

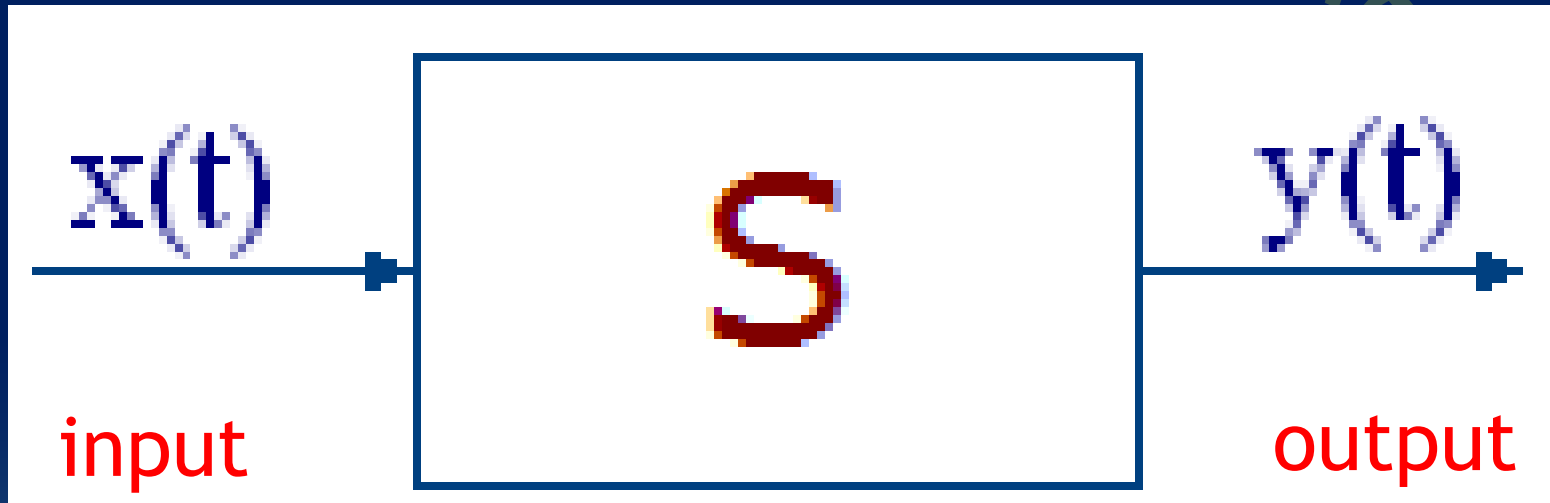
Control Systems

5

“Block Diagram, error and
PID controllers”

J. A. M. Felipe de Souza

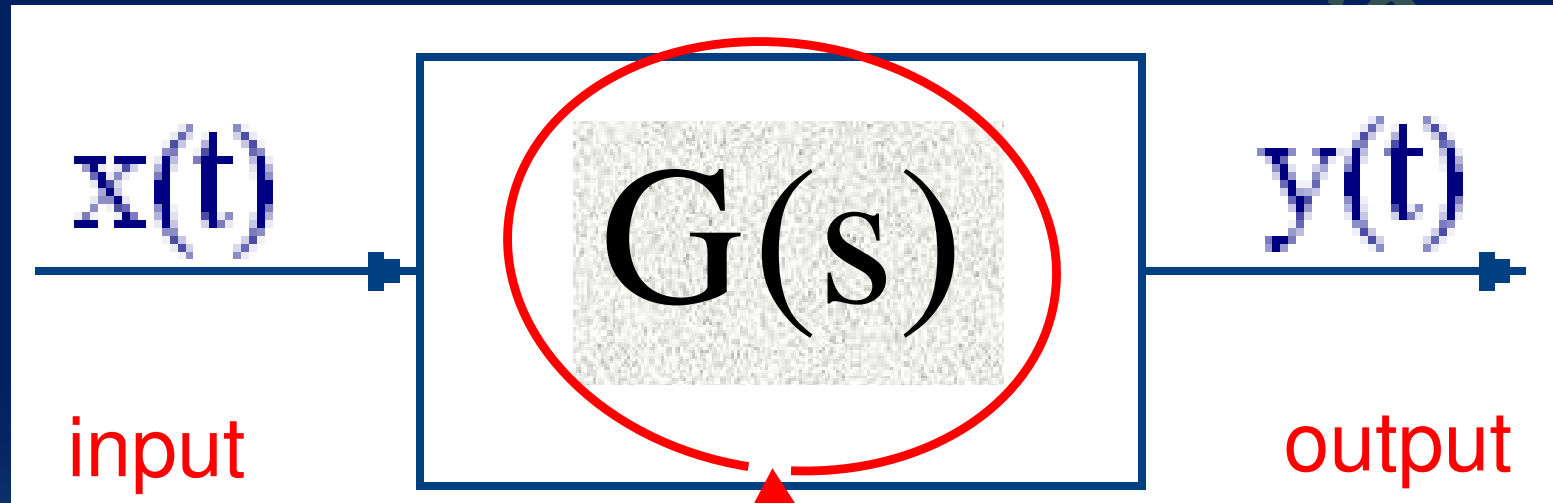
Block Diagrams & error



Single block

Black box

Black box



Transfer Function:

or:

$$G(s) = \frac{Y(s)}{X(s)}$$

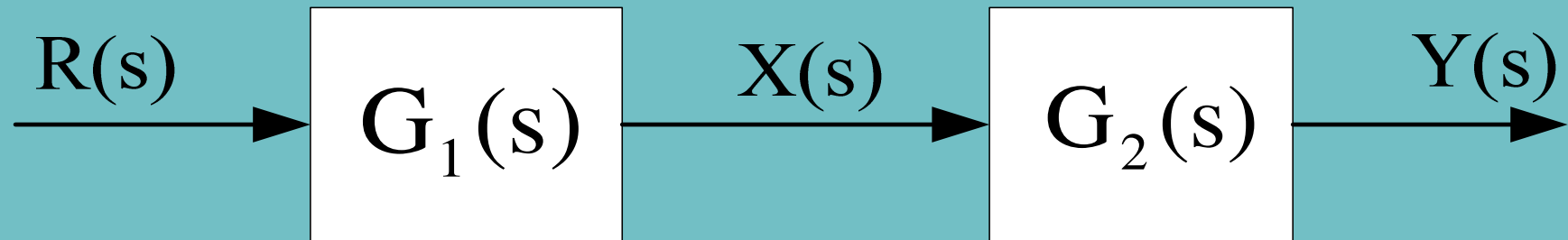
$$Y(s) = G(s) \cdot X(s)$$

that is,

$$\text{OUTPUT} = \text{T. F.} \times \text{INPUT}$$

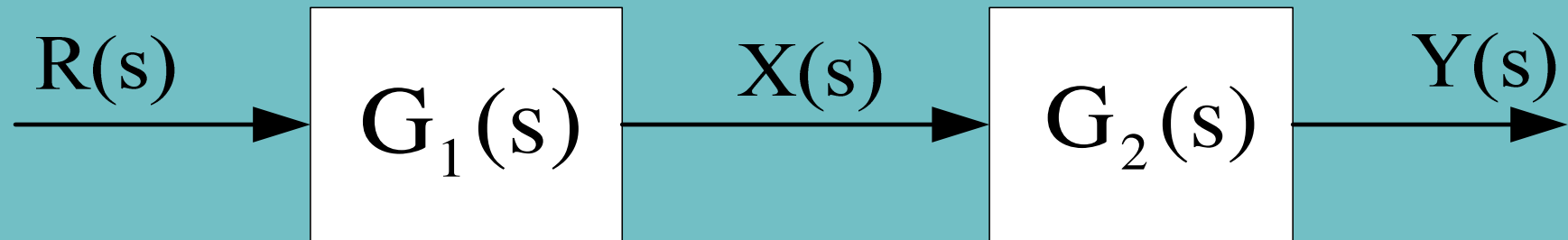
Block combination

blocks in cascade



the output $X(s)$ of the first block is
the input of the second block.

blocks in cascade

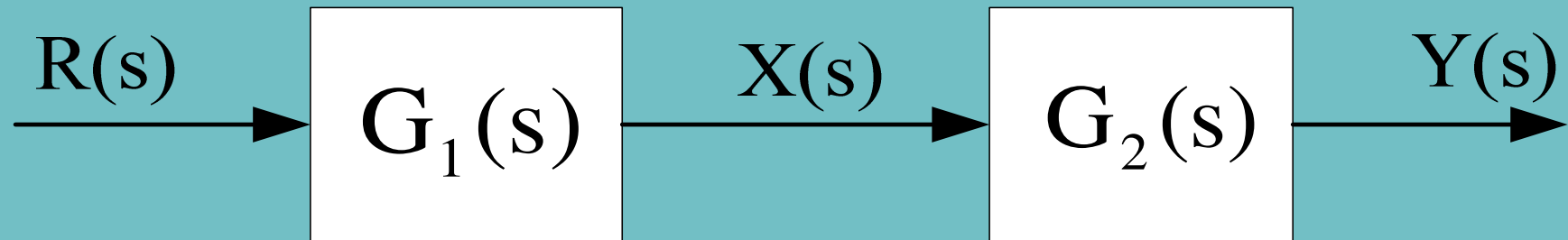


hence,

$$G_1(s) = \frac{X(s)}{R(s)}$$

$$G_2(s) = \frac{Y(s)}{X(s)}$$

blocks in cascade



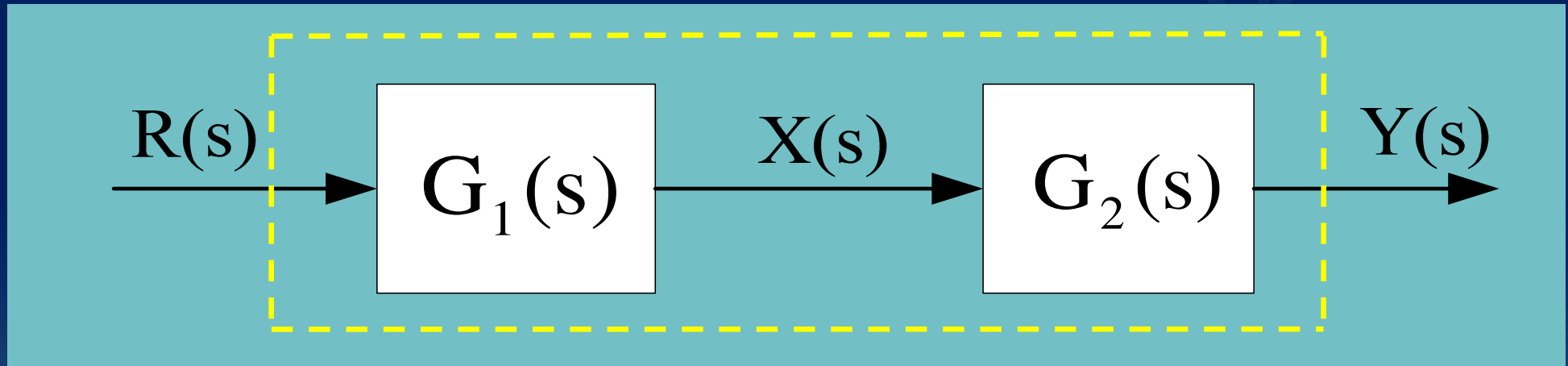
$$\text{OUTPUT} = \text{T.F.} \times \text{INPUT}$$

that is,

$$\left\{ \begin{array}{ll} X(s) = G_1(s) \cdot R(s) & \text{for the 1^o block} \\ Y(s) = G_2(s) \cdot X(s) & \text{for the 2^o block} \end{array} \right.$$

$$\text{OUTPUT} = \text{T.F.} \times \text{INPUT}$$

blocks in cascade



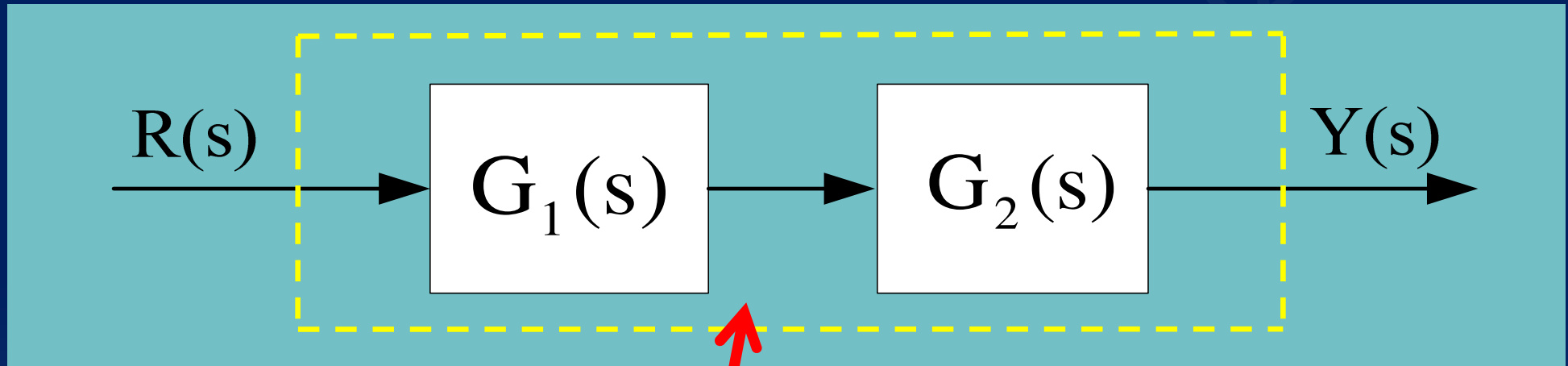
hence:

$$Y(s) = G_1(s) \cdot G_2(s) \cdot R(s)$$

or,

$$\frac{Y(s)}{R(s)} = G_1(s) \cdot G_2(s)$$

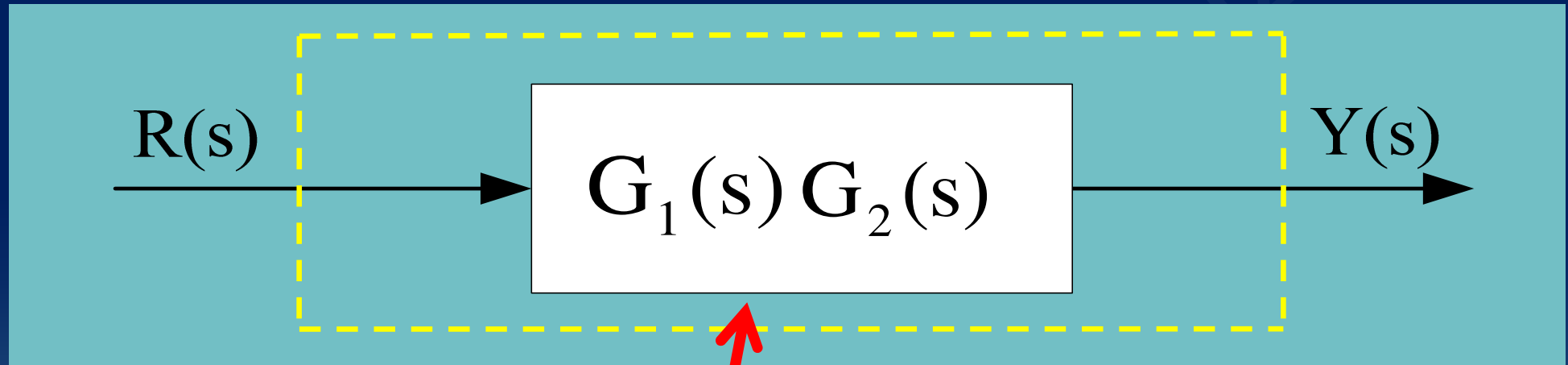
blocks in cascade



thus:

$$G_1(s) \cdot G_2(s)$$

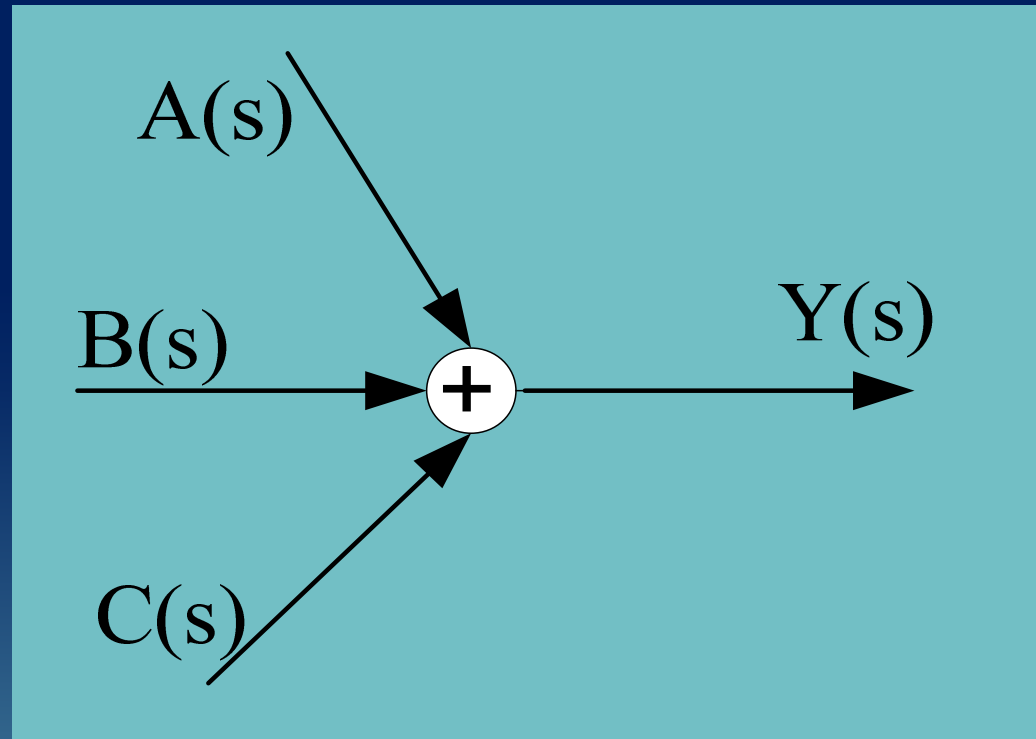
blocks in cascade



and hence:

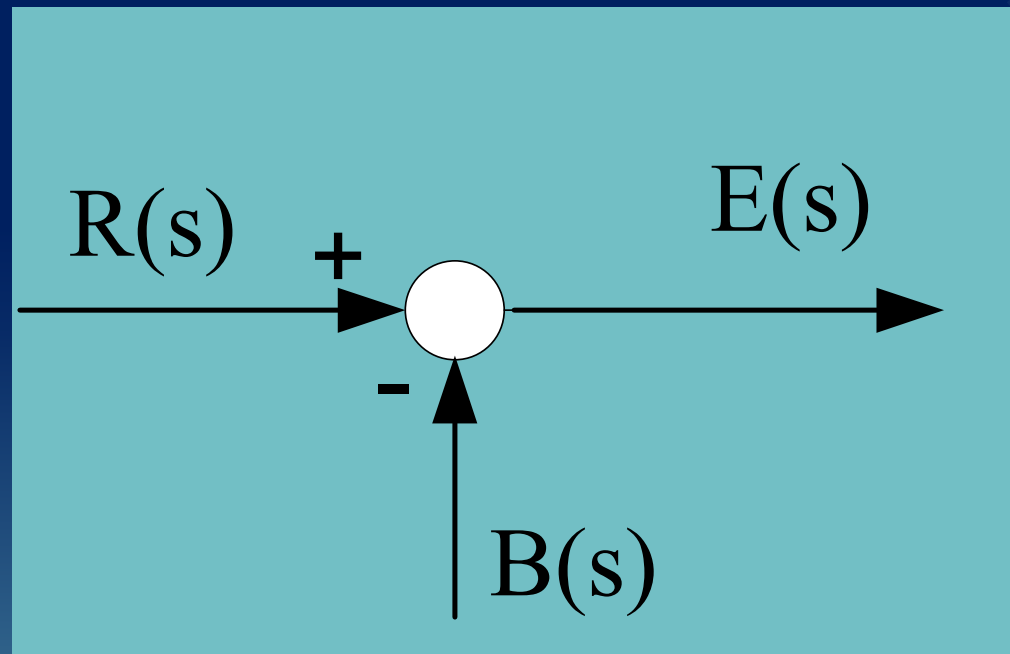
$$G_1(s) \cdot G_2(s)$$

summing point



$$Y(s) = A(s) + B(s) + C(s)$$

error detector



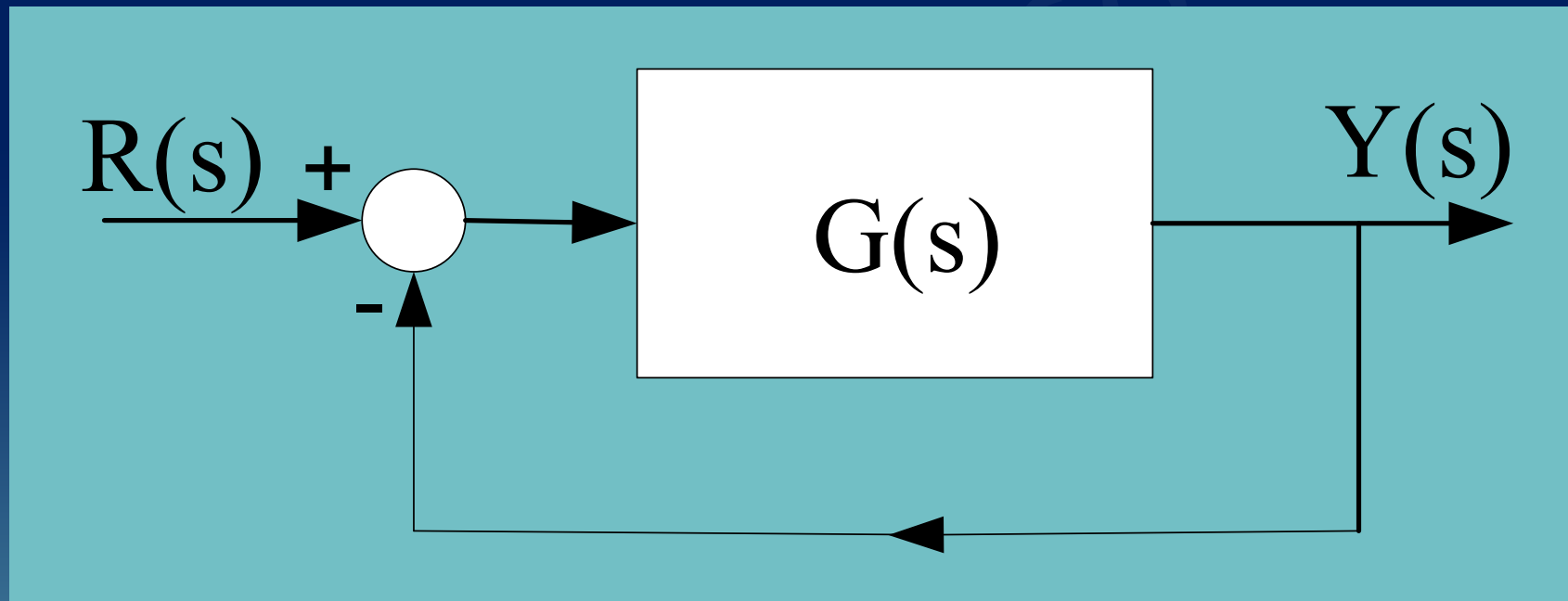
$$E(s) = R(s) - B(s)$$

Error

feedback

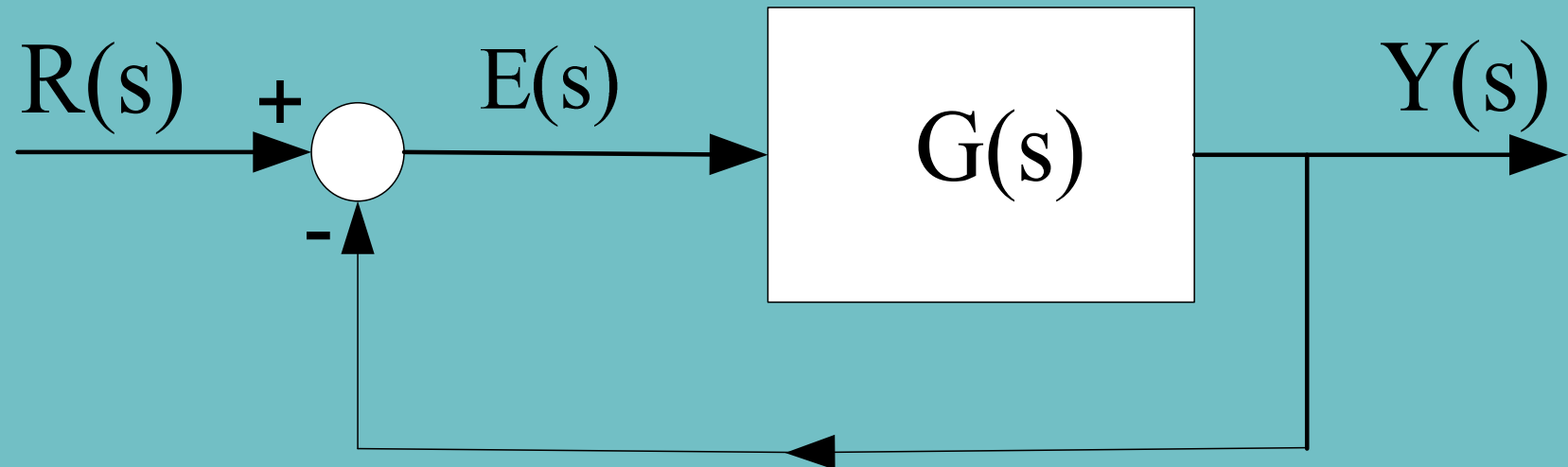
Prof. Felipe de Souza

feedback



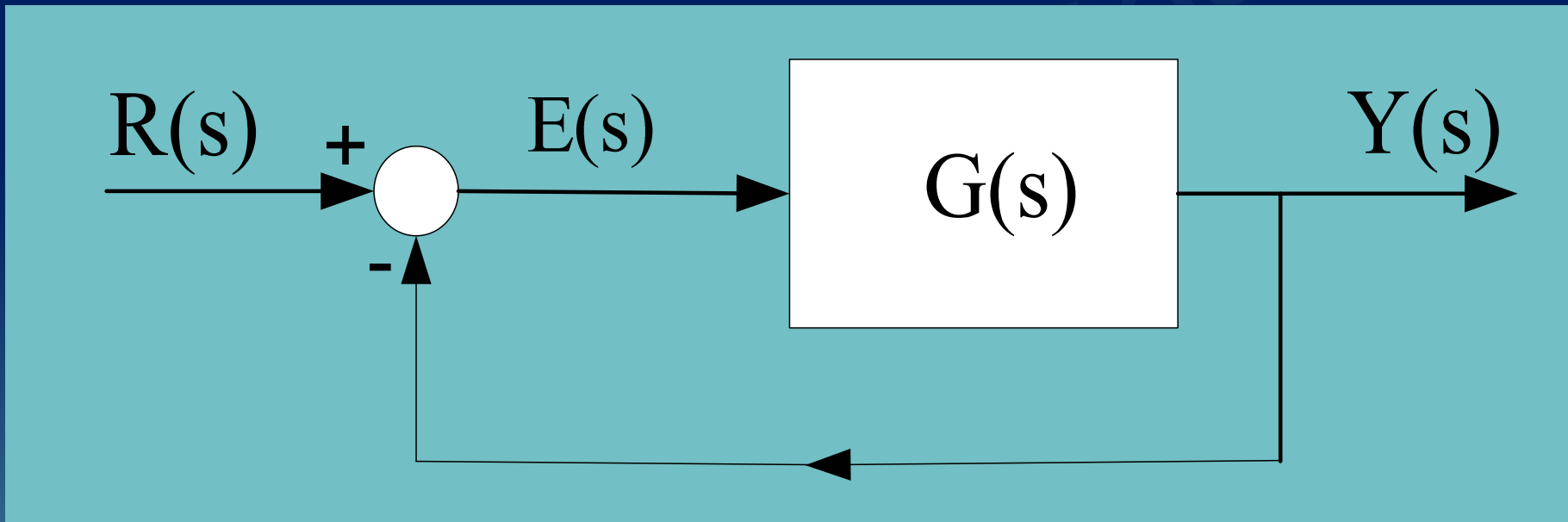
information from the **output** $Y(s)$ is reintroduced in the **input**, after comparing with the reference signal $R(s)$.

