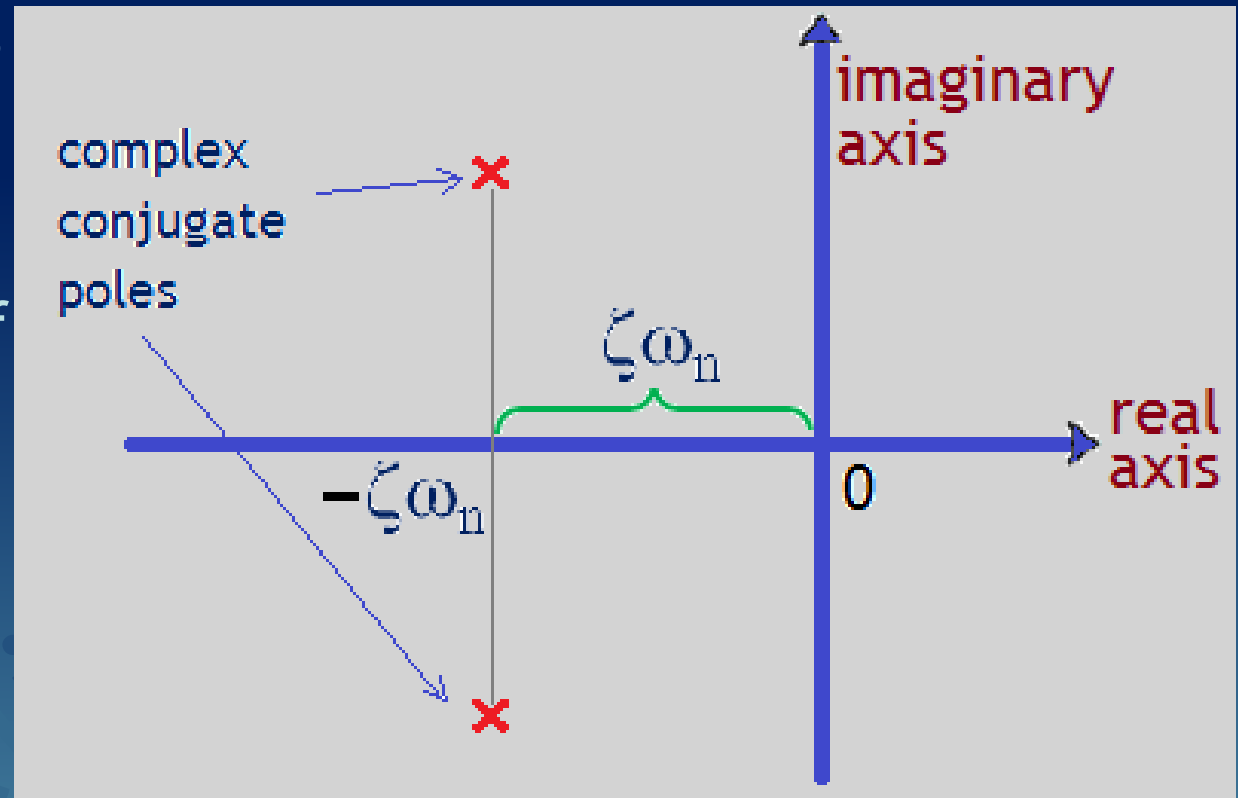
obtaining the following values:

$$t_s(5\%) = \frac{3}{\zeta\omega_n}$$

$$t_s(2\%) = \frac{4}{\zeta\omega_n}$$

settling time

Note that the settling time t_r is inversely proportional to $\zeta\omega_n$, which is the distance of the real part of the poles to the origin.