unit feedback



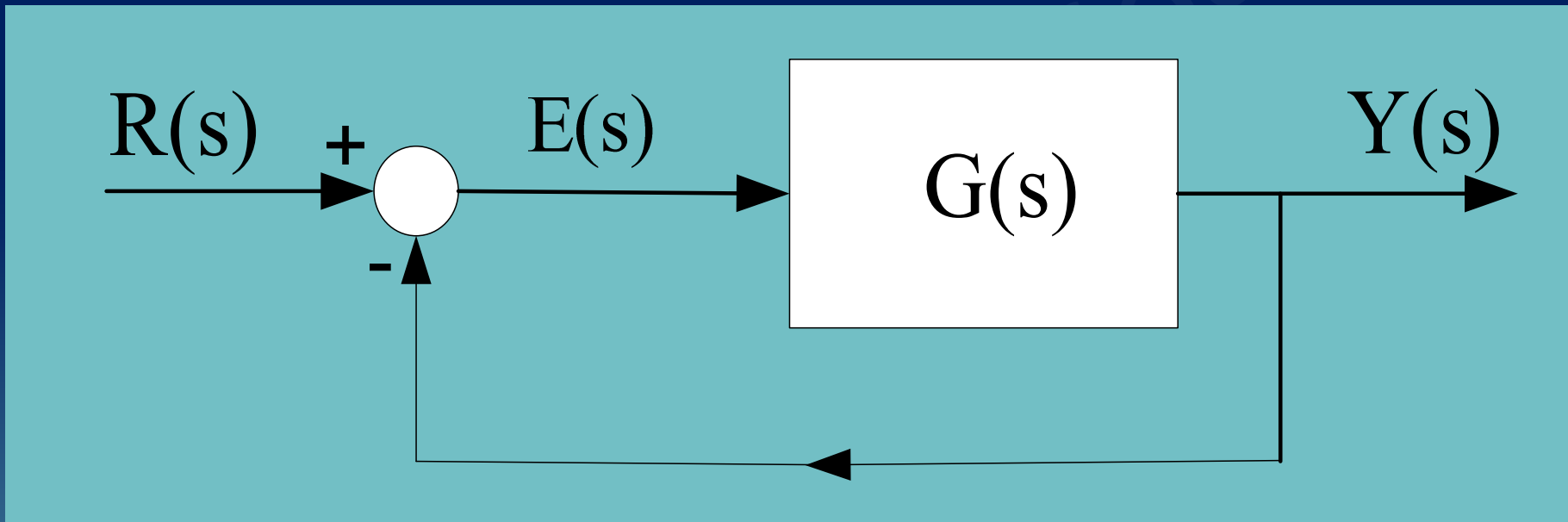
$$\begin{cases} E(s) = R(s) - Y(s) \\ Y(s) = G(s) \cdot E(s) \end{cases}$$

unit feedback



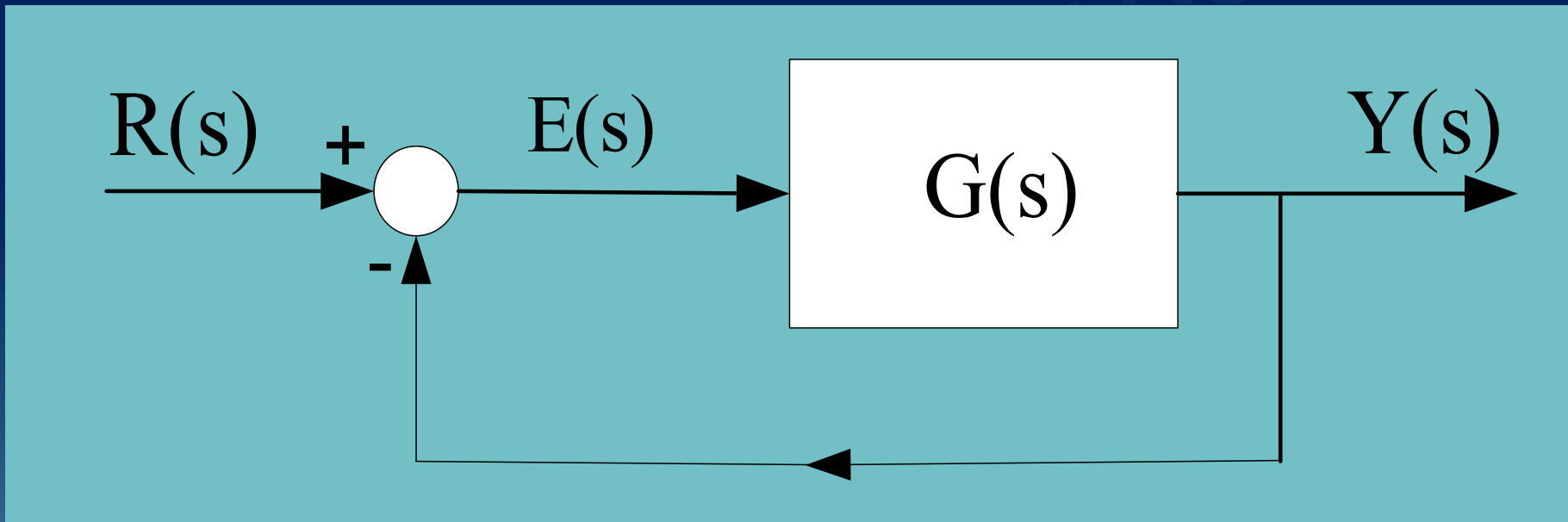
$$Y(s) = G(s) \cdot \overbrace{[R(s) - Y(s)]}^{E(s)}$$

unit feedback



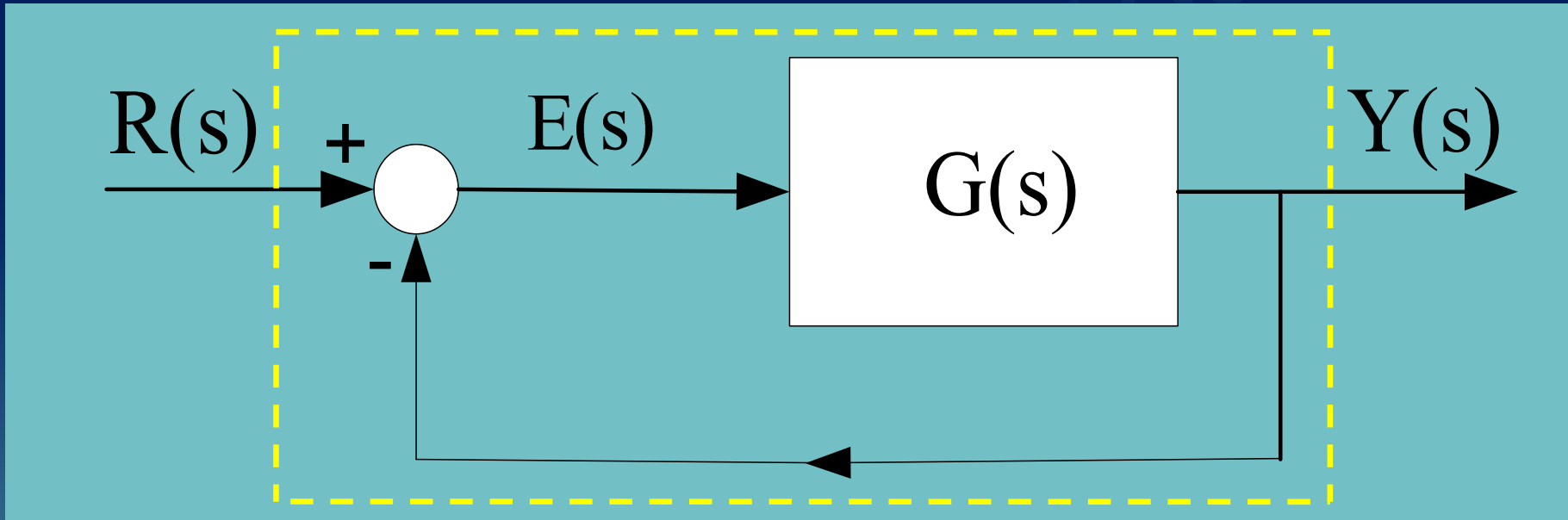
$$Y(s) = G(s) \cdot R(s) - G(s) Y(s)$$

unit feedback



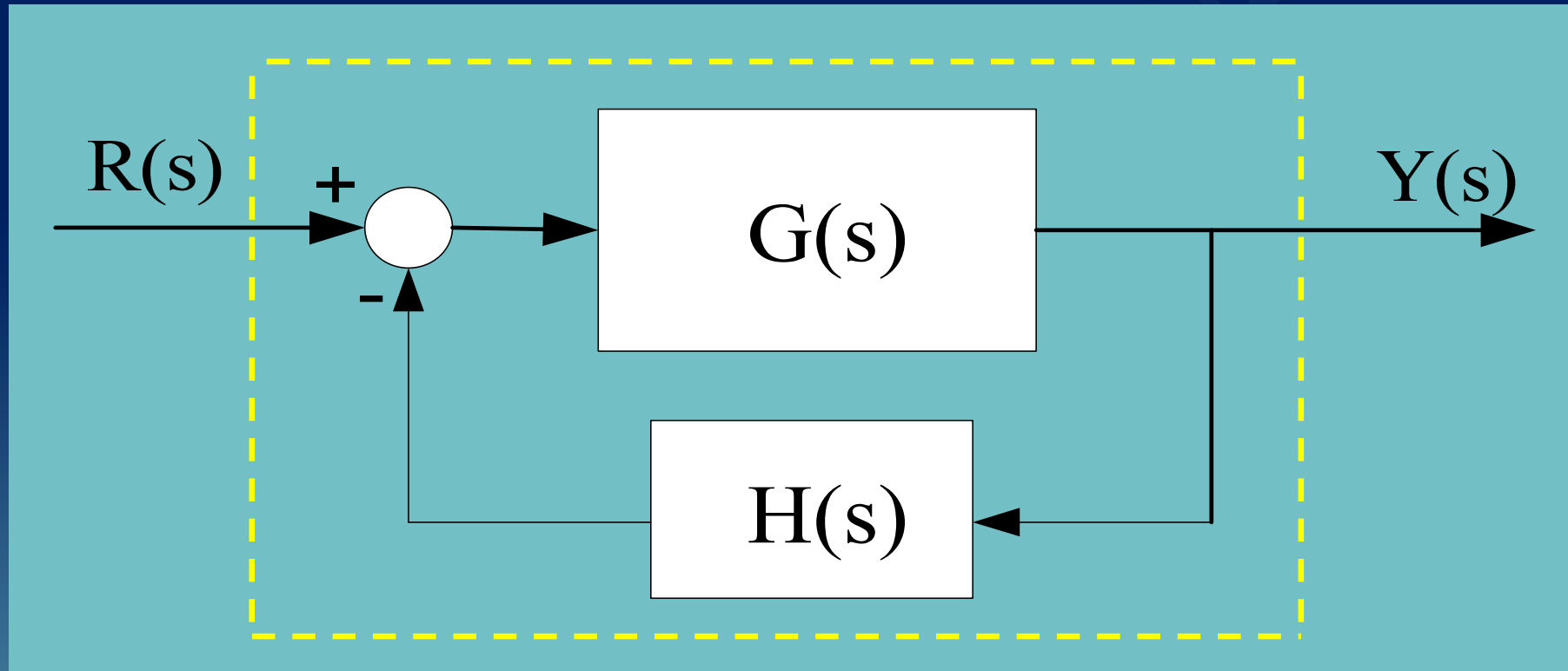
$$Y(s) \cdot [1 + G(s)] = R(s)G(s)$$

unit feedback



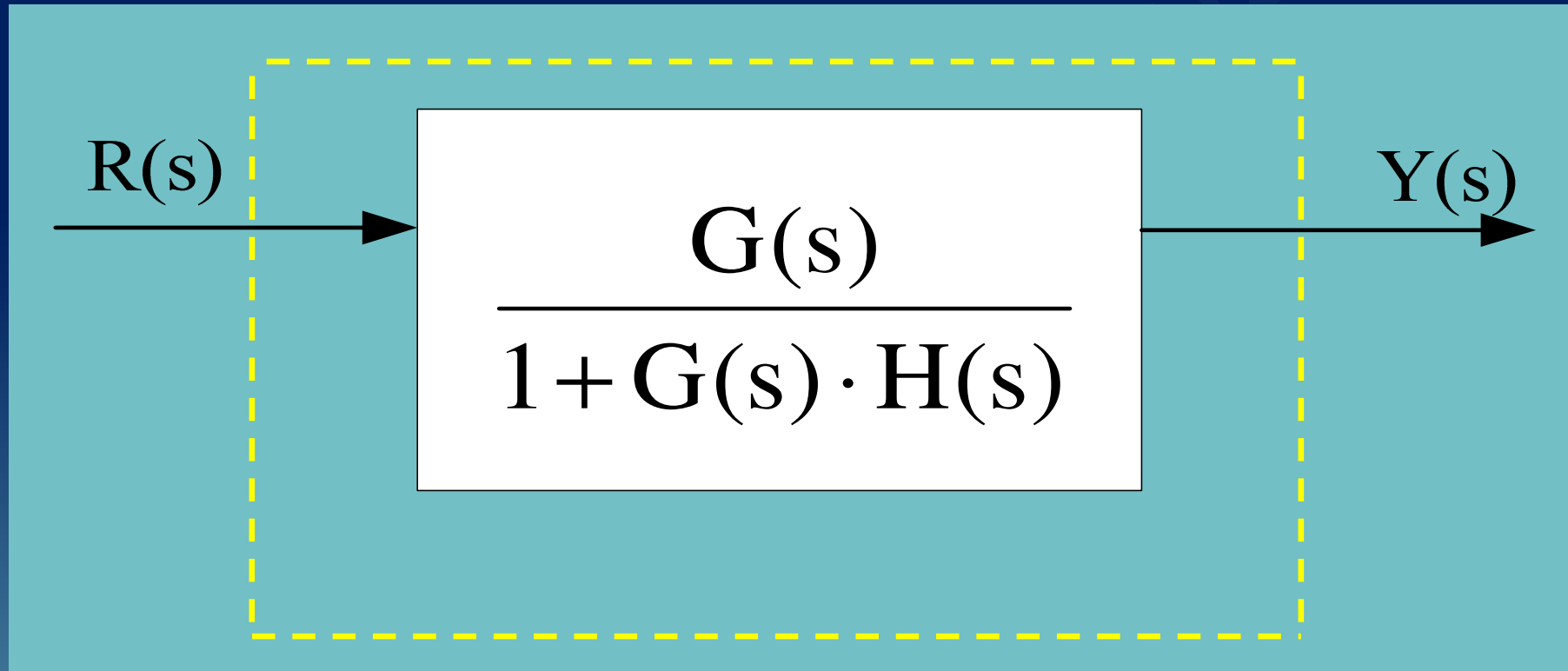
$$\frac{Y(s)}{R(s)} = \frac{G(s)}{1 + G(s)}$$

non unit feedback



$$\frac{Y(s)}{R(s)} = \frac{G(s)}{1 + G(s) \cdot H(s)}$$

non unit feedback



$$\frac{Y(s)}{R(s)} = \frac{G(s)}{1 + G(s) \cdot H(s)}$$

Note that

the unit feedback

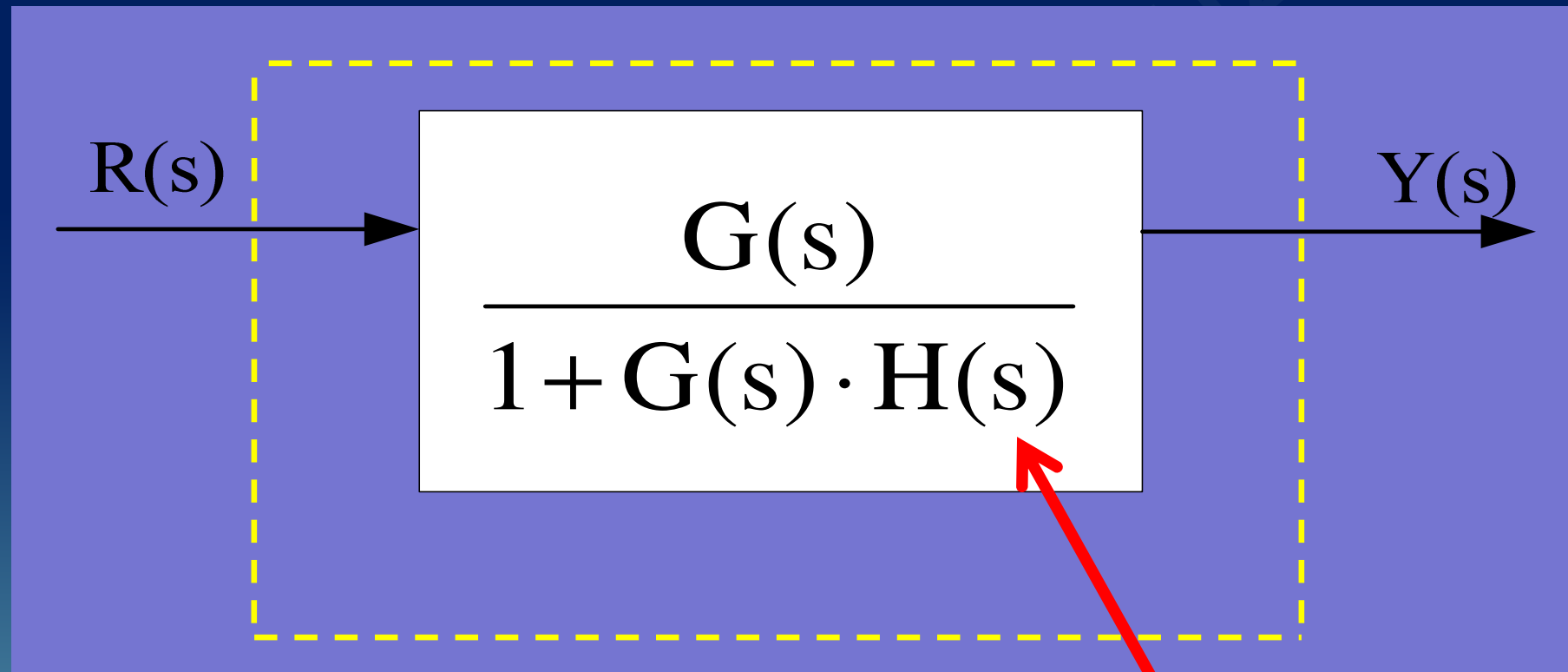
corresponds to

non unit feedback

with

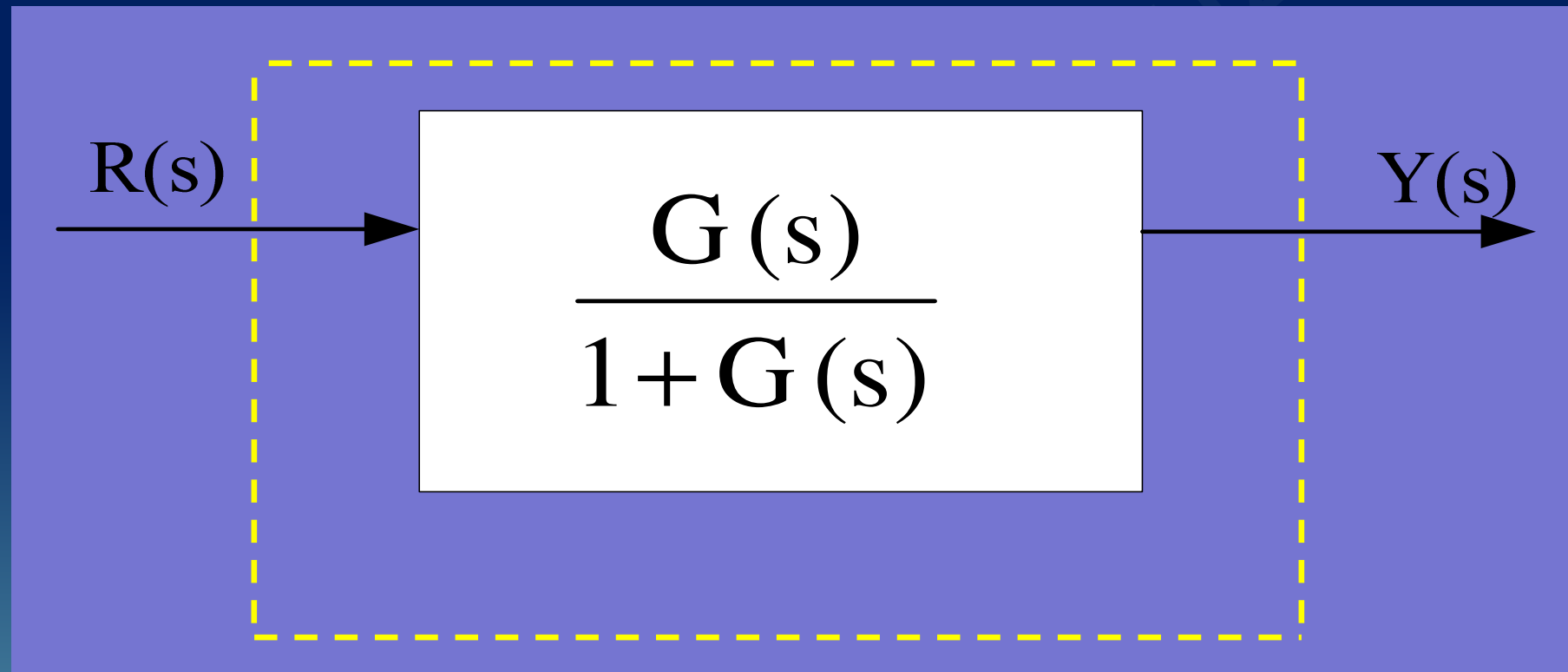
$$H(s) = 1$$

unit feedback



$$H(s) = 1$$

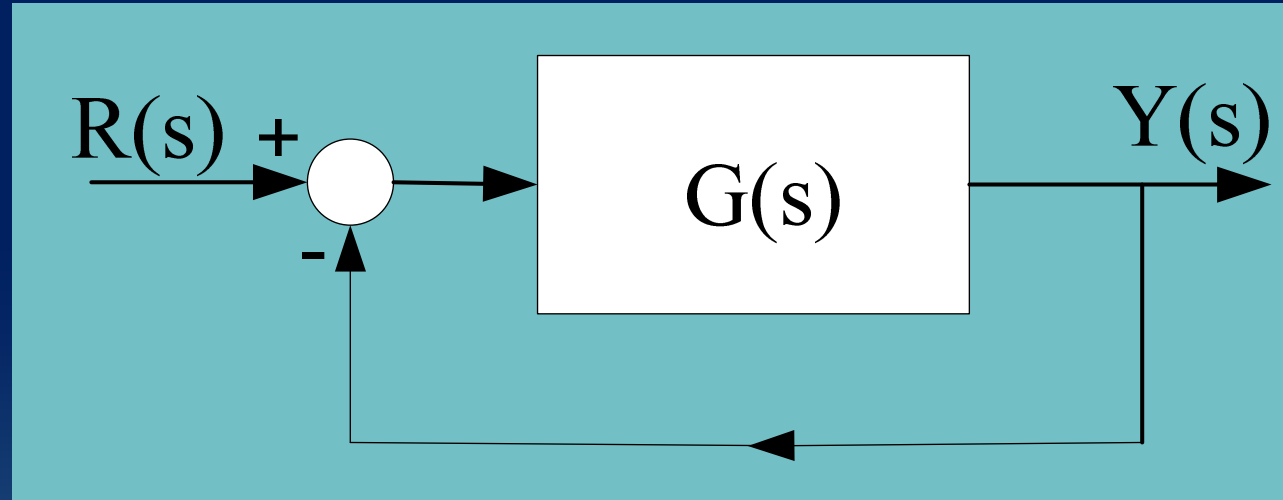
unit feedback



$$\frac{Y(s)}{R(s)} = \frac{G(s)}{1 + G(s)}$$

Example 1:

$$G(s) = \frac{5}{s(s+4)}$$



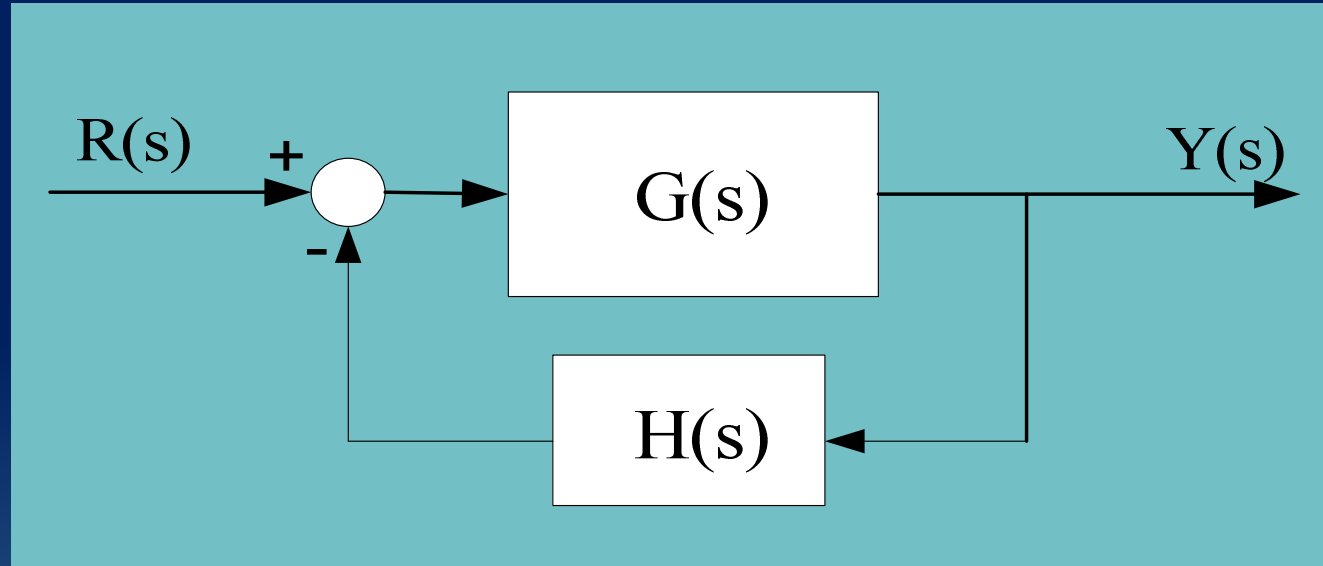
$$\frac{Y(s)}{R(s)} = \frac{G(s)}{1 + G(s)} = \frac{\frac{5}{s(s+4)}}{1 + \frac{5}{s(s+4)}} = \frac{5}{s^2 + 4s + 5}$$

Block Diagrams & error

Example 2:

$$G(s) = \frac{5}{s(s+4)}$$

$$H(s) = \frac{1}{(s+3)}$$



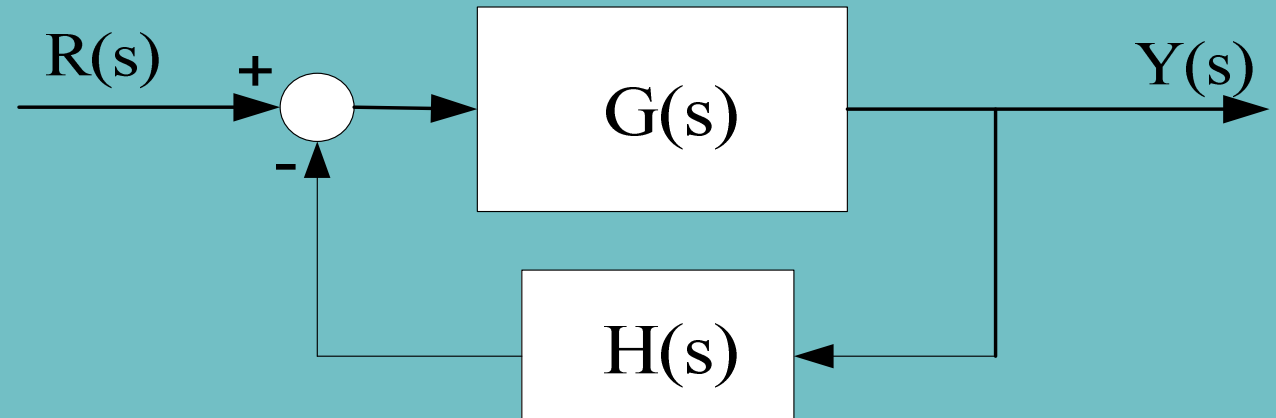
$$\frac{Y(s)}{R(s)} = \frac{G(s)}{1 + G(s)H(s)} = \frac{\frac{5}{s(s+4)}}{1 + \frac{5}{s(s+4)} \cdot \frac{1}{(s+3)}}$$

Block Diagrams & error

Example 2:

$$G(s) = \frac{5}{s(s+4)}$$

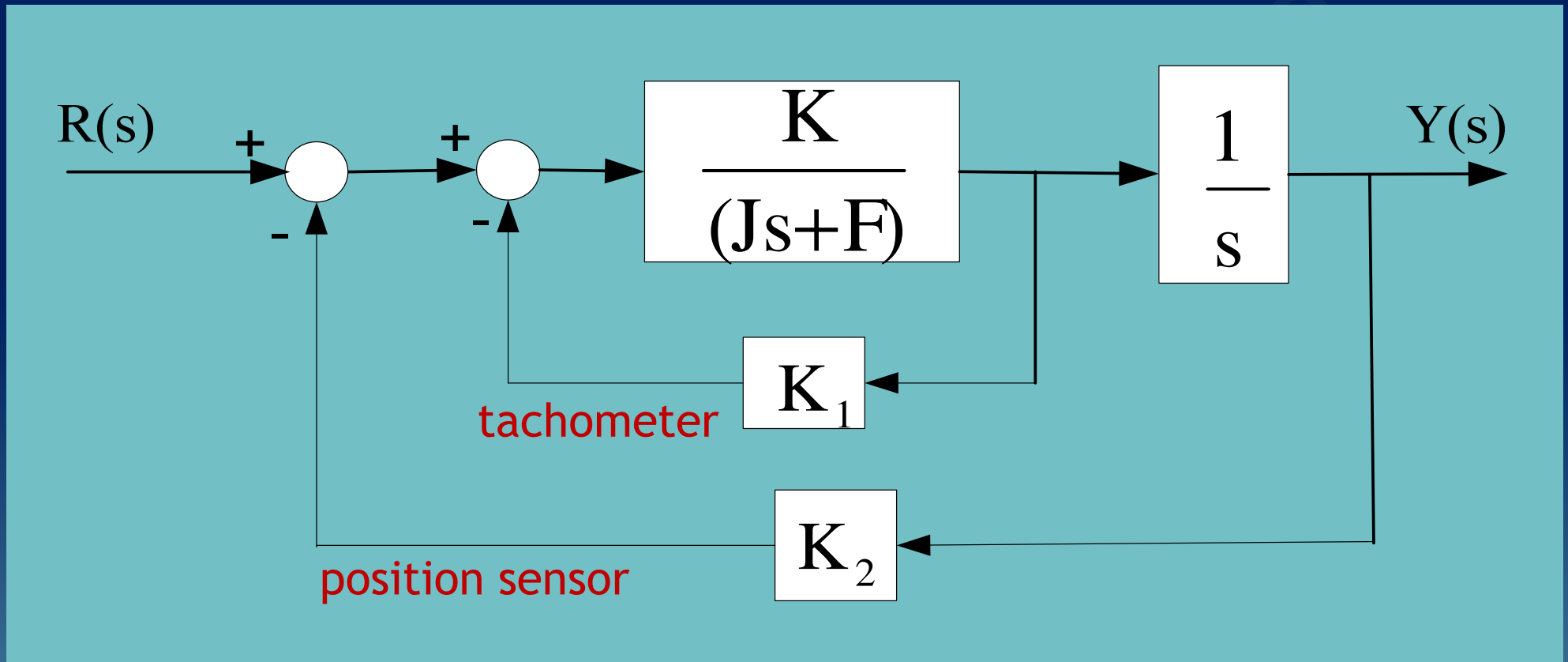
$$H(s) = \frac{1}{(s+3)}$$



$$\frac{Y(s)}{R(s)} = \frac{5(s+3)}{(s^3 + 7s^2 + 12s + 5)}$$

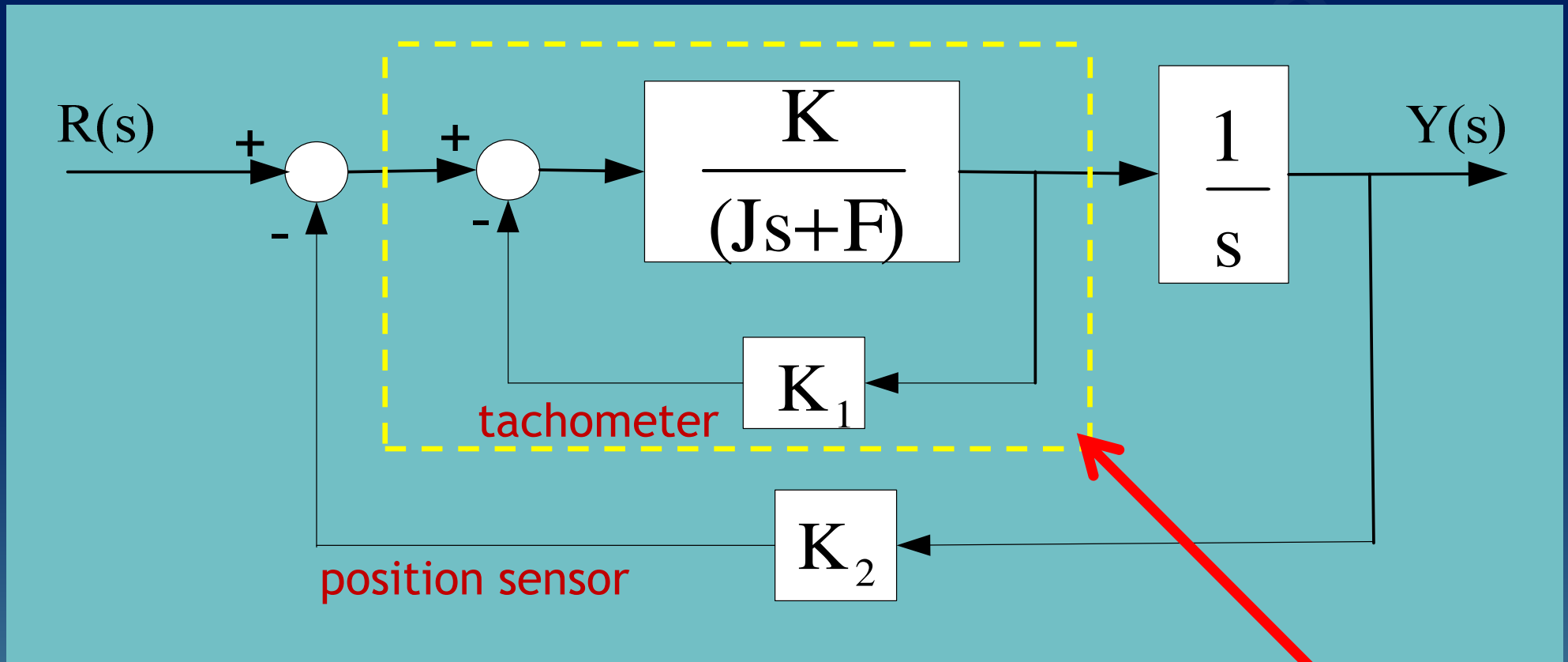
feedback with tachometers

feedback with tachometers



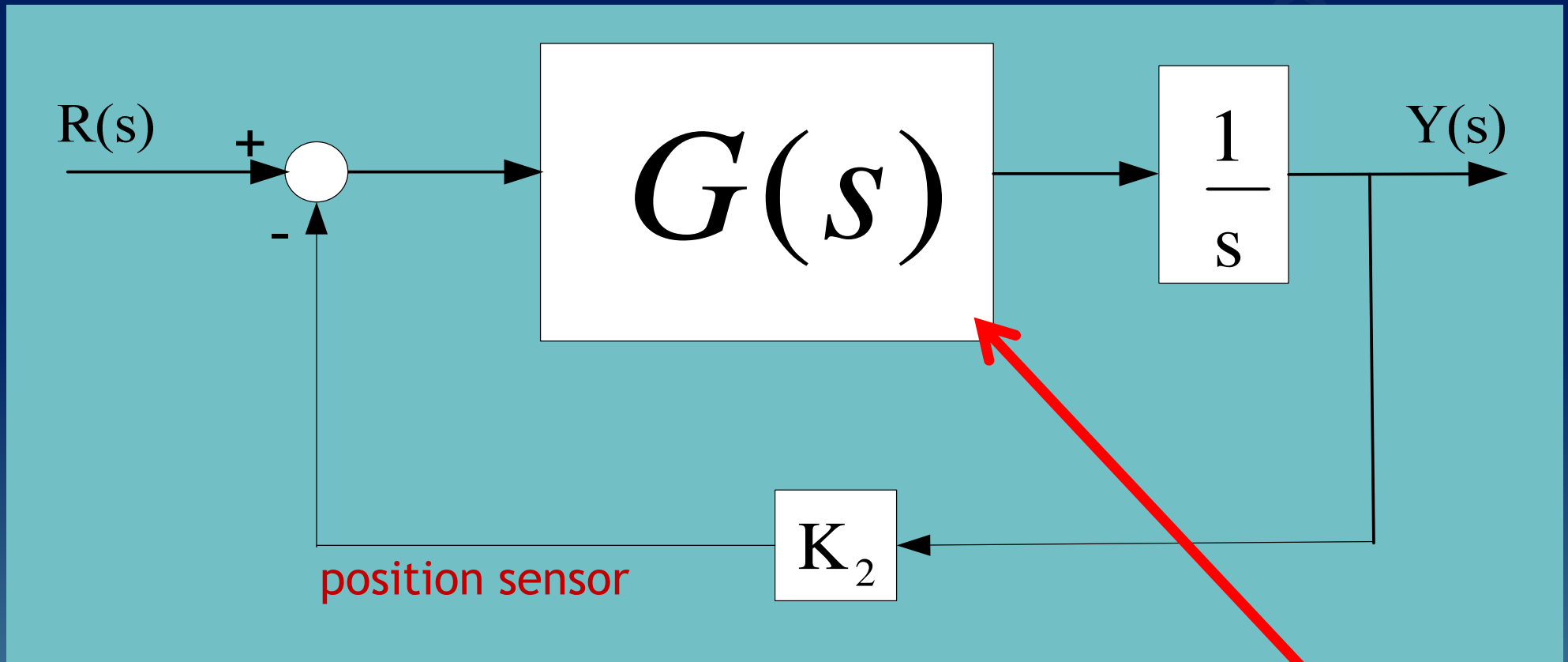
for servo systems with velocity feedback

feedback with tachometers



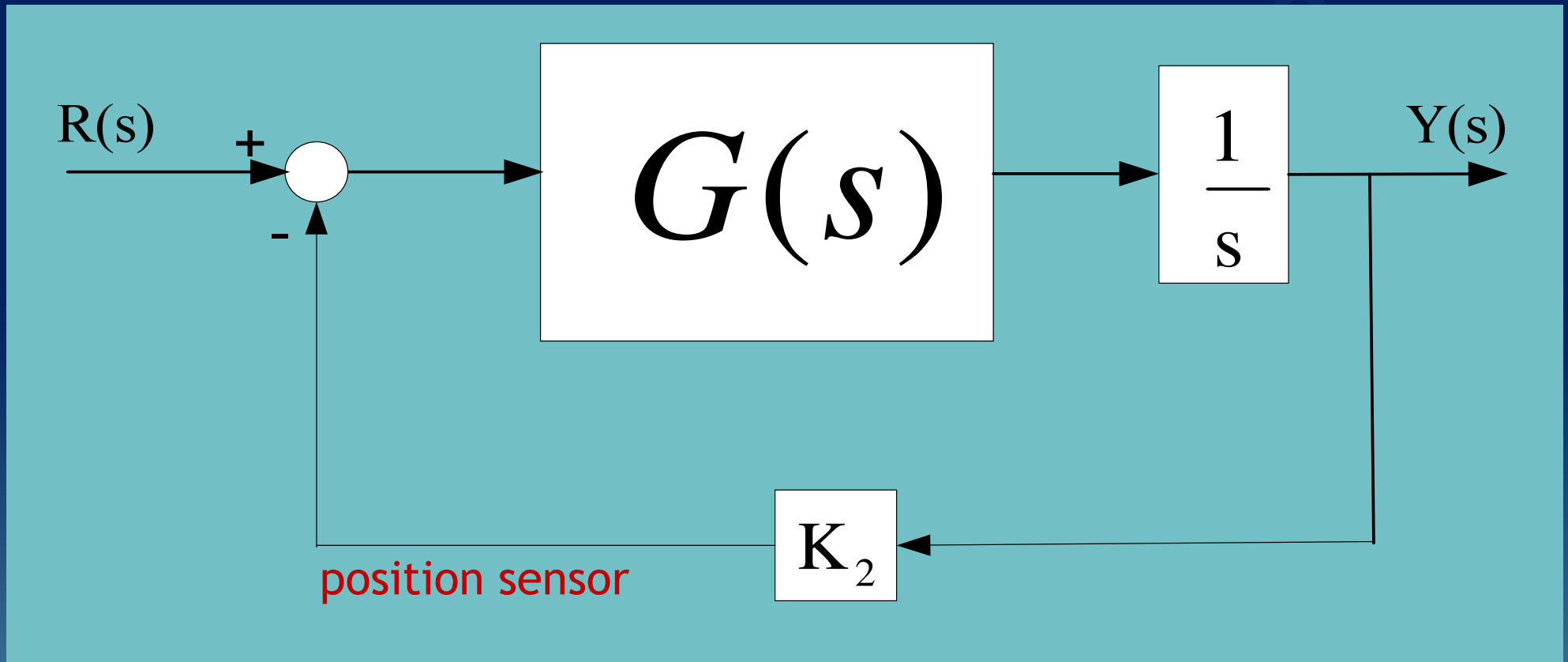
$$G(s) = \frac{\frac{K}{(Js + F)}}{1 + \frac{KK_1}{(Js + F)}}$$

feedback with tachometers



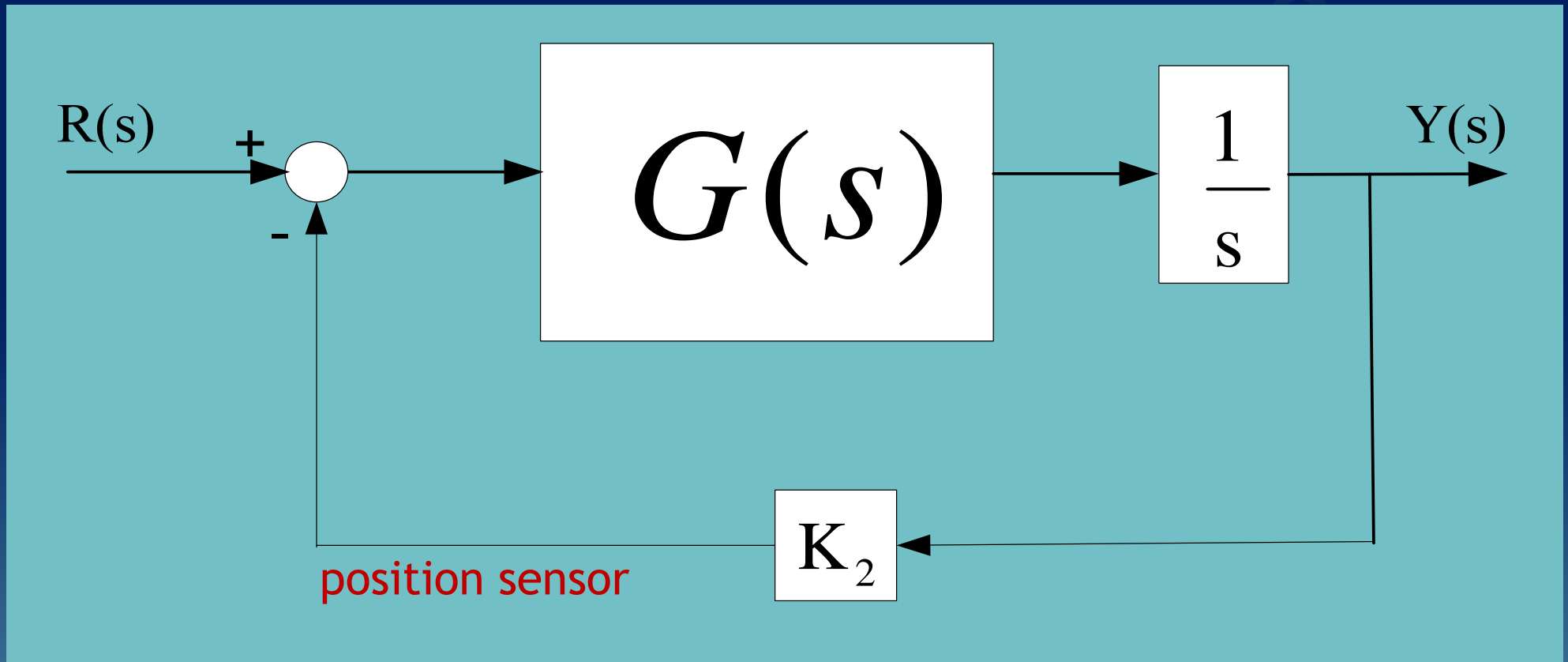
$$G(s) = \frac{\frac{K}{(Js + F)}}{1 + \frac{KK_1}{(Js + F)}}$$

feedback with tachometers



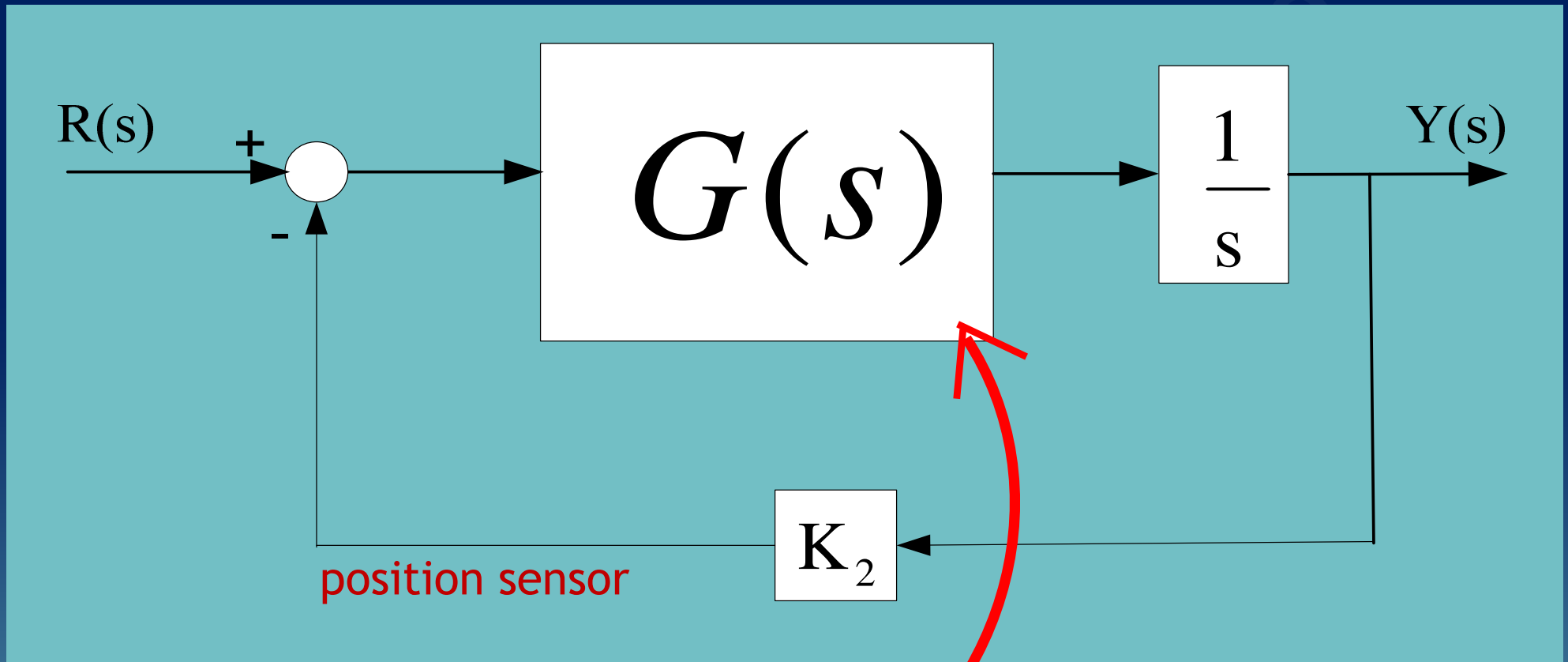
$$G(s) = \frac{\frac{K}{(Js + F)}}{1 + \frac{KK_1}{(Js + F)}}$$