hence:

$$t_s(5\%) = \frac{3}{\zeta\omega_n}$$

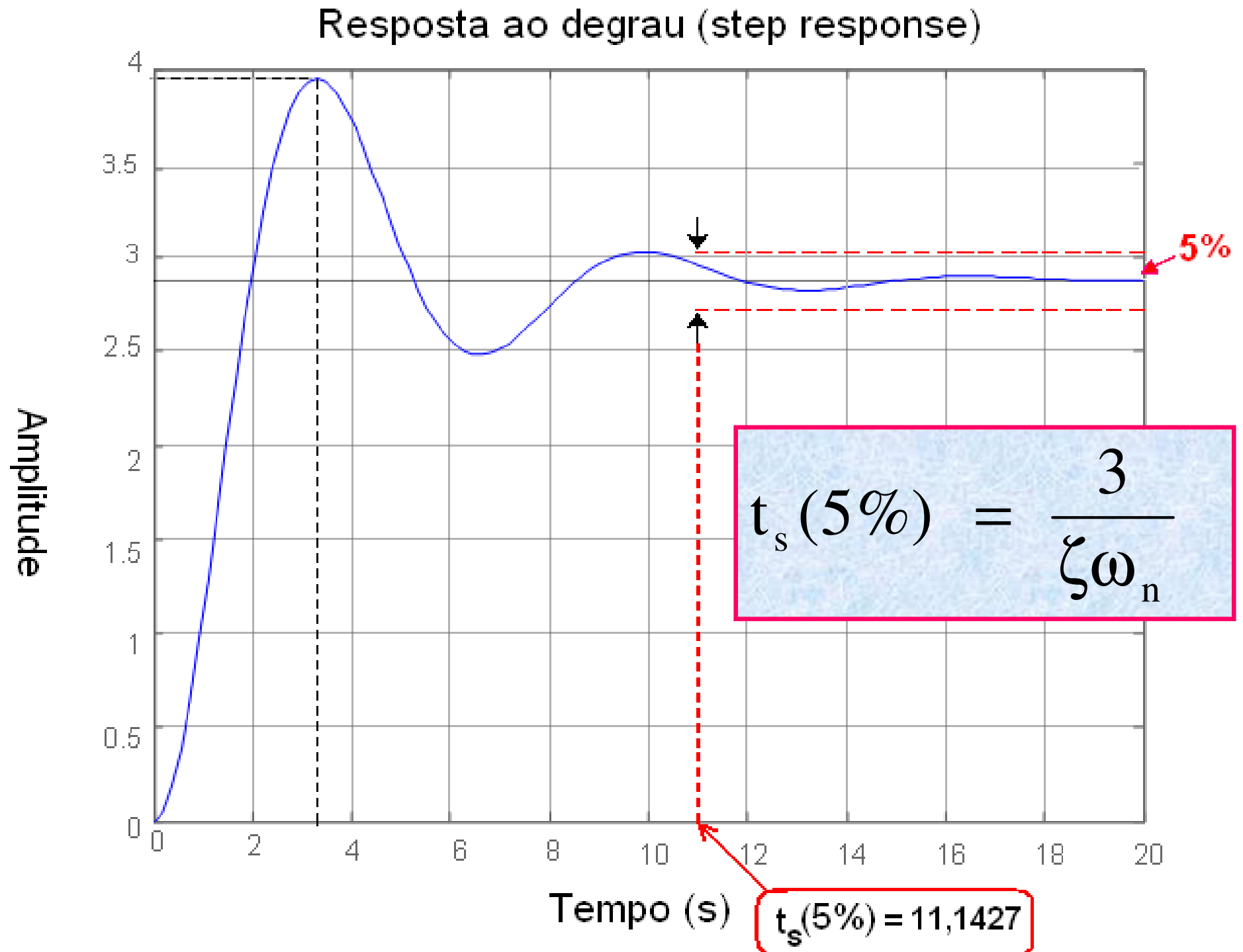
and

$$t_s(2\%) = \frac{4}{\zeta\omega_n}$$

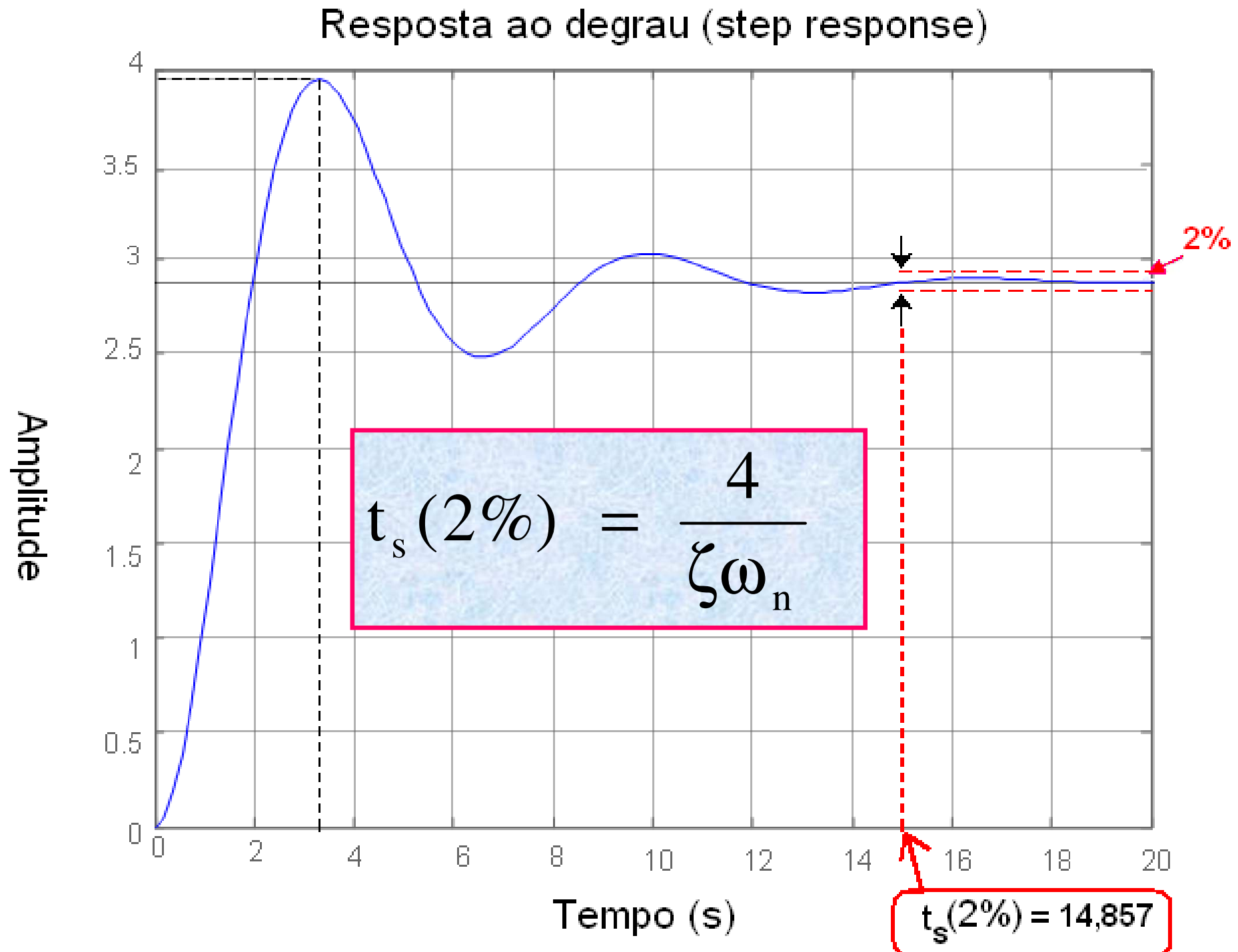
$$t_s(5\%) = 3 / \zeta\omega_n$$

$$t_s(2\%) = 4 / \zeta\omega_n$$

Time domain analysis - 2nd order systems



Time domain analysis - 2nd order systems



Note that we have seen cases in which

$$0 < \zeta < 1$$

$$\zeta = 1$$

$$\zeta > 1$$

that is:

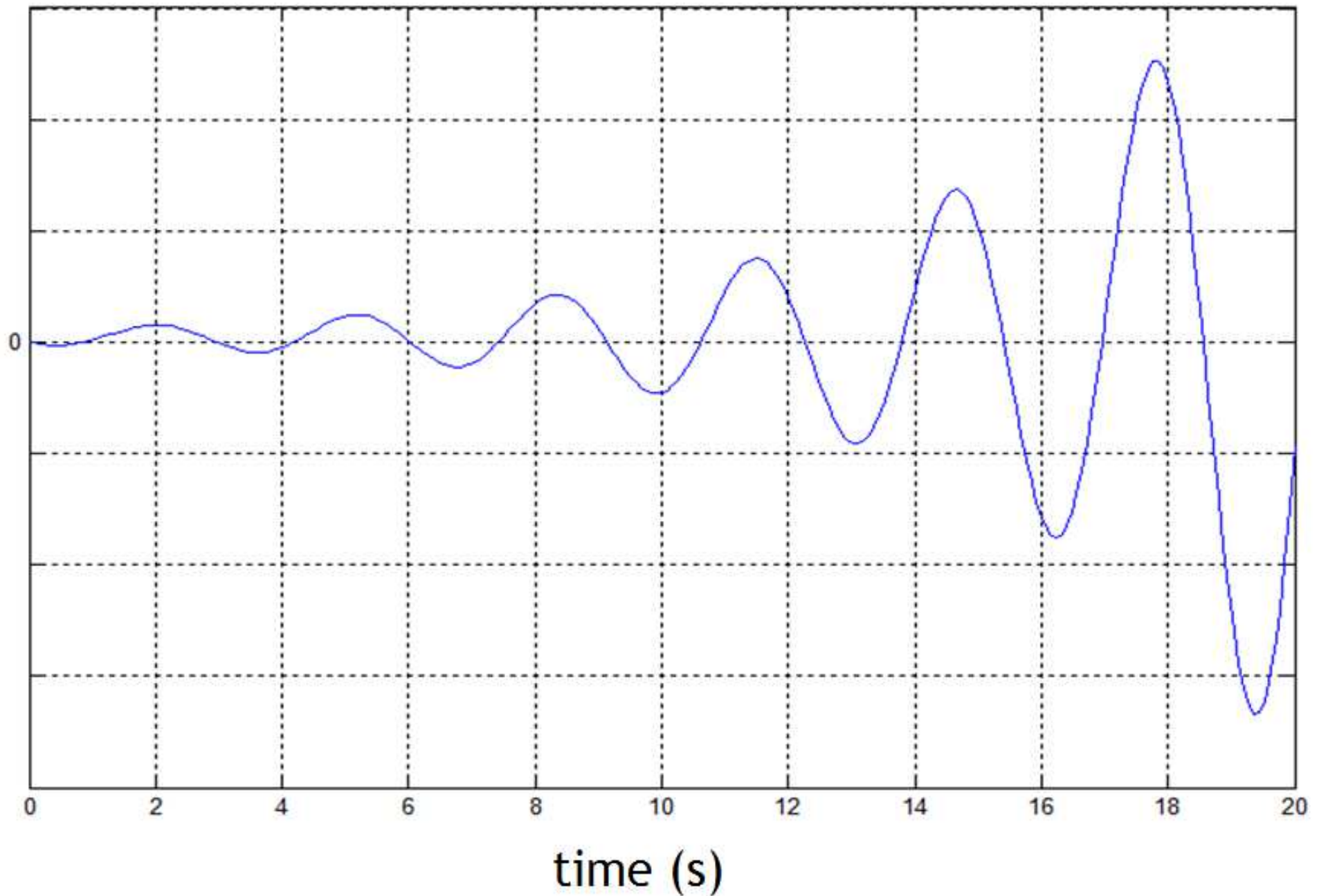
$$\zeta > 0$$

However, if $\zeta < 0$ then:

the system is unstable

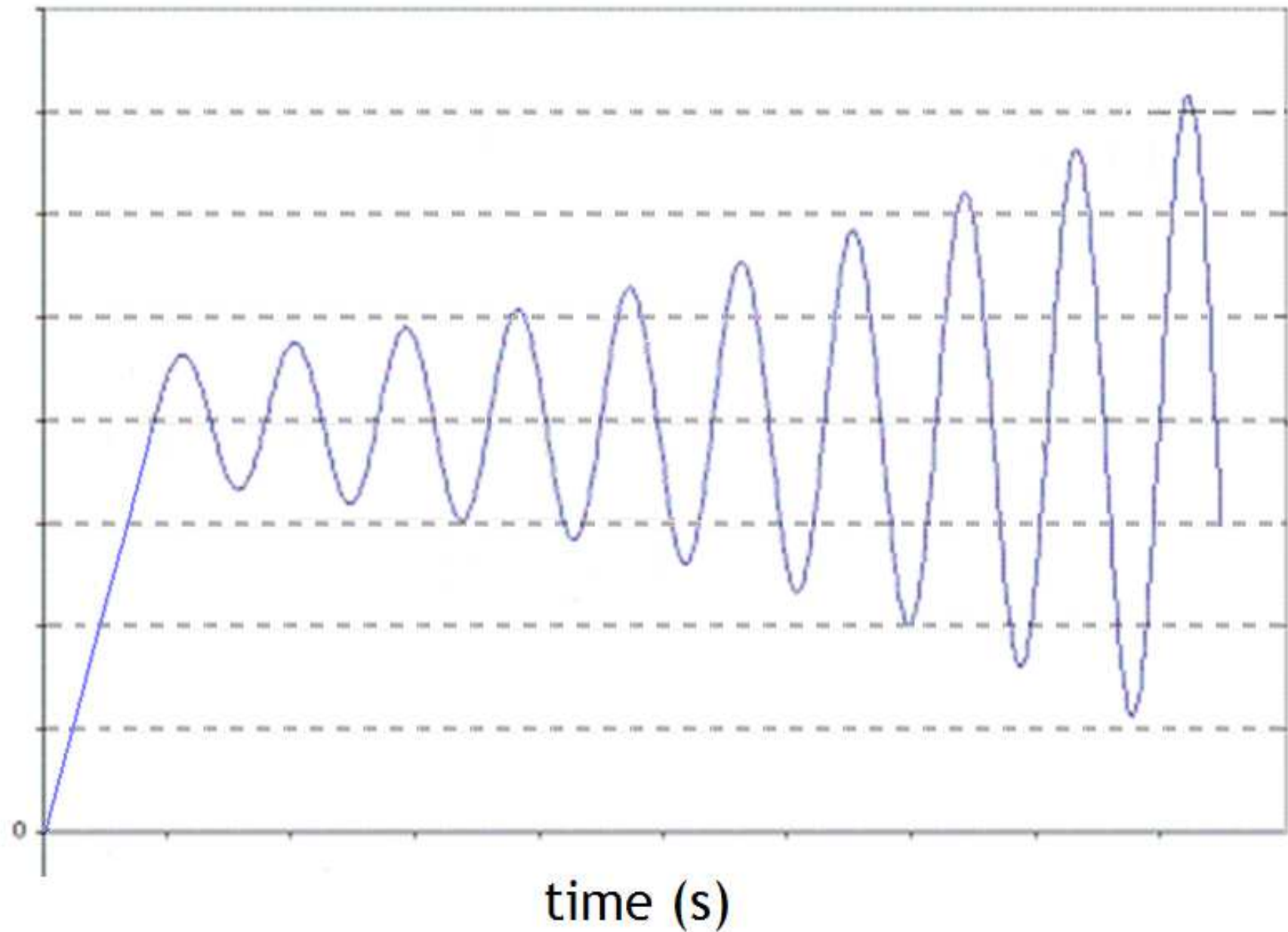
Time domain analysis - 2nd order systems

$\zeta < 0 \rightarrow$ **unstable system** (an example)



Time domain analysis - 2nd order systems

$\zeta < 0 \rightarrow$ unstable system (another example)





Departamento de
Engenharia Eletromecânica

Thank you!

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