feedback with tachometers



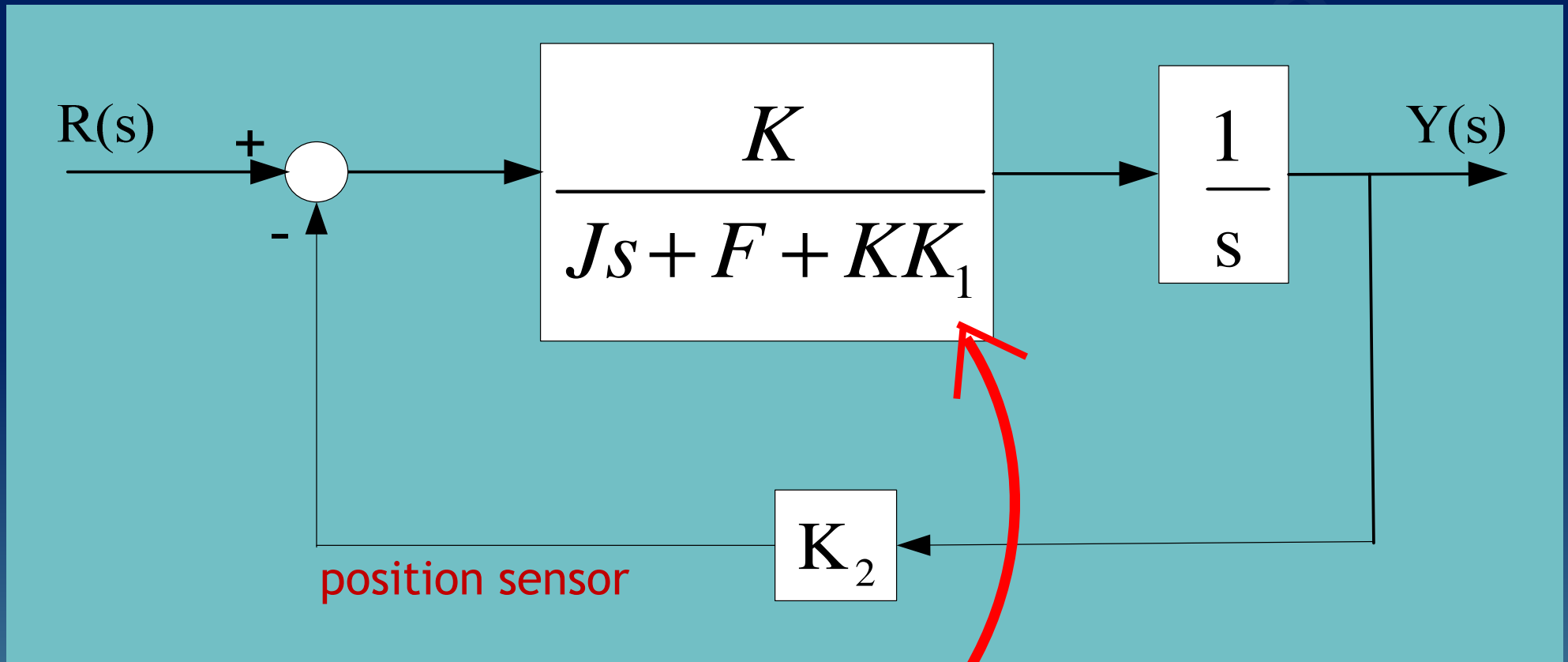
$$G(s) = \frac{\frac{K}{(Js + F)}}{1 + \frac{KK_1}{(Js + F)}} = \frac{K}{Js + F + KK_1}$$

feedback with tachometers



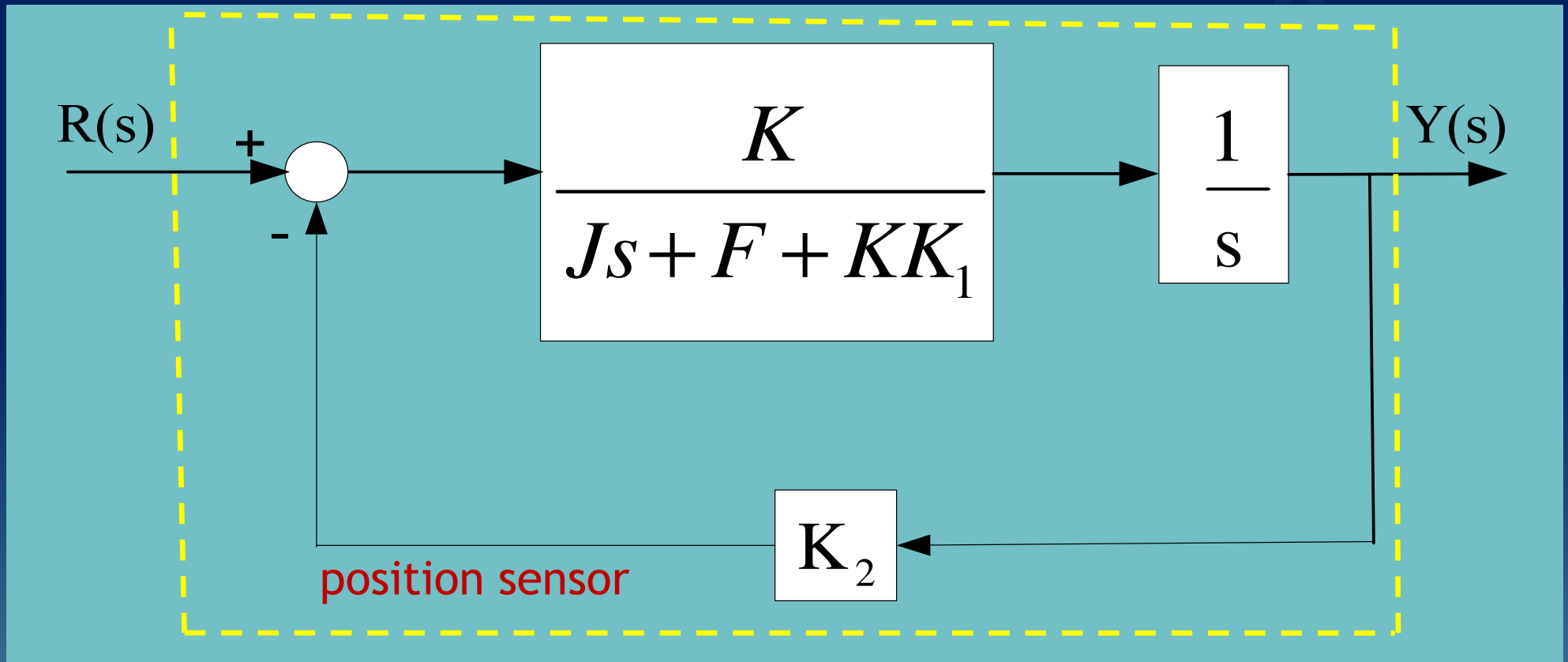
$$G(s) = \frac{K}{Js + F + KK_1}$$

feedback with tachometers



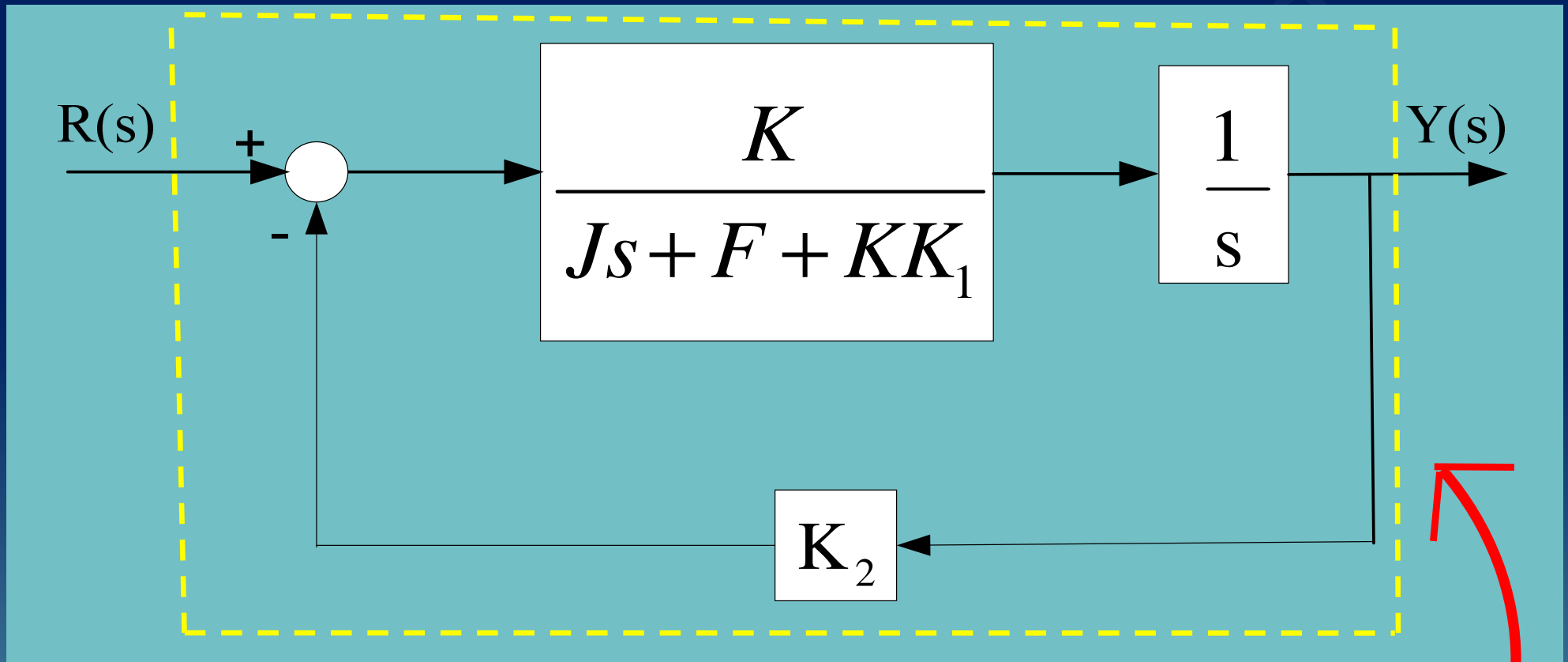
$$G(s) = \frac{K}{Js + F + KK_1}$$

feedback with tachometers



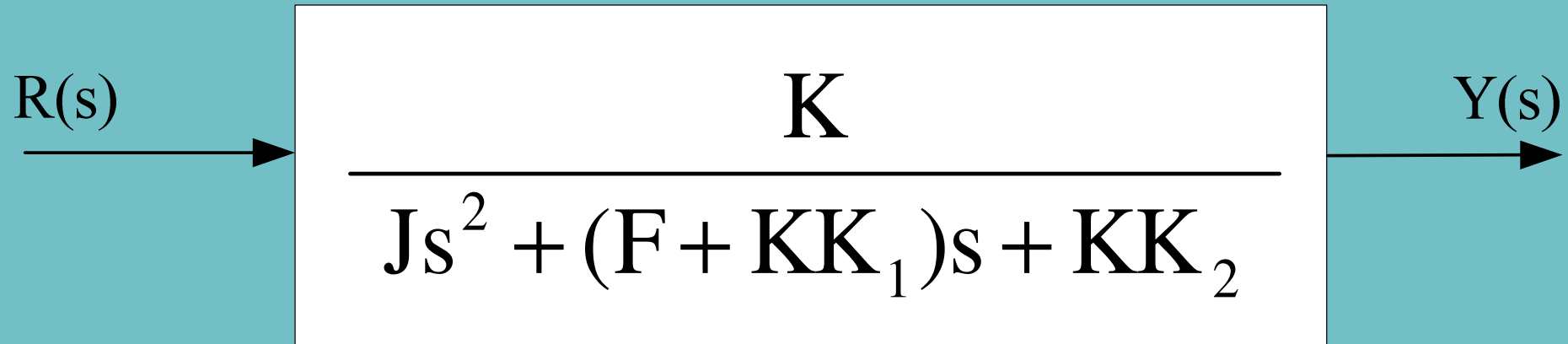
$$\frac{Y(s)}{R(s)} = \frac{\frac{K}{Js + (F + KK_1)} \cdot \frac{1}{s}}{1 + \frac{K}{Js + (F + KK_1)} \cdot \frac{1}{s} \cdot K_2}$$

feedback with tachometers



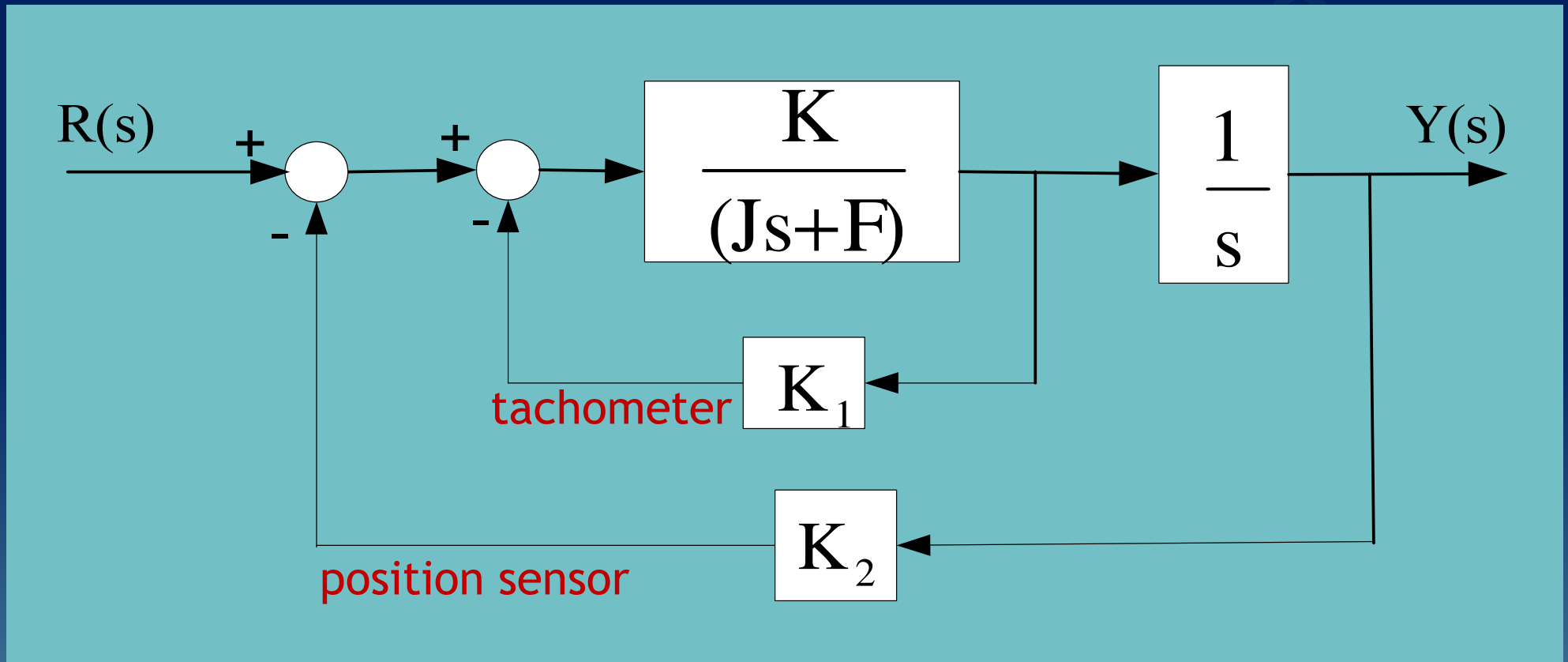
$$\frac{Y(s)}{R(s)} = \frac{K}{Js^2 + (F + KK_1)s + KK_2}$$

feedback with tachometers

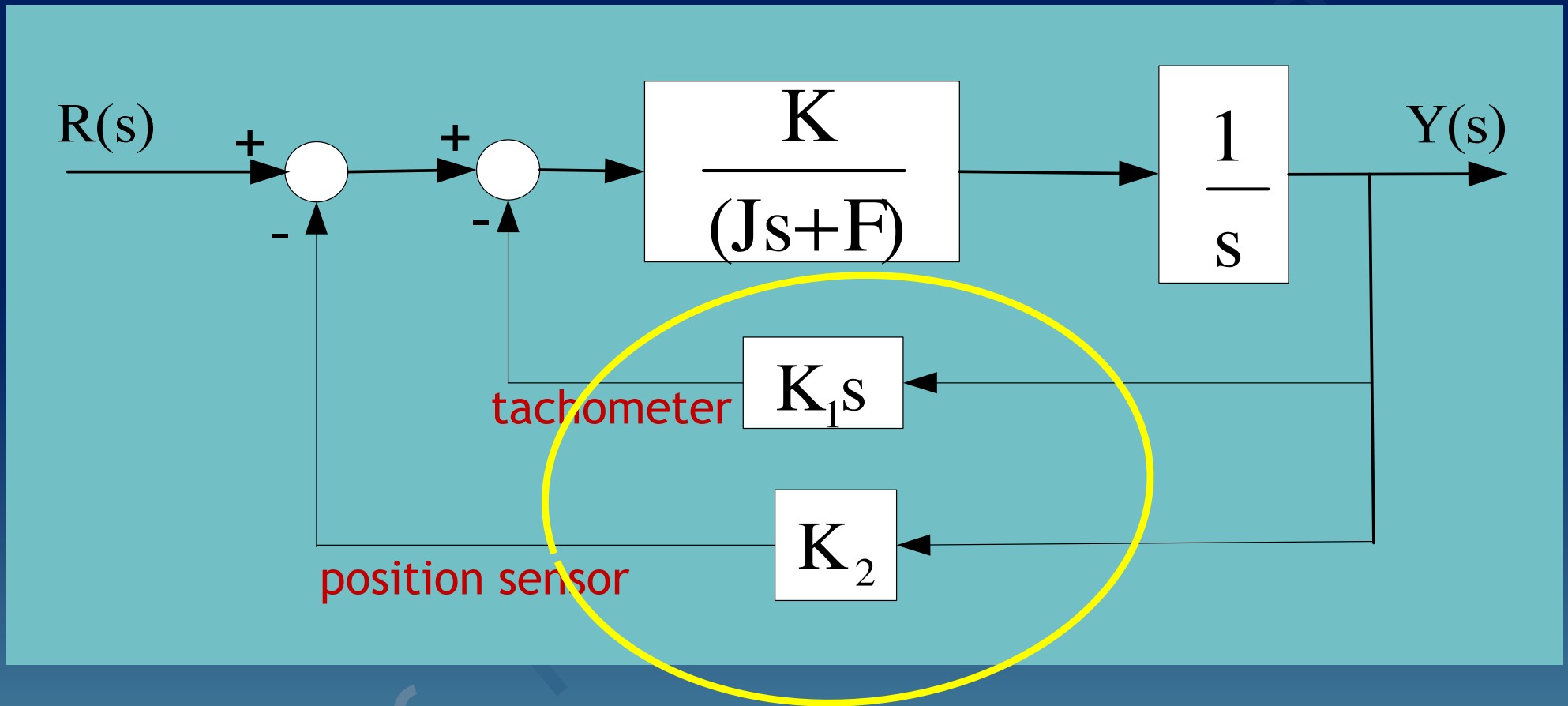


feedback with tachometers
(another approach)

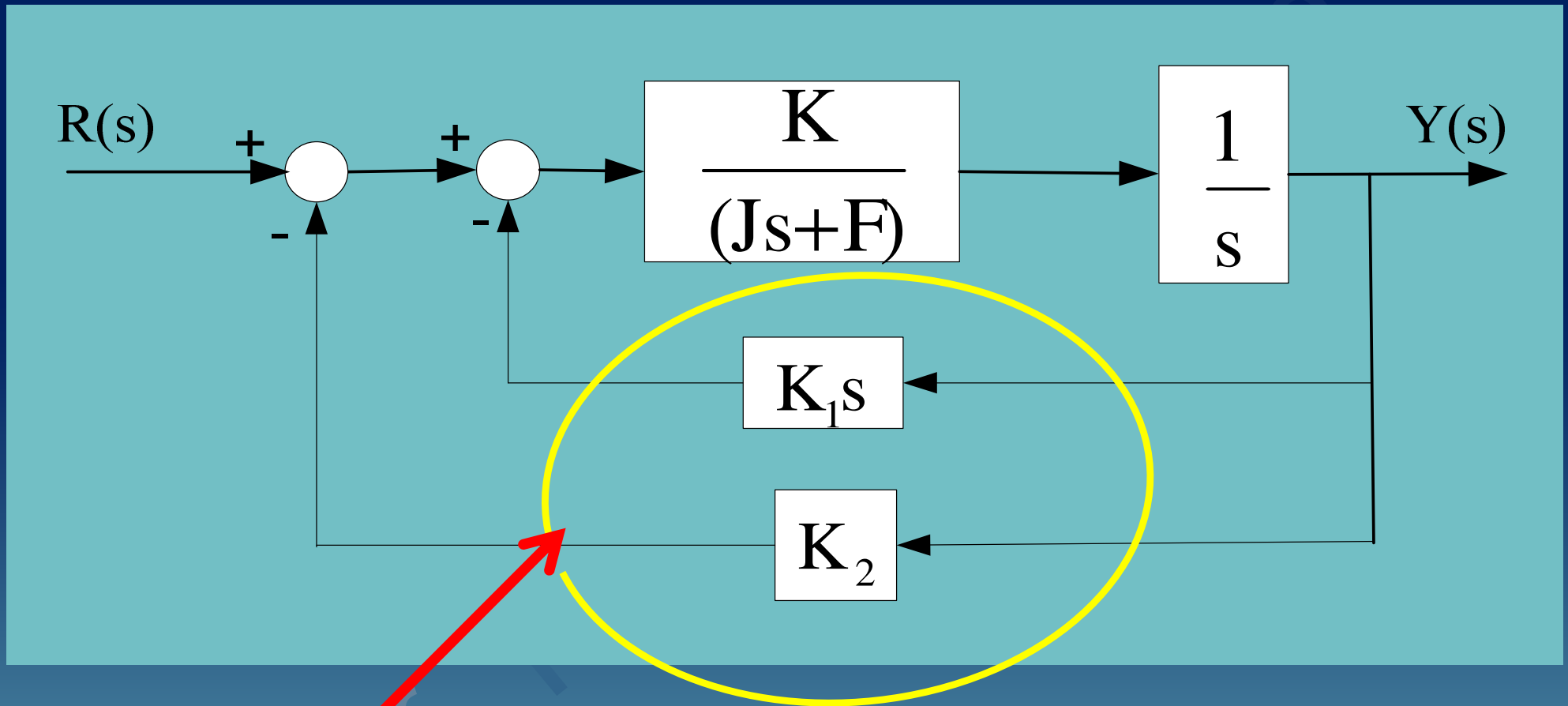
feedback with tachometers



feedback with tachometers

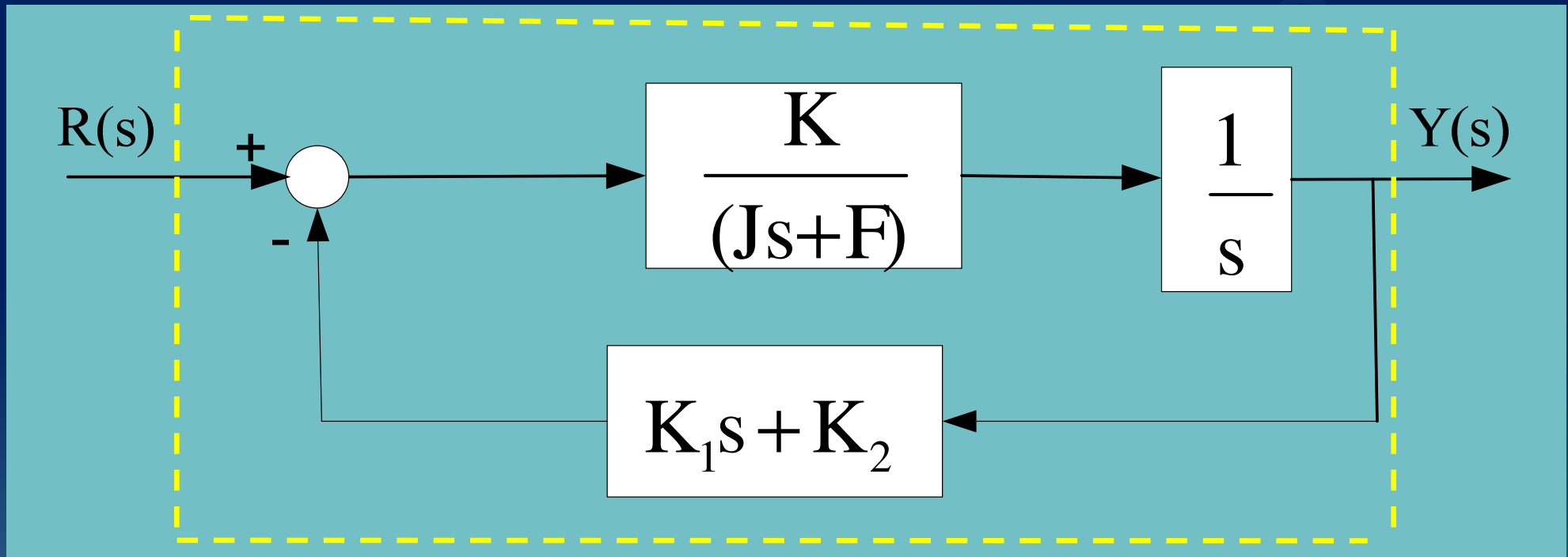


feedback with tachometers



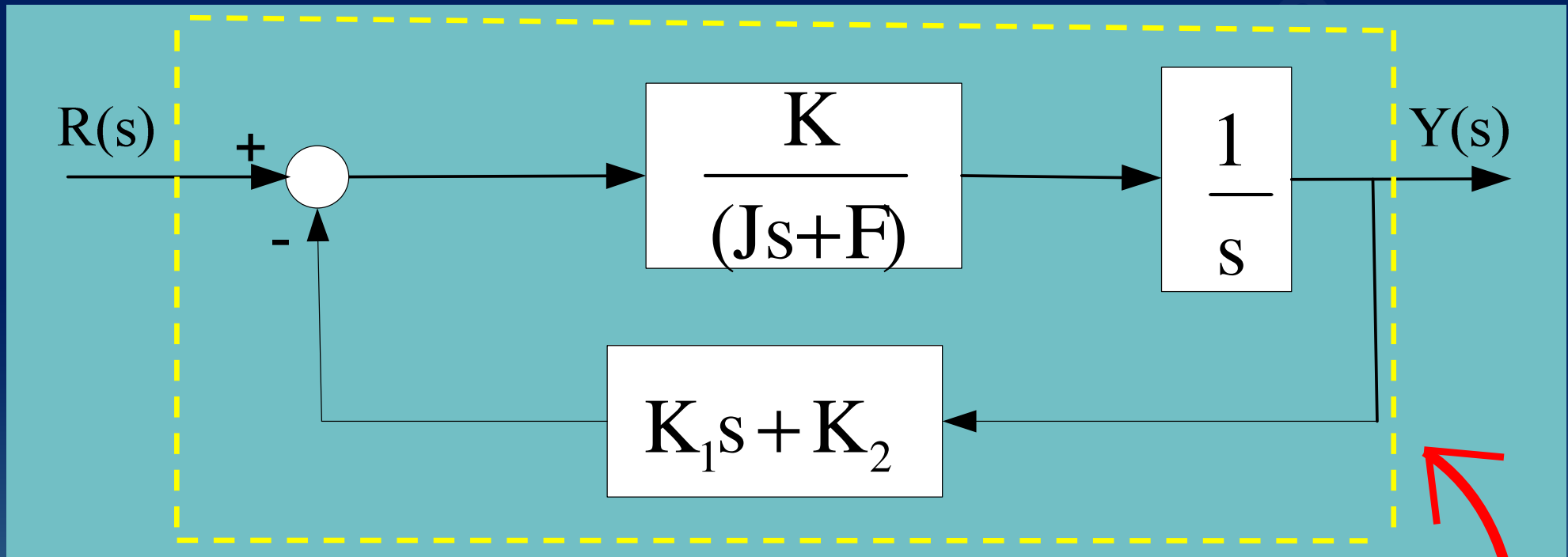
$$K_1s + K_2$$

feedback with tachometers



$$\frac{Y(s)}{R(s)} = \frac{\frac{K}{(Js + F)} \cdot \frac{1}{s}}{1 + \frac{K(K_1s + K_2)}{(Js + F)s}}$$

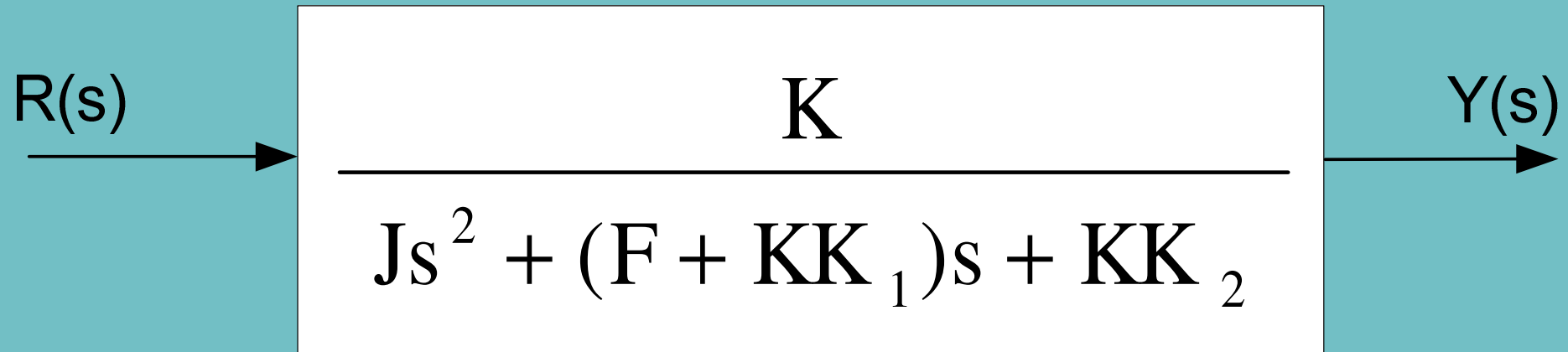
feedback with tachometers



$$\frac{Y(s)}{R(s)} = \frac{K}{Js^2 + (F + KK_1)s + KK_2}$$

which is the **same result** obtained earlier, with the first approach

feedback with tachometers



$$\frac{Y(s)}{R(s)} = \frac{K}{Js^2 + (F + KK_1)s + KK_2}$$

which is the **same result** obtained earlier, with the first approach

Error

Error

For an open loop system (that is, with no feedback) the definition of error is:

$$E(s) = R(s) - Y(s)$$



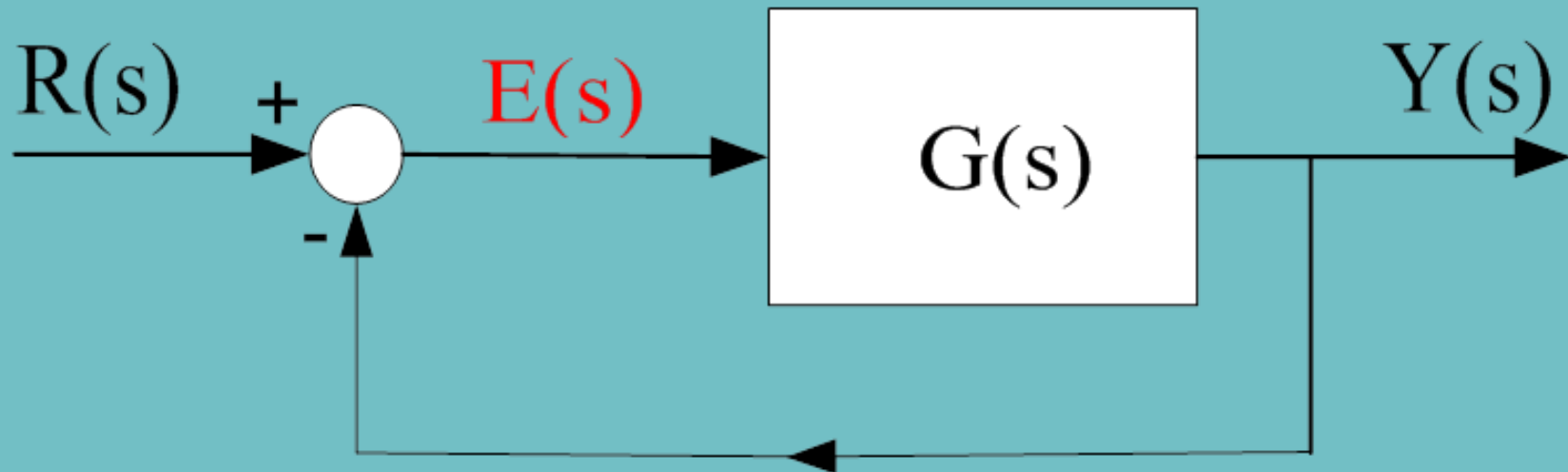
$$E(s) = R(s) - Y(s)$$

Error

unit feedback

here, the
error is also:

$$E(s) = R(s) - Y(s)$$

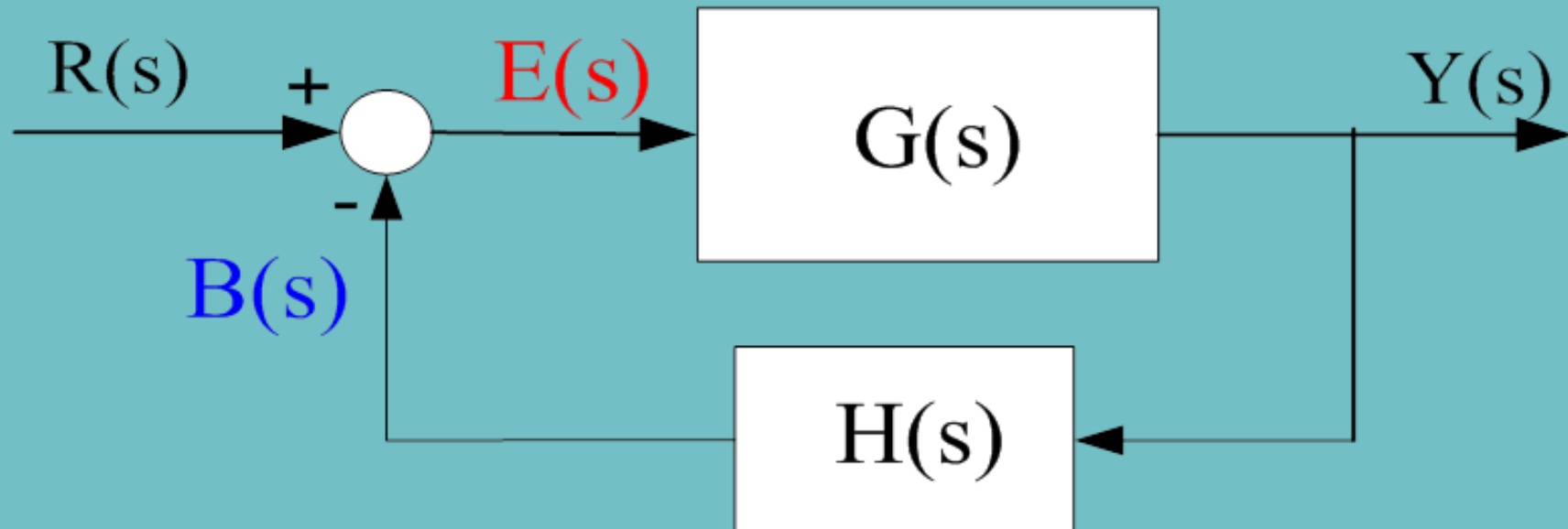


Error

non unit feedback

the error becomes:

$$E(s) = R(s) - B(s)$$

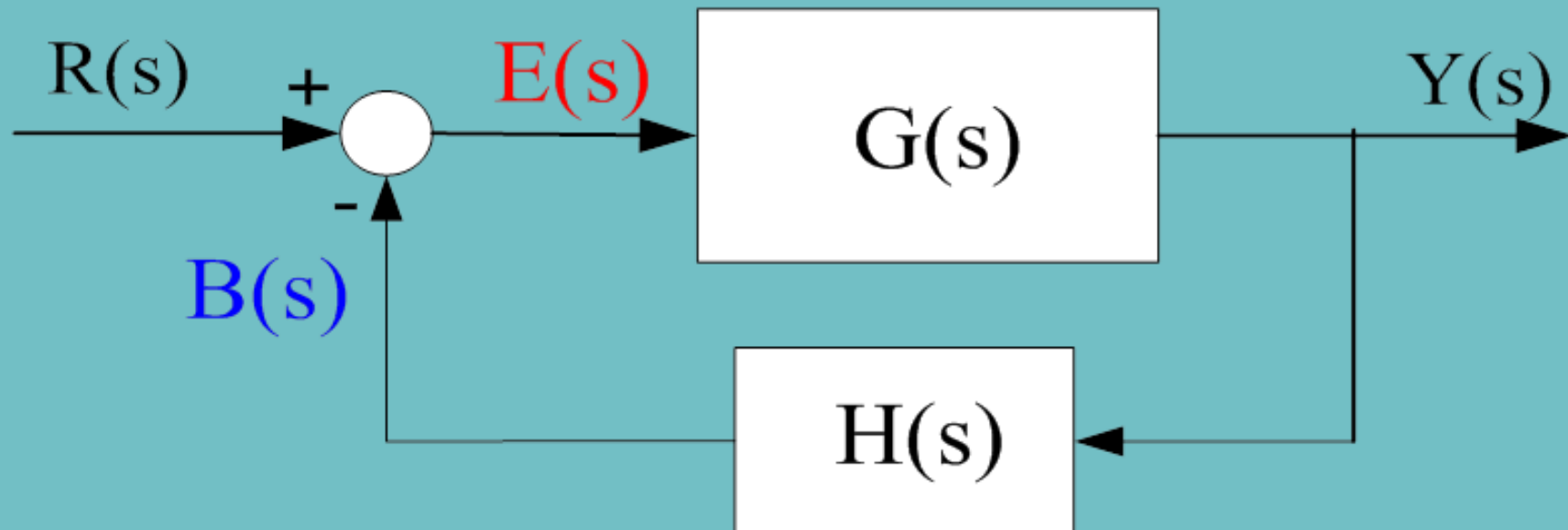


that is:

error:

$$E(s) = R(s) - Y(s)H(s)$$

$B(s)$



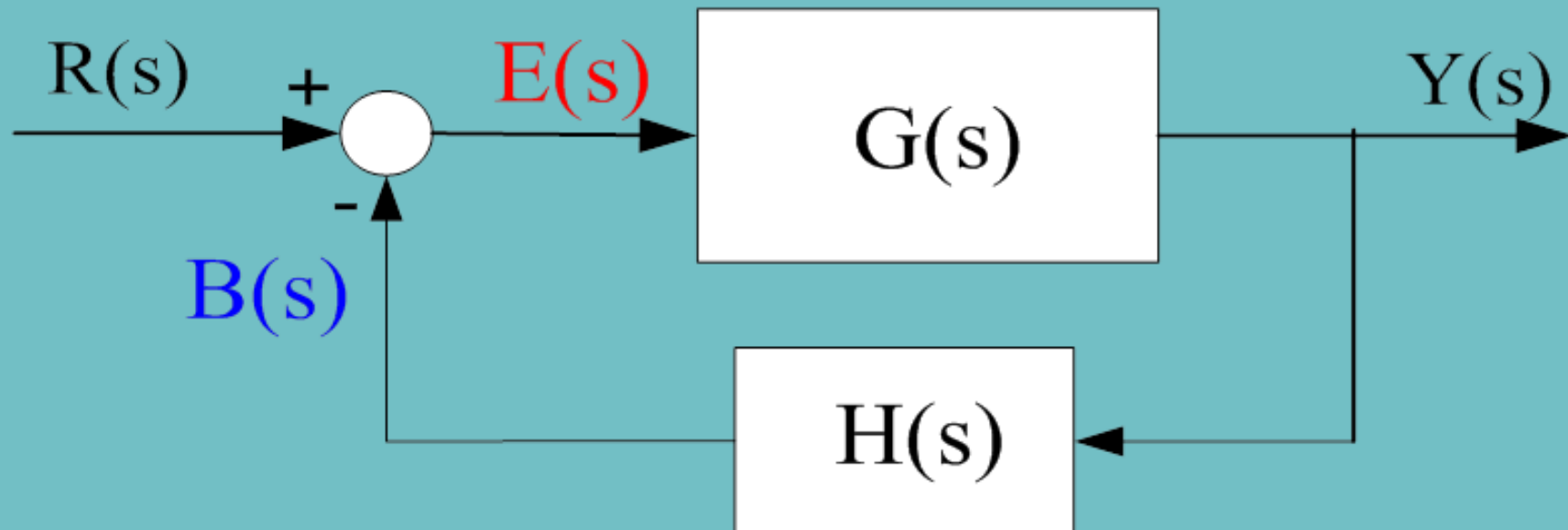
but:

$$Y(s) = G(s) \cdot E(s)$$

thus:



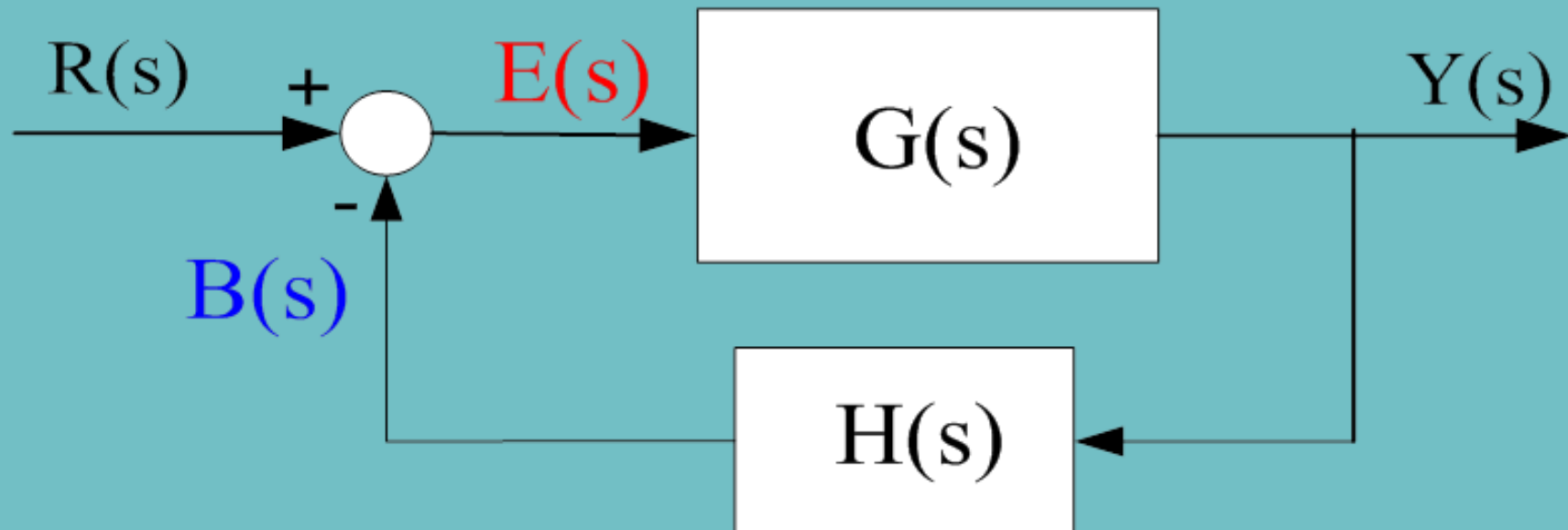
$$E(s) = R(s) - \overbrace{G(s)E(s)H(s)}^{Y(s)}$$



hence:

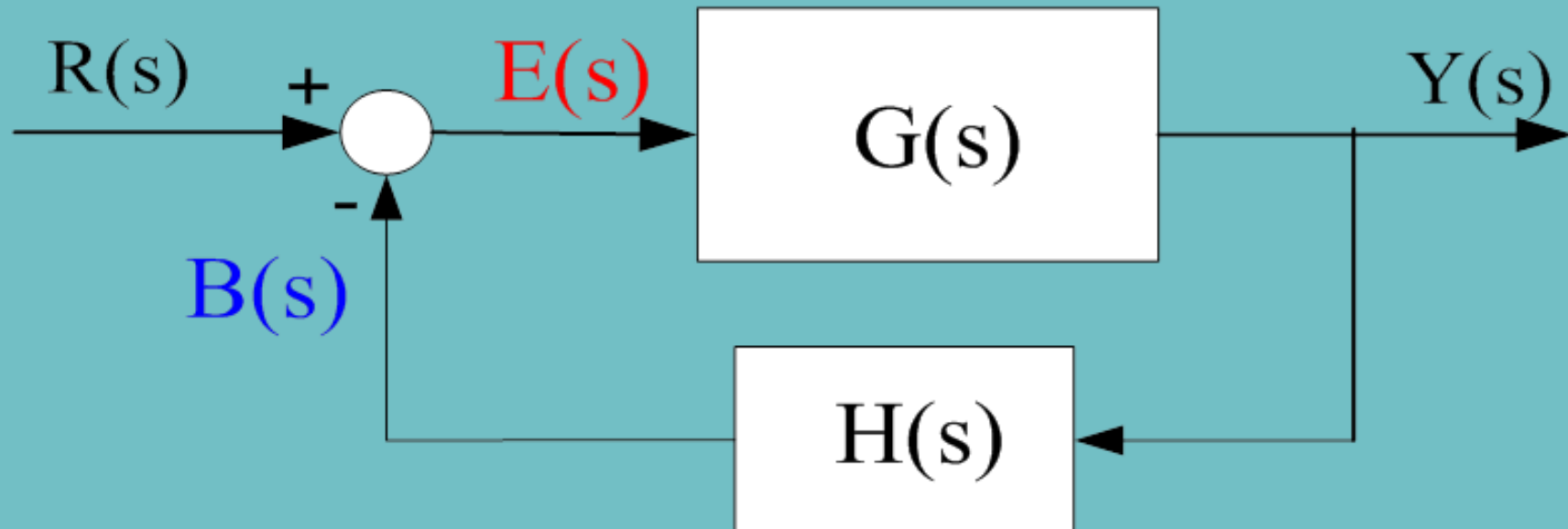


$$E(s) [1 + G(s)H(s)] = R(s)$$



and the expression for the 'error' is:

$$E(s) = \frac{R(s)}{[1 + G(s)H(s)]}$$



Steady state error
Steady state output

Initial Value Theorem:


$$x(0) = \lim_{t \rightarrow 0} x(t) = \lim_{s \rightarrow \infty} s \cdot X(s) \quad (\text{IVT})$$

Final Value Theorem:


$$x(\infty) = \lim_{t \rightarrow \infty} x(t) = \lim_{s \rightarrow 0} s \cdot X(s) \quad (\text{FVT})$$

Initial Value Theorem:



$$x(0) = \lim_{s \rightarrow \infty} s \cdot X(s) \quad (\text{IVT})$$

Final Value Theorem:



$$x(\infty) = \lim_{s \rightarrow 0} s \cdot X(s) \quad (\text{FVT})$$

Example 3:

$$Y(s) = \frac{3s - 2}{s(s + 5)}$$

IVT

$$\begin{aligned} y(0) &= \lim_{s \rightarrow \infty} s \cdot Y(s) \\ &= \lim_{s \rightarrow \infty} \cancel{s} \cdot \frac{3s - 2}{\cancel{s}(s + 5)} \\ &= \lim_{s \rightarrow \infty} \frac{3s - 2}{(s + 5)} \\ &= 3 \end{aligned}$$

FVT

$$\begin{aligned} y(\infty) &= \lim_{s \rightarrow 0} s \cdot Y(s) \\ &= \lim_{s \rightarrow 0} \cancel{s} \cdot \frac{3s - 2}{\cancel{s}(s + 5)} \\ &= \lim_{s \rightarrow 0} \frac{3s - 2}{(s + 5)} \\ &= -2/5 \end{aligned}$$

Example 4:

$$E(s) = \frac{2s}{s^2 - 4s + 3}$$

IVT

$$\begin{aligned} e(0) &= \lim_{s \rightarrow \infty} s \cdot E(s) \\ &= \lim_{s \rightarrow \infty} \frac{2s^2}{s^2 - 4s + 3} \\ &= 2 \end{aligned}$$

FVT

$$\begin{aligned} e(\infty) &= \lim_{s \rightarrow 0} s \cdot E(s) \\ &= \lim_{s \rightarrow 0} \frac{2s^2}{s^2 - 4s + 3} \\ &= 0 \end{aligned}$$

Steady state error:

$$e_{ss} = \lim_{t \rightarrow \infty} e(t)$$



$$e_{ss} = \lim_{t \rightarrow \infty} e(t) = \lim_{s \rightarrow 0} s \cdot E(s) \quad (\text{FVT})$$

$$e_{ss} = \lim_{s \rightarrow 0} s \cdot E(s) = \lim_{s \rightarrow 0} \frac{s \cdot R(s)}{[1 + G(s)H(s)]}$$

Steady state error:

$$e_{ss} = \lim_{s \rightarrow 0} \frac{s \cdot R(s)}{[1 + G(s)H(s)]}$$

Steady state output:

$$y_{ss} = \lim_{t \rightarrow \infty} y(t)$$

 $y_{ss} = \lim_{t \rightarrow \infty} y(t) = \lim_{s \rightarrow 0} s \cdot Y(s) \quad (\text{FVT})$

However,
we know that

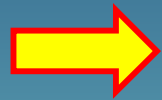
$$\frac{Y(s)}{R(s)} = \frac{G(s)}{1 + G(s)H(s)}$$

Steady state output:

hence,

$$Y(s) = \frac{G(s)}{[1 + G(s)H(s)]} \cdot R(s)$$

$$y_{ss} = \lim_{s \rightarrow 0} s \cdot Y(s) =$$

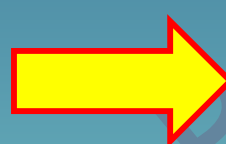


$$= \lim_{s \rightarrow 0} s \cdot \frac{G(s)}{[1 + G(s)H(s)]} \cdot R(s)$$

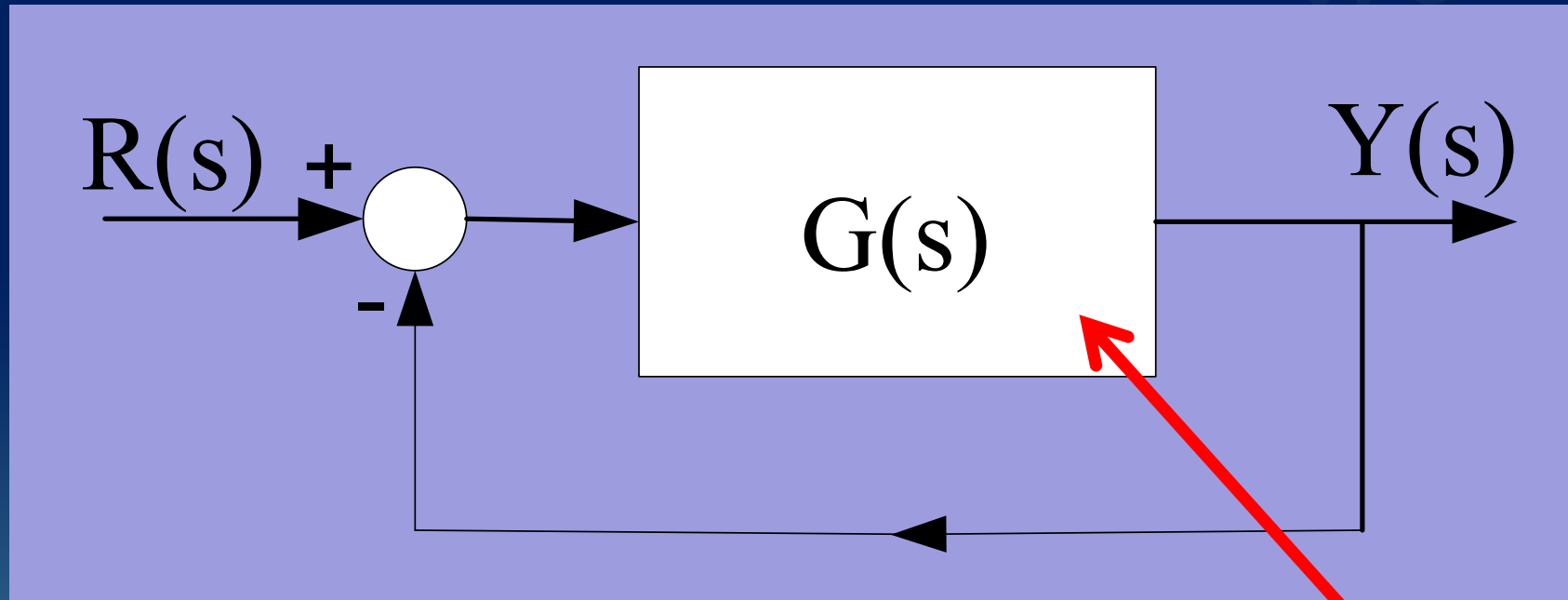
Steady state output:

and then,

$$y_{ss} = \lim_{s \rightarrow 0} s \cdot Y(s) = \lim_{s \rightarrow 0} \frac{s G(s) R(s)}{[1 + G(s)H(s)]}$$

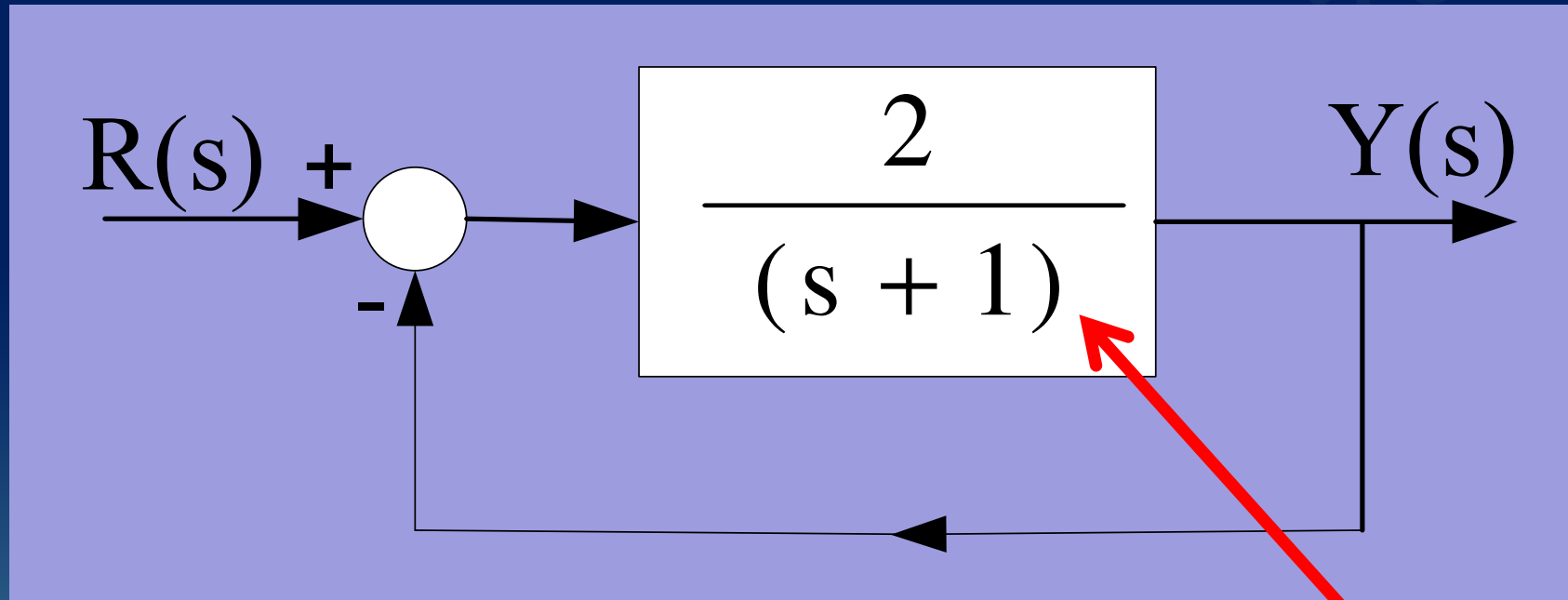

$$y_{ss} = \lim_{s \rightarrow 0} \frac{s G(s) R(s)}{[1 + G(s)H(s)]}$$

Example 5:



$$G(s) = \frac{2}{(s+1)}$$

Example 5: (continued)



input $r(t)$:

$$r(t) = u_1(t)$$

$r(t)$ = unit step

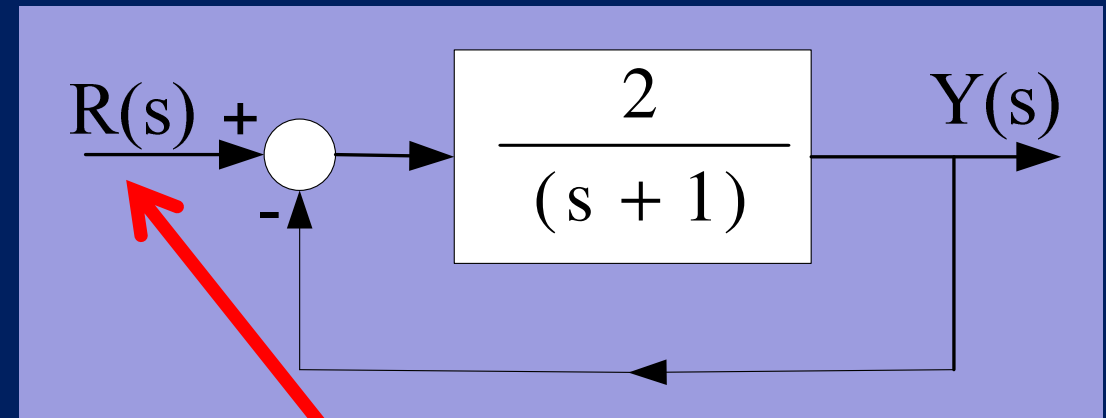
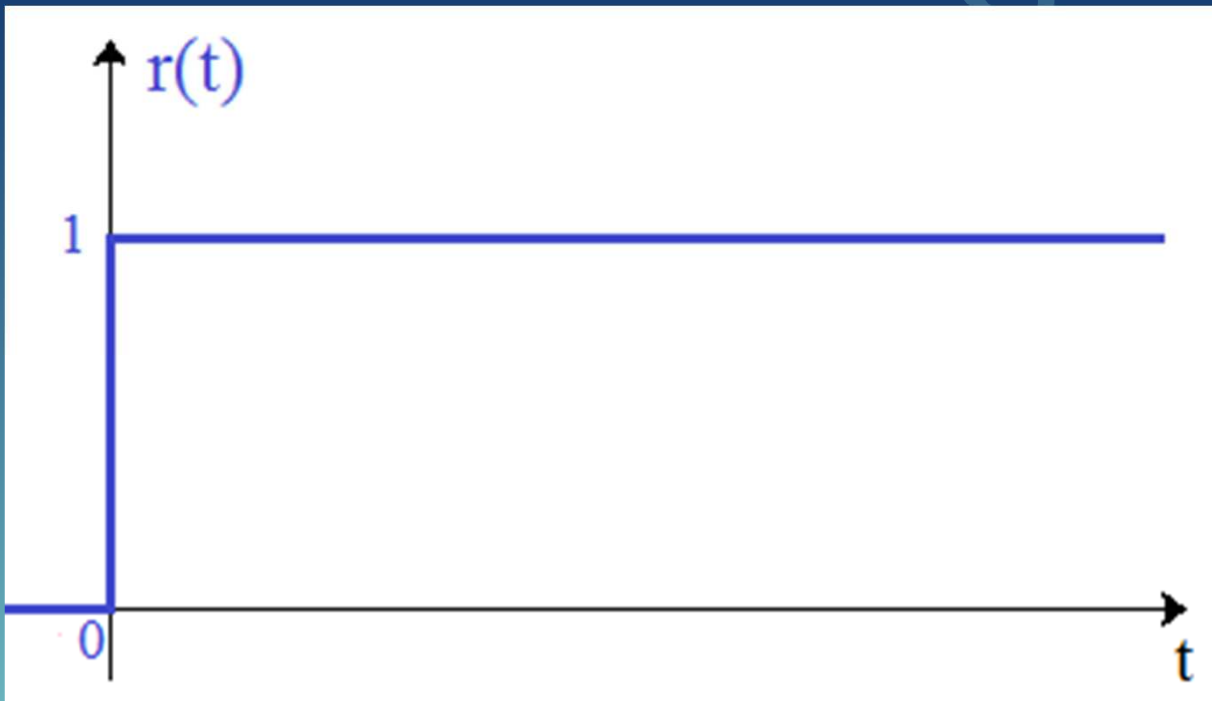
$$G(s) = \frac{2}{(s+1)}$$

Example 5: (continued)

input $r(t)$:

$$r(t) = u_1(t)$$

$r(t)$ = unit step

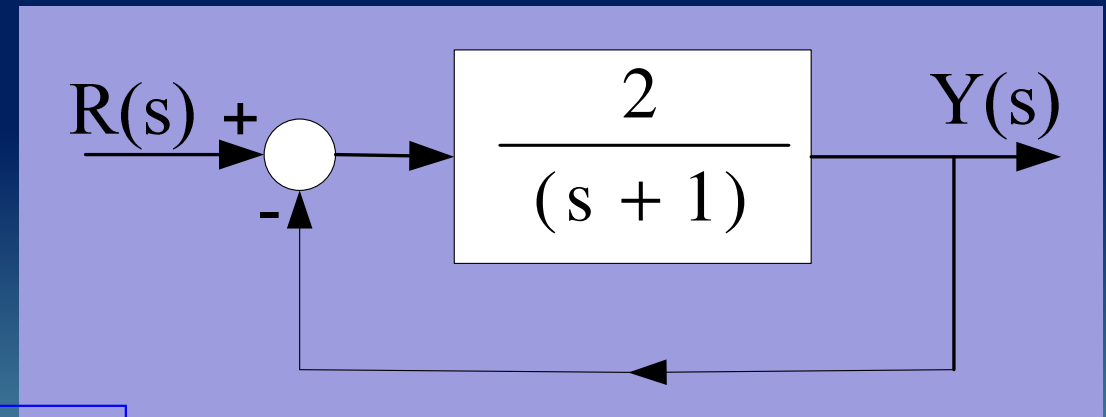


 $R(s) = \frac{1}{s}$

Example 5: (continued)

$$R(s) = \frac{1}{s}$$

output $y(t)$

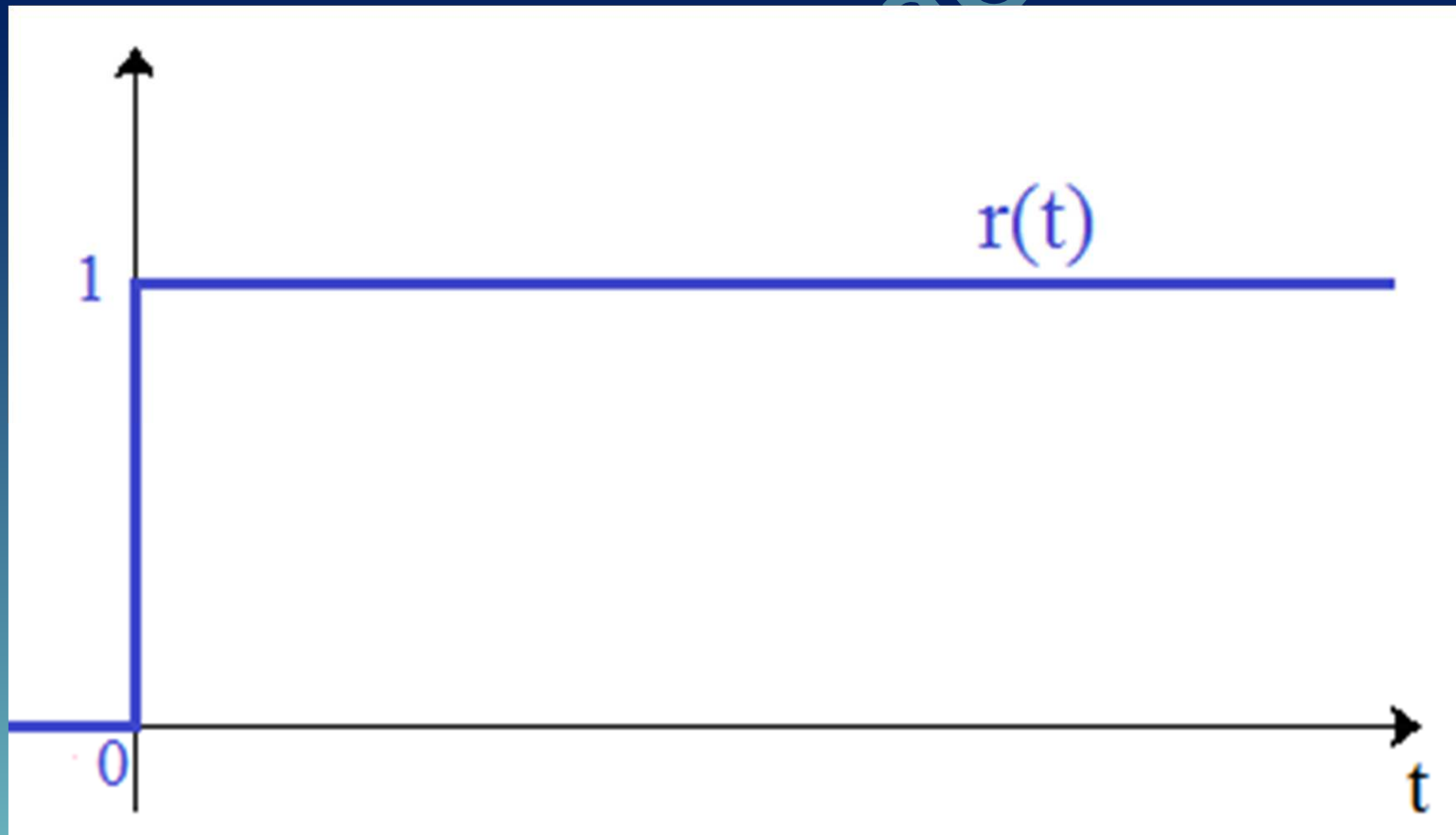
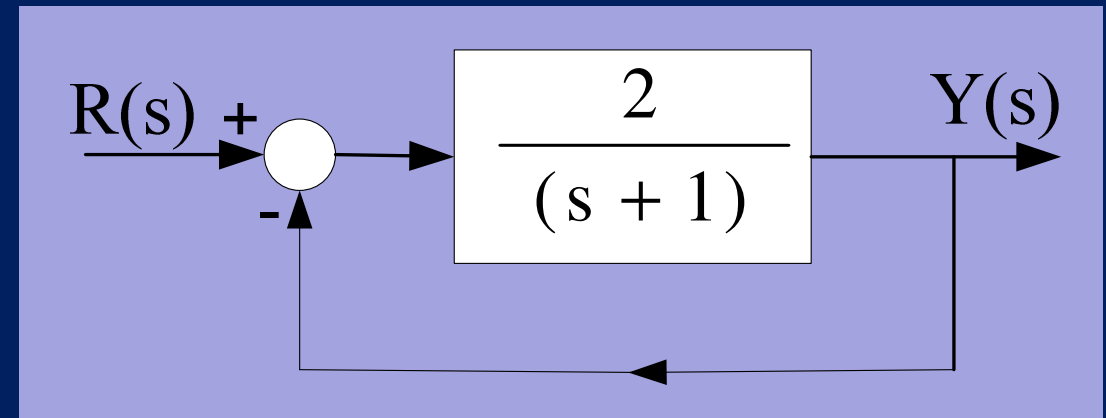


$$\begin{aligned} Y(s) &= \frac{G(s)}{[1 + G(s)H(s)]} \cdot R(s) \\ &= \frac{\frac{2}{(s+1)}}{\left[1 + \frac{2}{(s+1)}\right]} \cdot \frac{1}{s} \\ &= \frac{2}{s(s+3)} \end{aligned}$$

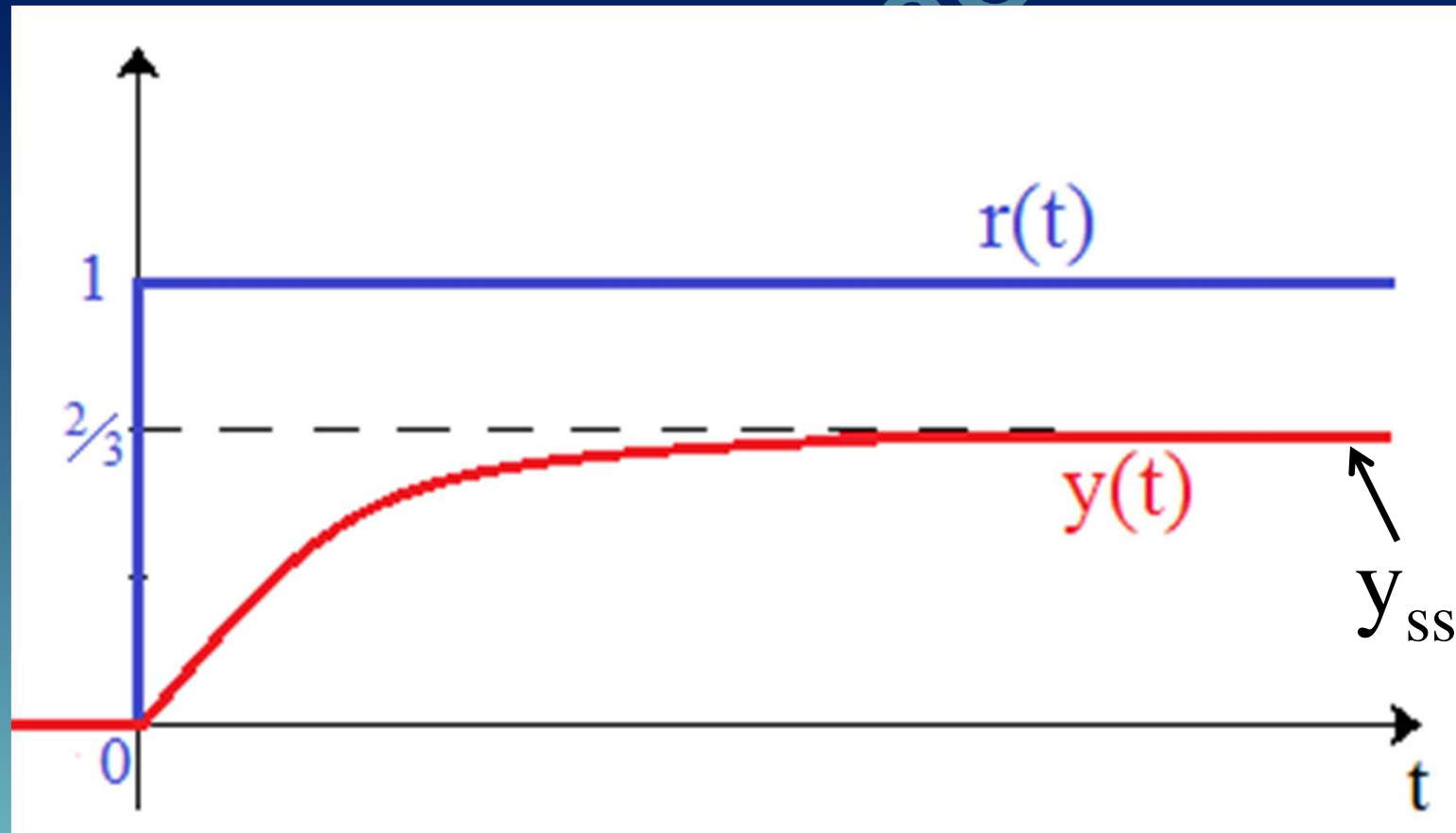
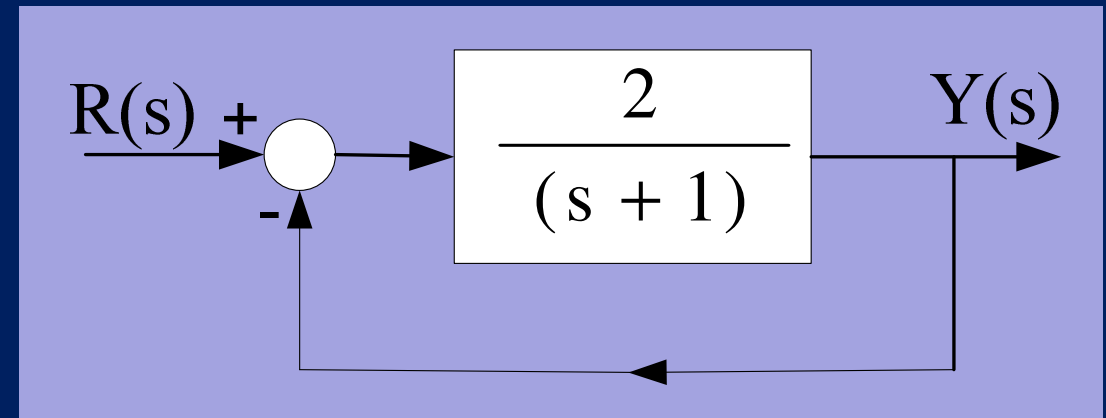
output in
steady state y_{ss}

$$\begin{aligned} y_{ss} &= \lim_{s \rightarrow 0} s \cdot Y(s) = \\ &= \lim_{s \rightarrow 0} \cancel{s} \cdot \frac{2}{\cancel{s}(s+3)} \\ &= 2/3 \end{aligned}$$

Example 5: (continued)



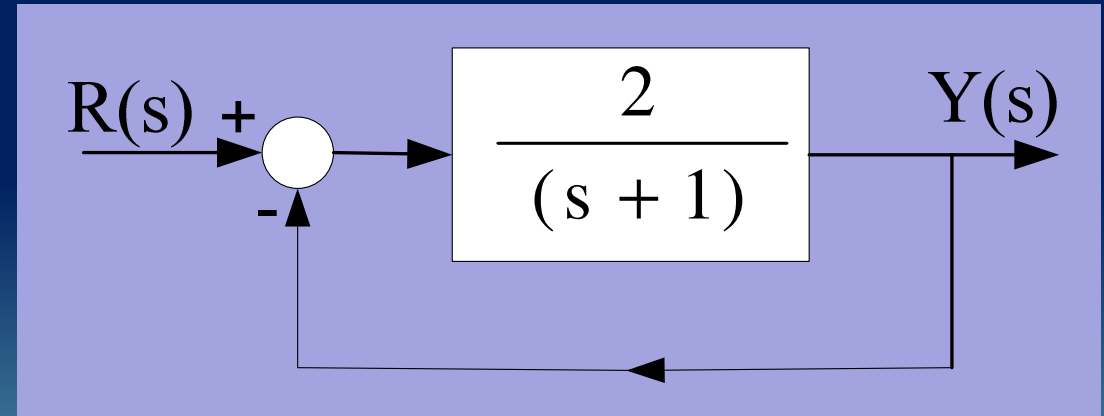
Example 5: (continued)



$$y_{ss} = 2/3$$

Example 5:
(continued)

$$R(s) = \frac{1}{s}$$



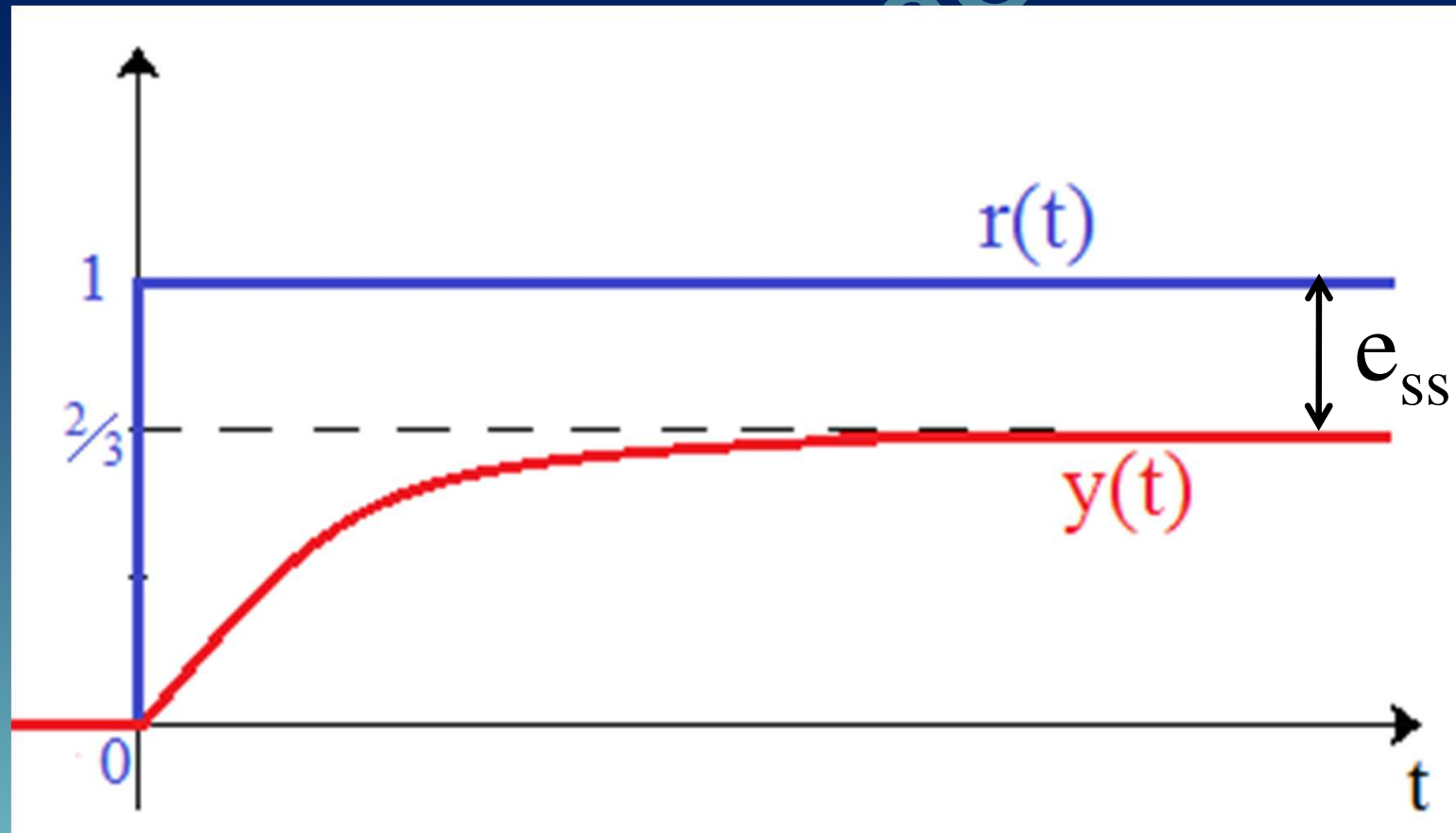
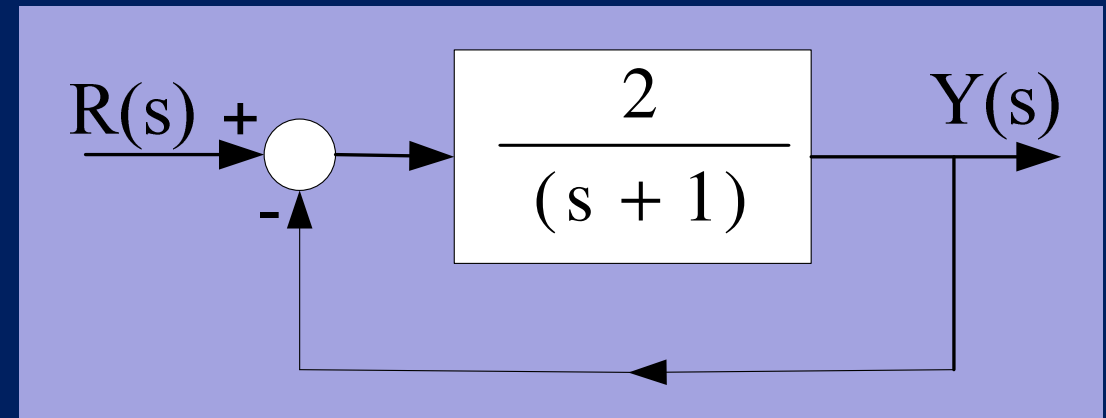
error $e(t)$

$$\begin{aligned} E(s) &= \frac{R(s)}{[1 + G(s)H(s)]} \\ &= \frac{1/s}{\left[1 + \frac{2}{(s+1)}\right]} \\ &= \frac{(s+1)}{s(s+3)} \end{aligned}$$

error in
steady state e_{ss}

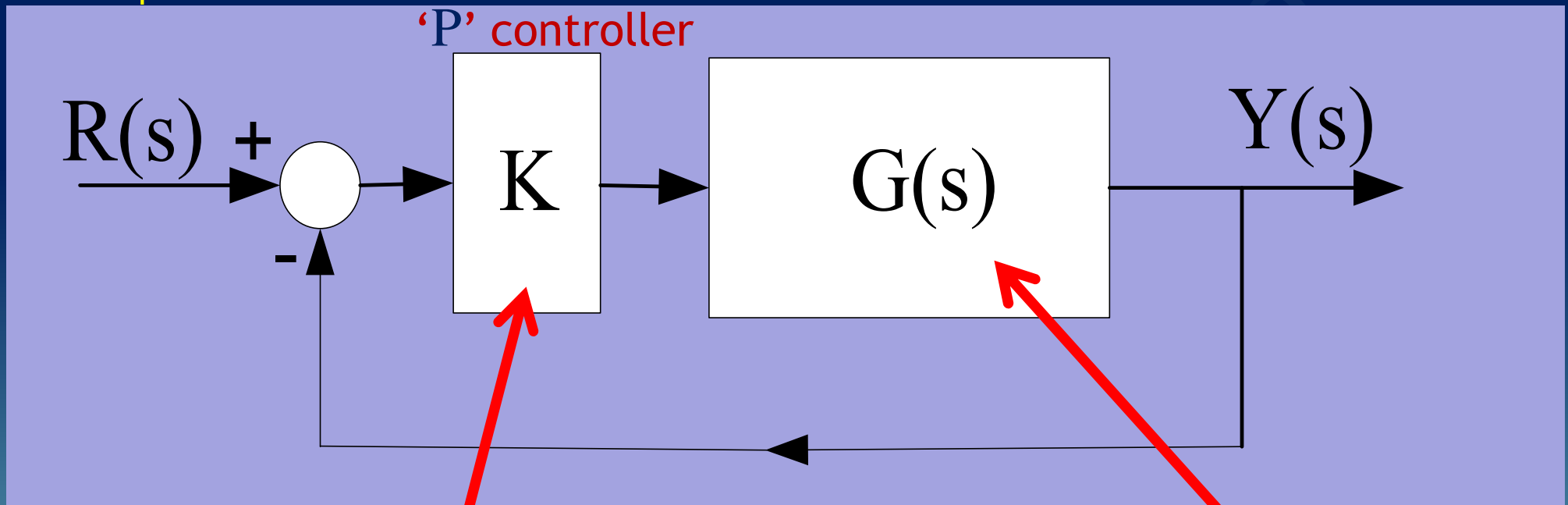
$$\begin{aligned} e_{ss} &= \lim_{s \rightarrow 0} s \cdot E(s) = \\ &= \lim_{s \rightarrow 0} s \cdot \frac{(s+1)}{s(s+3)} \\ &= 1/3 \end{aligned}$$

Example 5: (continued)



$$e_{ss} = 1/3$$

Example 6:

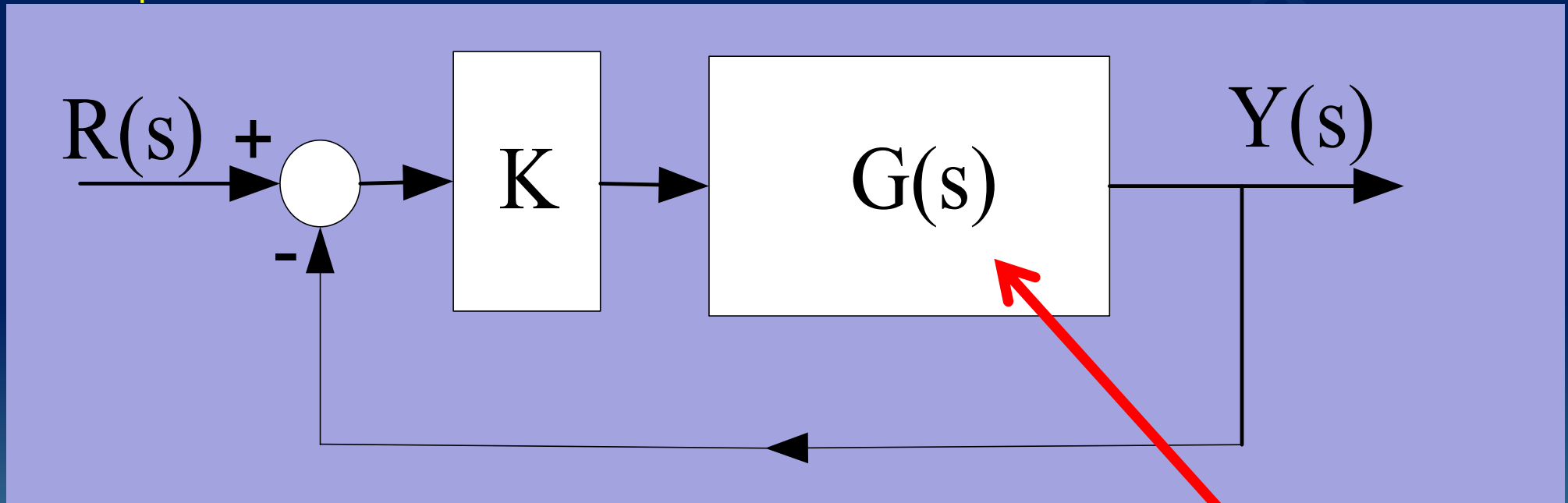


But now we have K , namely,
a “*proportional controller*”
or the “*type P controller*”

$$G(s) = \frac{2}{(s+1)}$$

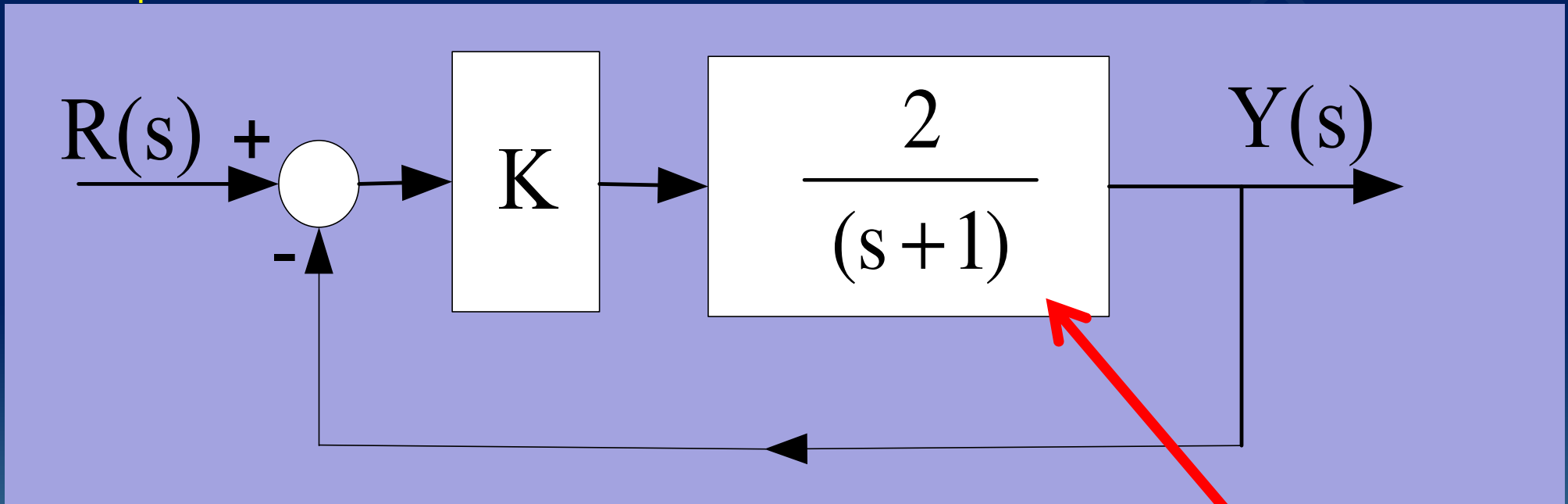
the same as in the
previous example

Example 6: (continued)



$$G(s) = \frac{2}{(s+1)}$$

Example 6: (continued)



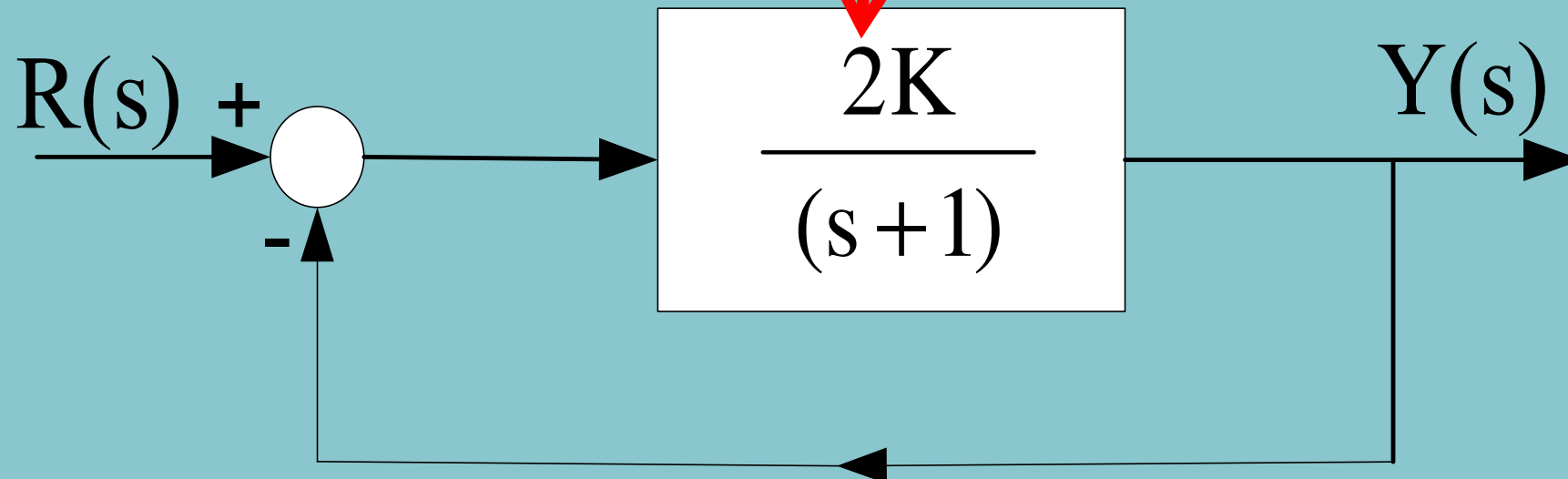
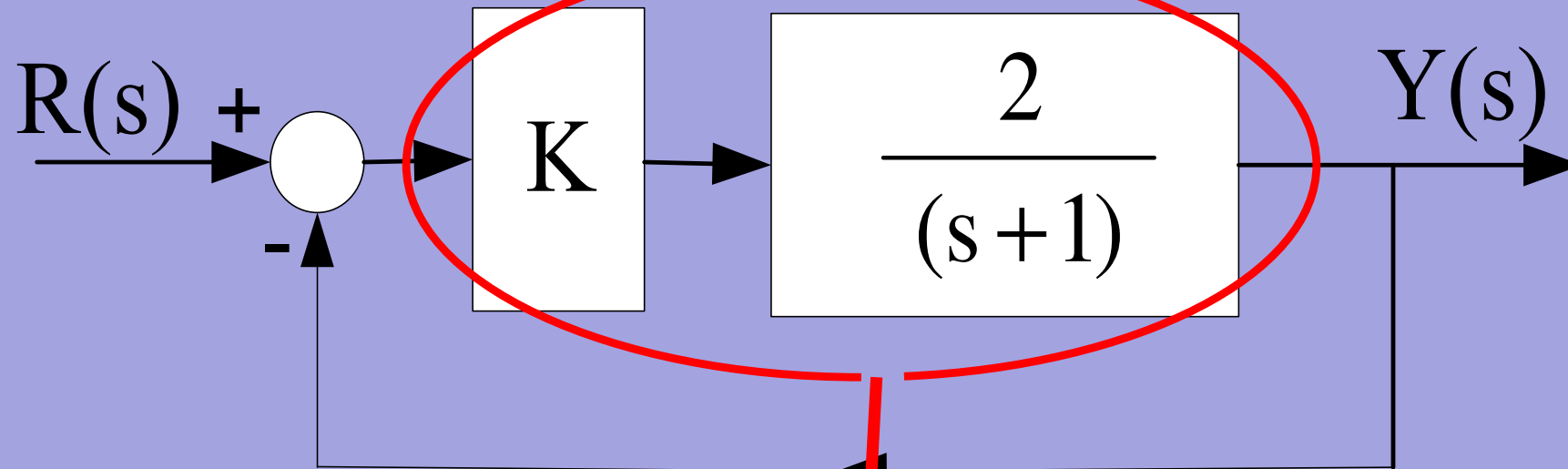
input $r(t)$:

$$r(t) = u_1(t)$$

$r(t)$ = unit step
(again)

$$G(s) = \frac{2}{(s+1)}$$

Example 6: (continued)

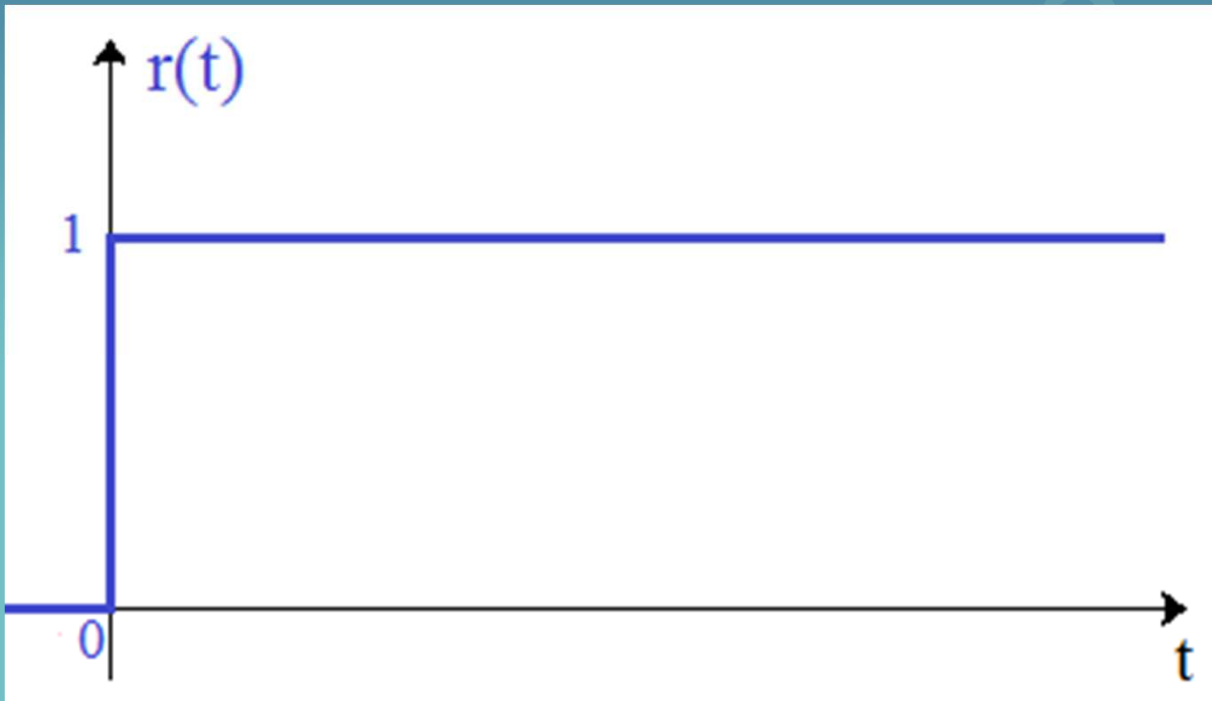
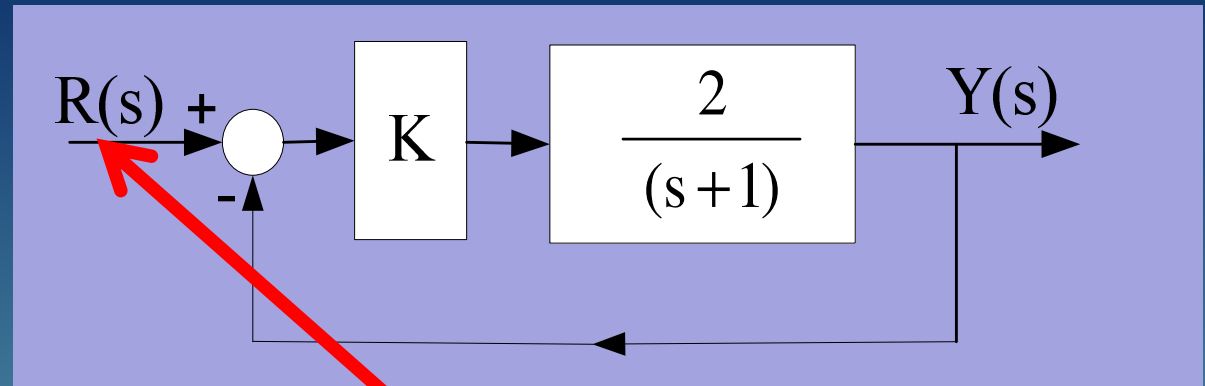


Example 6: (continued)

input $r(t)$:

$$r(t) = u_1(t)$$

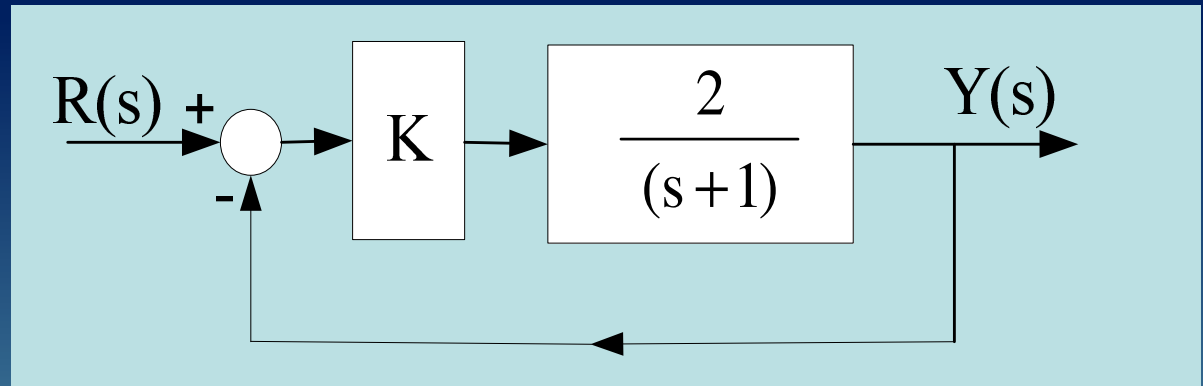
$r(t)$ = unit step



$$R(s) = \frac{1}{s}$$

Example 6: (continued)

$$R(s) = \frac{1}{s}$$

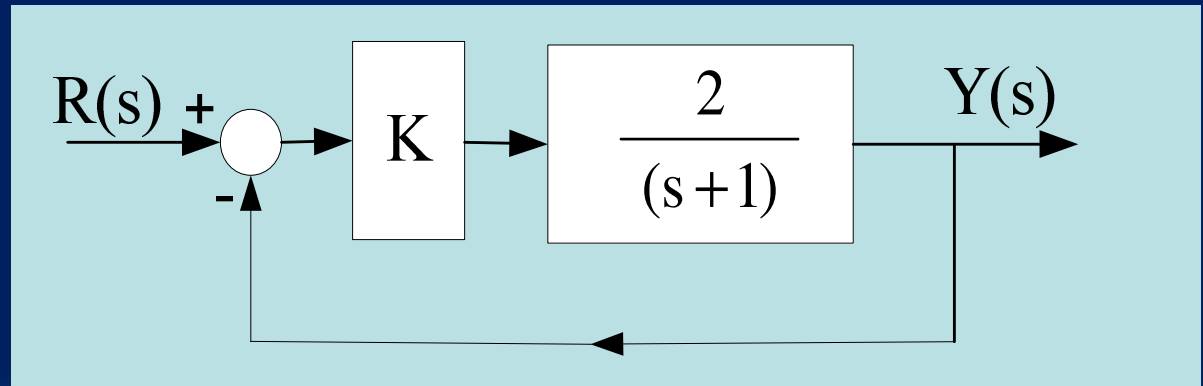
output $y(t)$ 

$$\begin{aligned}
 Y(s) &= \frac{G(s)}{[1 + G(s)H(s)]} \cdot R(s) \\
 &= \frac{\frac{2K}{(s+1)}}{\left[1 + \frac{2K}{(s+1)}\right]} \cdot \frac{1}{s} \\
 &= \frac{2K}{s(s+2K+1)}
 \end{aligned}$$

output in
steady state y_{ss}

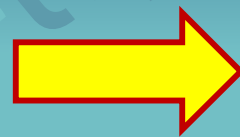
$$\begin{aligned}
 y_{ss} &= \lim_{s \rightarrow 0} s \cdot Y(s) = \\
 &= \lim_{s \rightarrow 0} \cancel{s} \cdot \frac{2K}{\cancel{s}(s+2K+1)} \\
 &= \frac{2K}{(2K+1)}
 \end{aligned}$$

Example 6: (continued)



output in steady state y_{ss}

if K is large enough

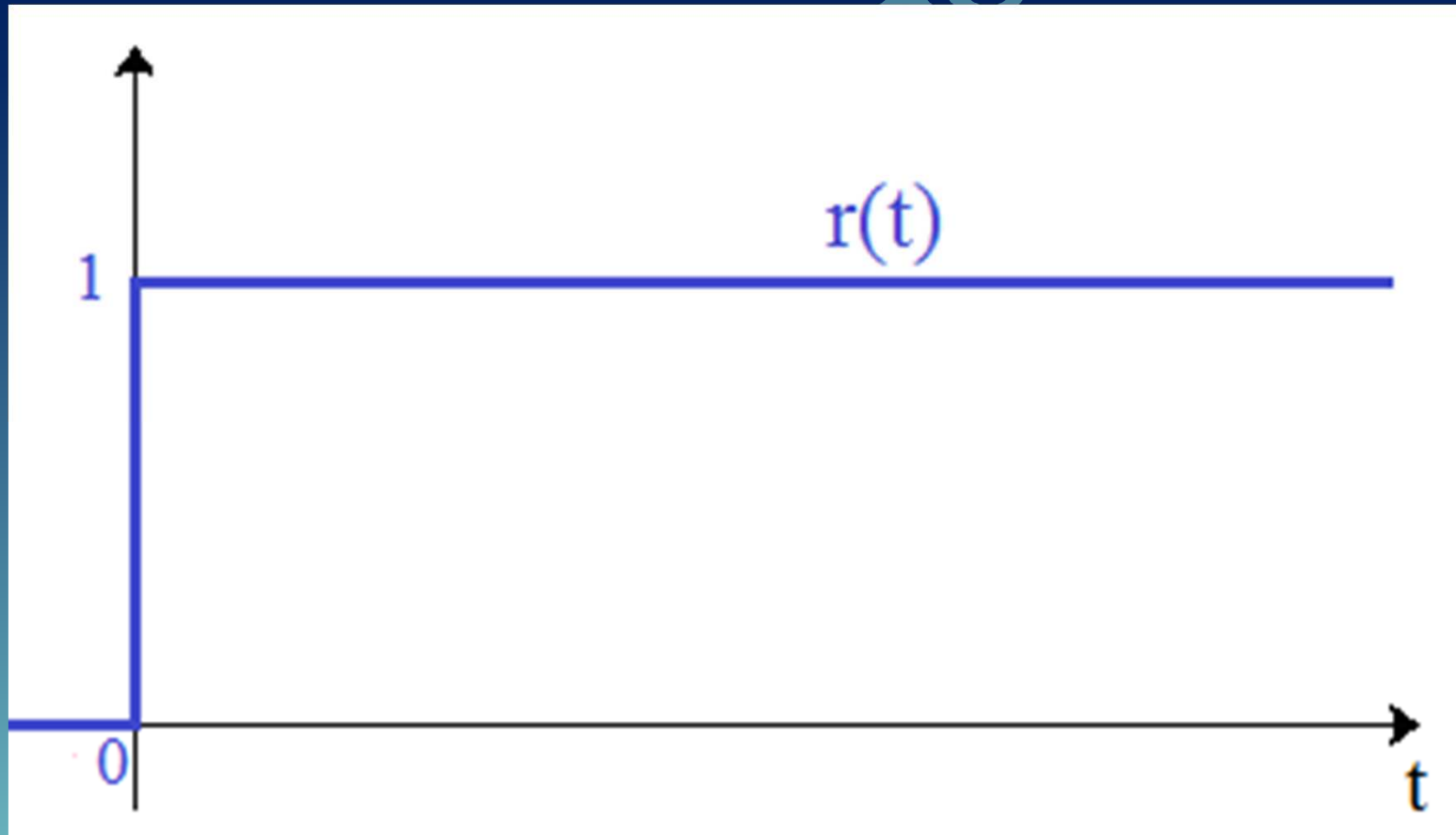
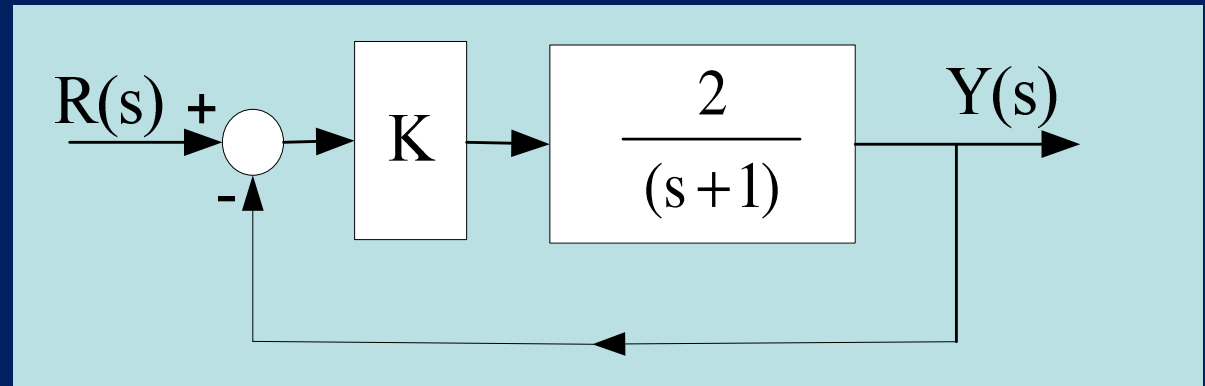


$$y_{ss} = \frac{2K}{(2K+1)} \cong 1$$

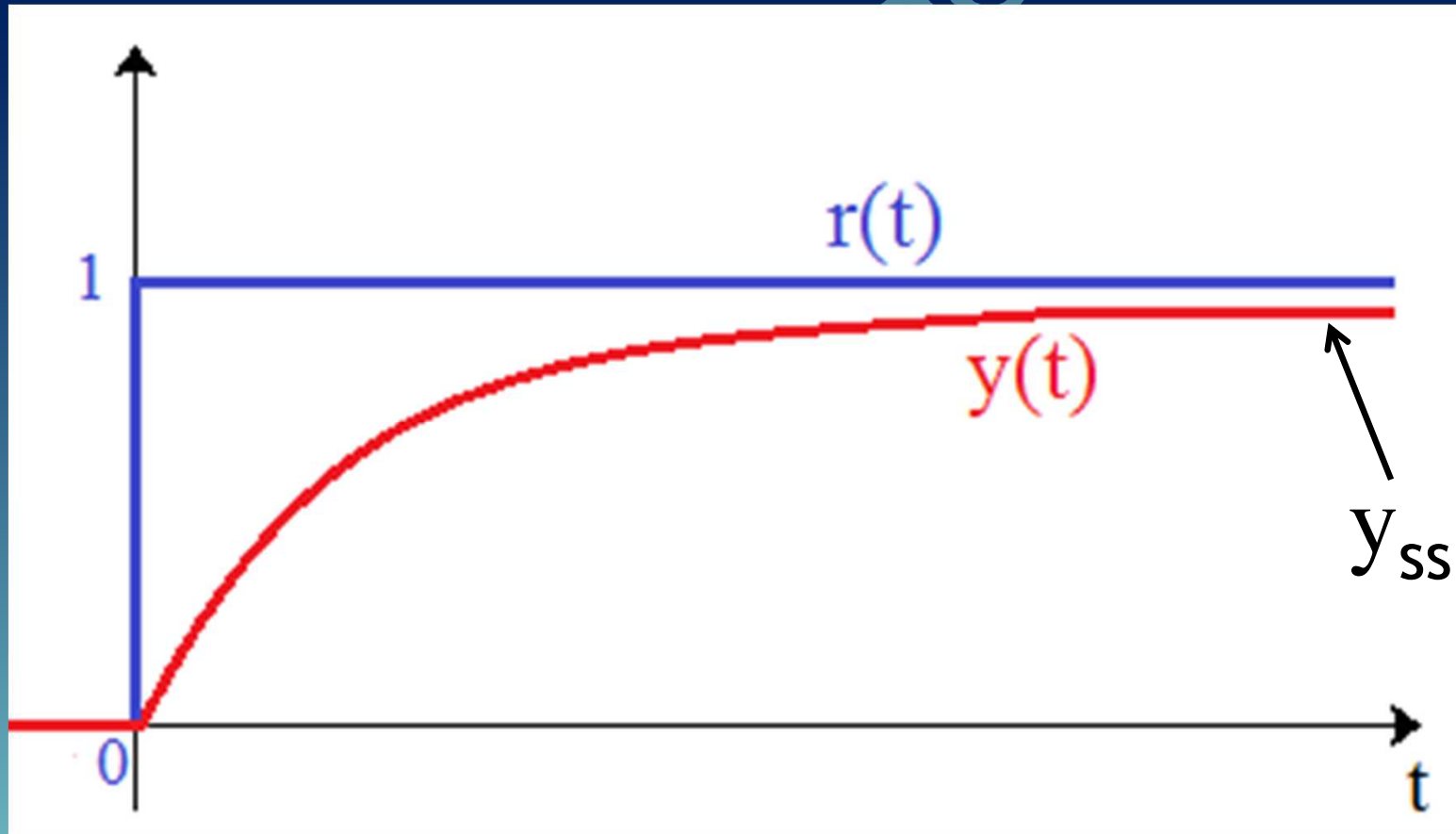
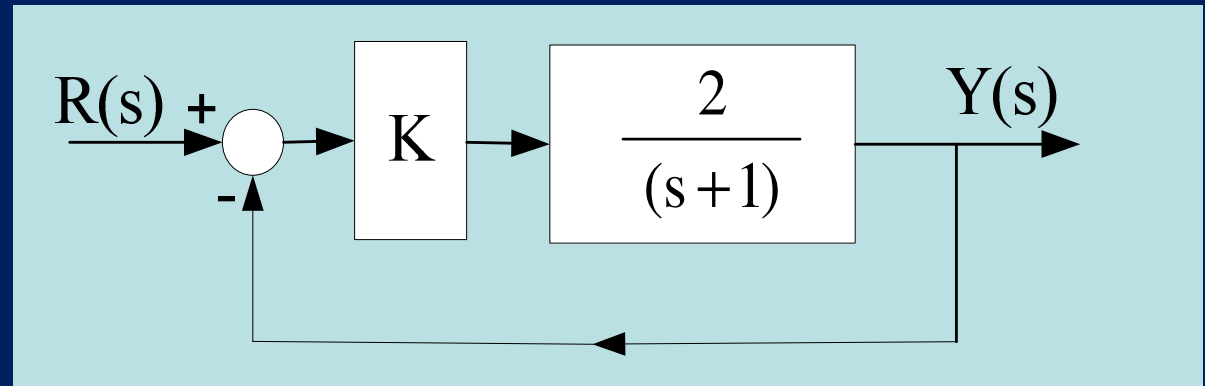
or

$$y_{ss} \rightarrow 1 \quad \text{when} \quad K \rightarrow \infty$$

Example 6: (continued)

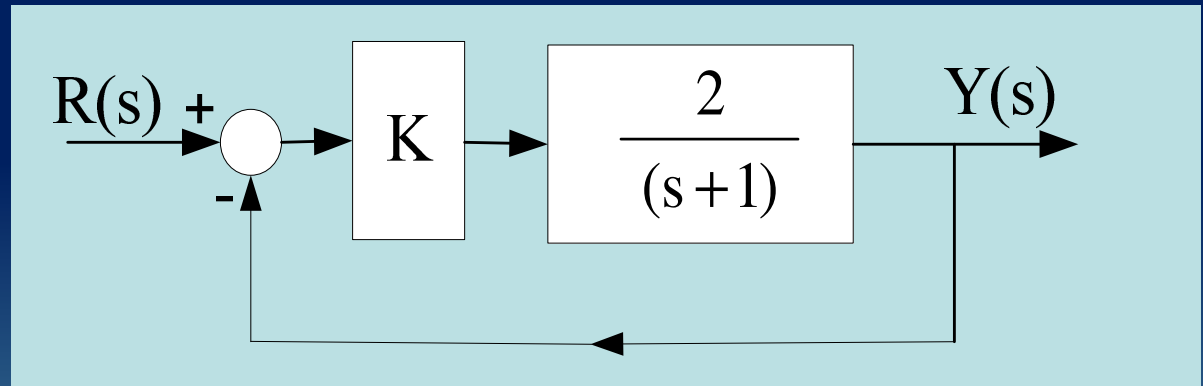


Example 6: (continued)



Example 6: (continued)

$$R(s) = \frac{1}{s}$$

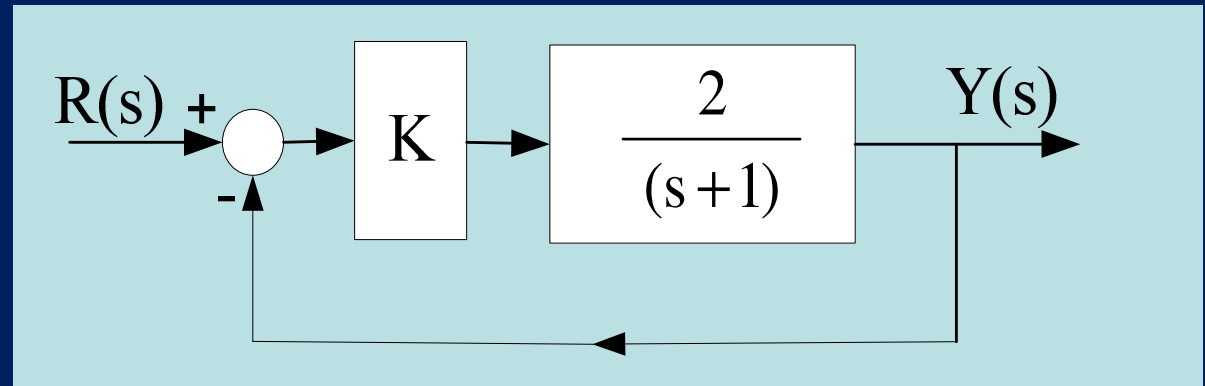
error $e(t)$

$$\begin{aligned} E(s) &= \frac{R(s)}{[1 + G(s)H(s)]} \\ &= \frac{1/s}{\left[1 + \frac{2K}{(s+1)}\right]} \\ &= \frac{(s+1)}{s(s+2K+1)} \end{aligned}$$

error in
steady state e_{ss}

$$\begin{aligned} e_{ss} &= \lim_{s \rightarrow 0} s \cdot E(s) = \\ &= \lim_{s \rightarrow 0} \cancel{s} \cdot \frac{(s+1)}{\cancel{s}(s+2K+1)} \\ &= \frac{1}{(2K+1)} \end{aligned}$$

Example 6: (continued)



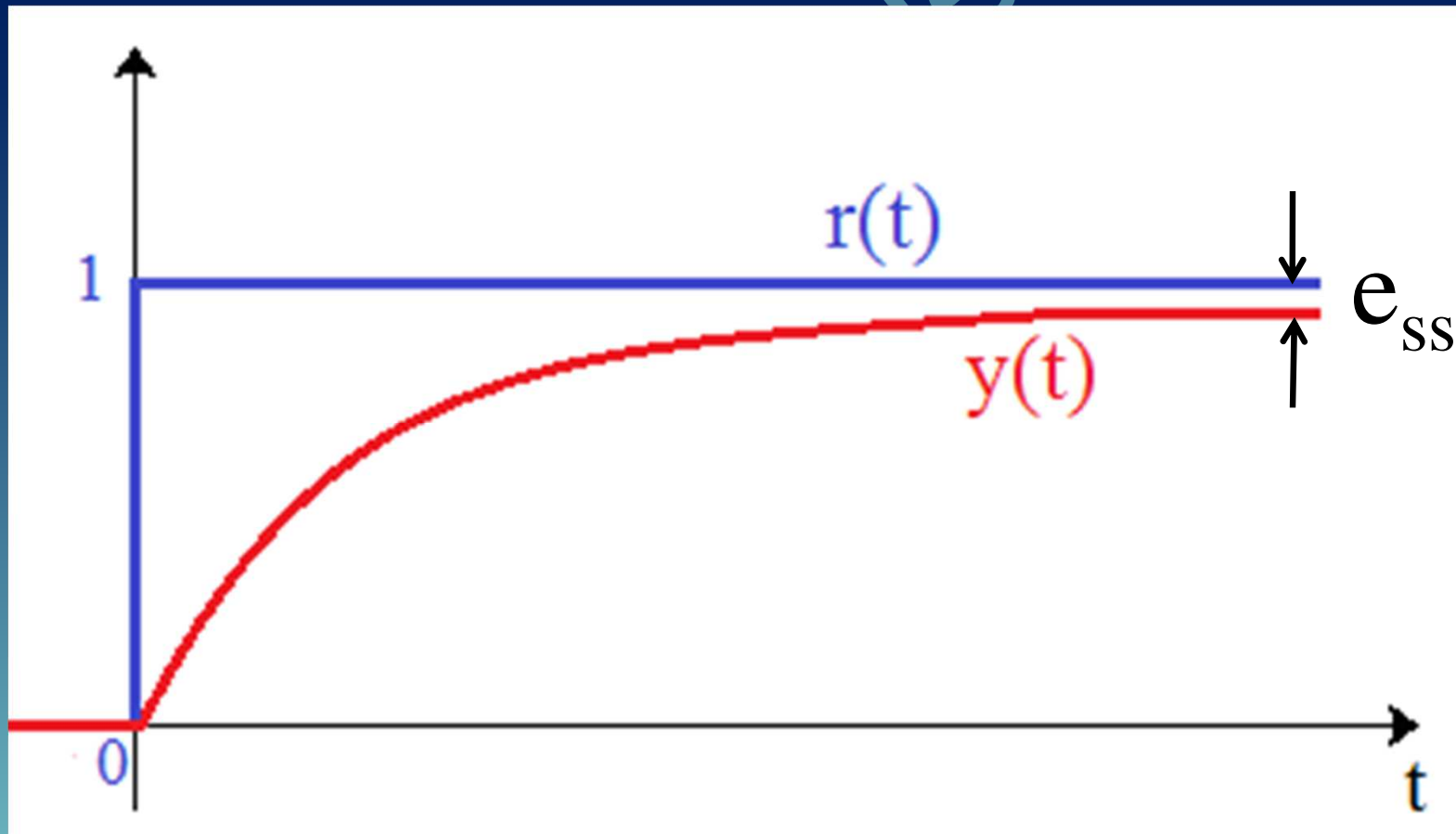
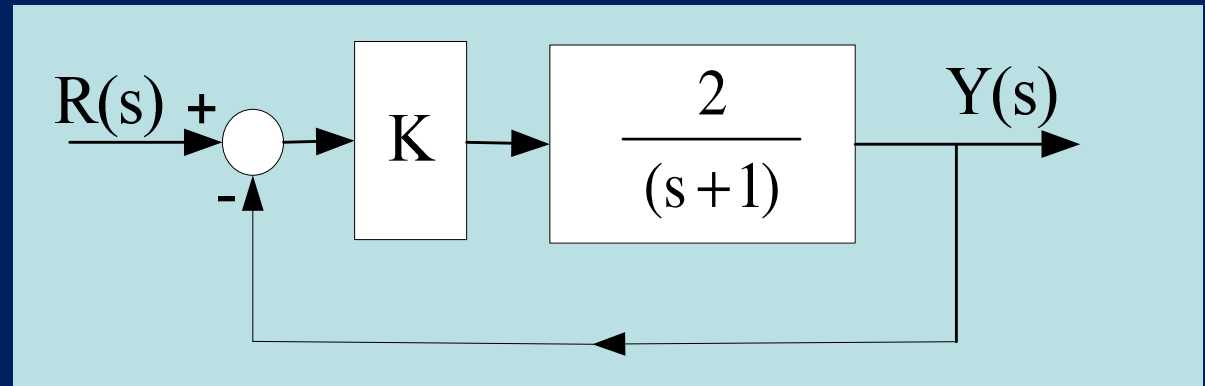
error in *steady state* e_{ss}

if K is large enough $\Rightarrow e_{ss} = \frac{1}{(2K + 1)} \cong 0$

or

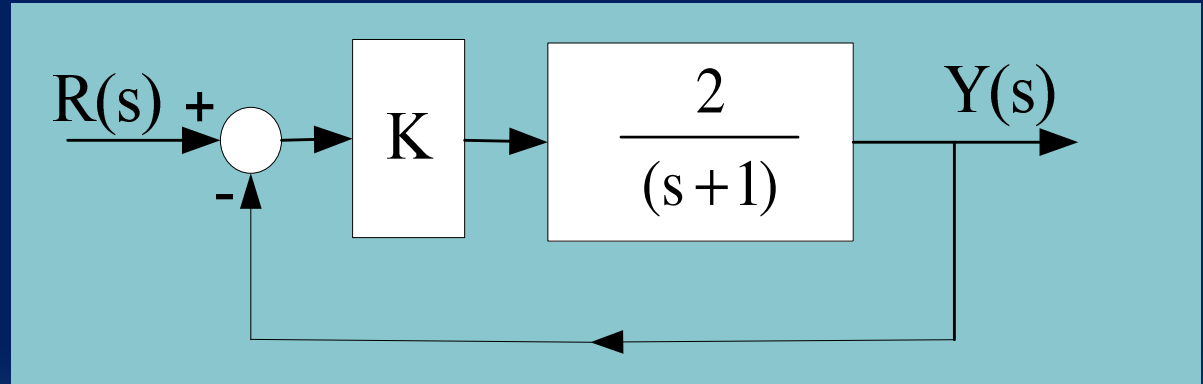
$$e_{ss} \rightarrow 0 \quad \text{when} \quad K \rightarrow \infty$$

Example 6: (continued)



$e_{ss} \rightarrow 0$

Example 6: (continued)



which is the value that we should adjust K such that the *steady state error*

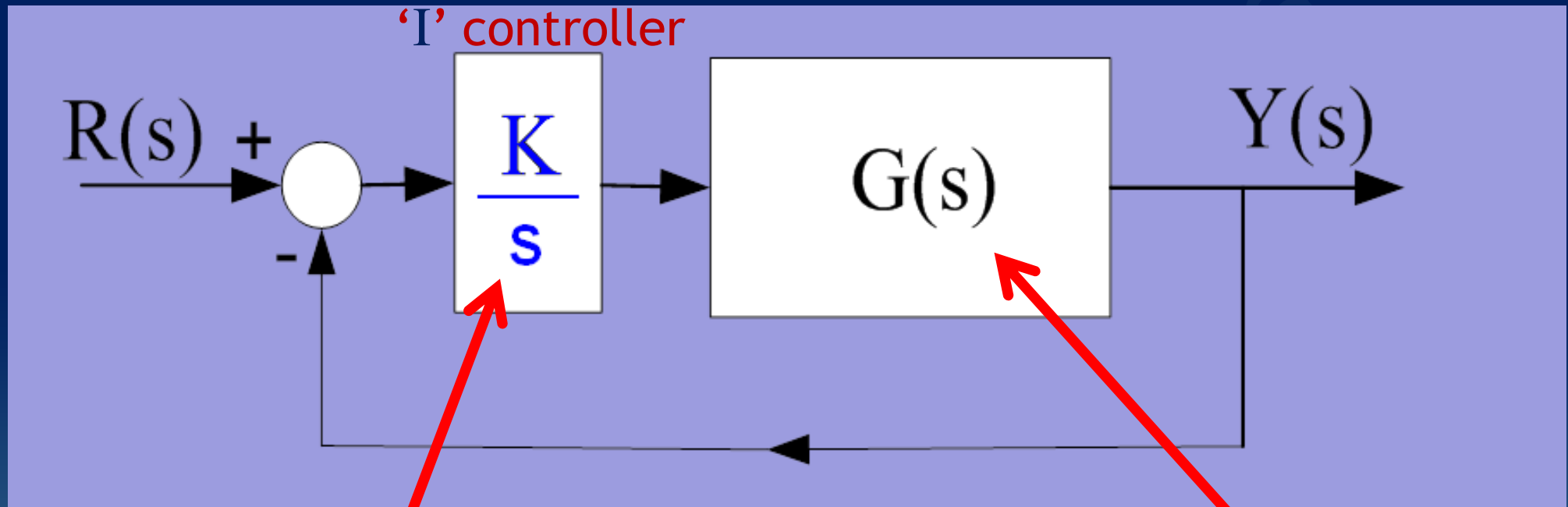
$$e_{ss} < 0,01$$

$$e_{ss} = \frac{1}{(2K+1)} < 0,01 = \frac{1}{100} \quad \Rightarrow \quad 100 < (2K+1)$$

$$\Rightarrow K > 99/2 \quad \Rightarrow \quad K > 49,5$$

we should choose $K > 49,5$

Example 7:



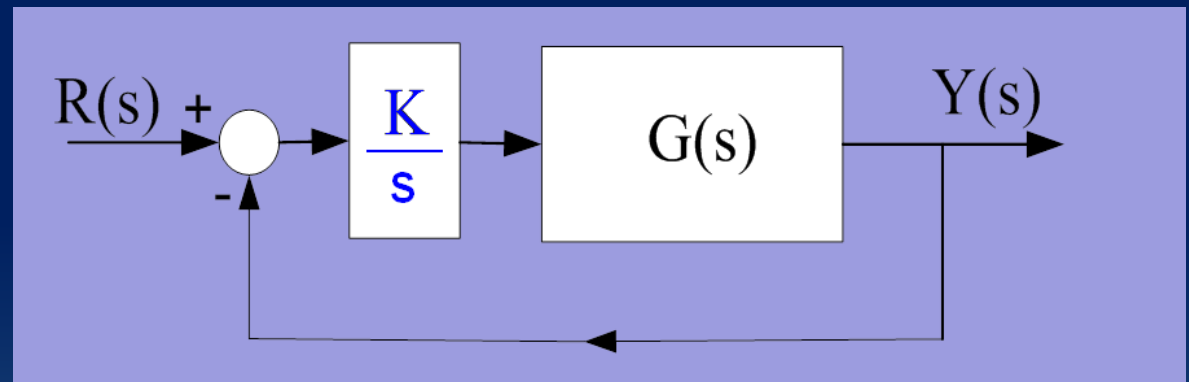
Using K/s , we get a
“integral controller” or a
“type I controller”.

$$G(s) = \frac{2}{(s+1)}$$

the same as in the
 previous example

Example 7: (continued)

$$R(s) = \frac{1}{s}$$



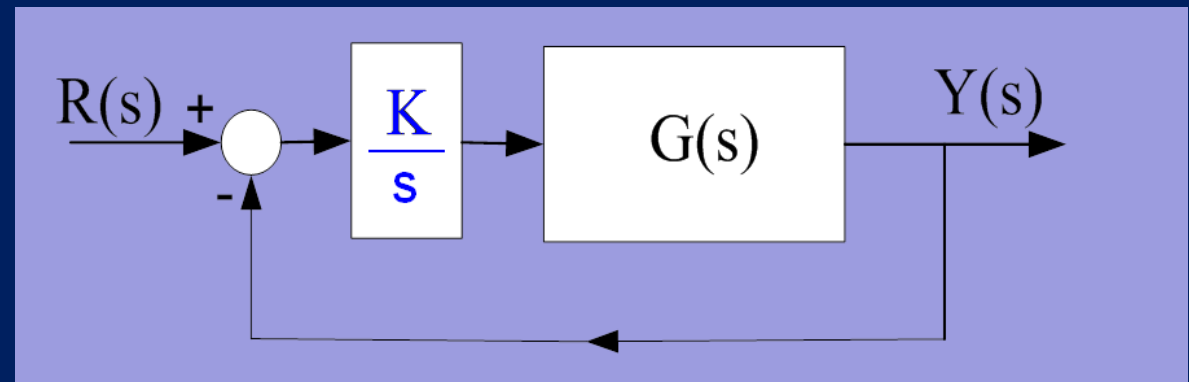
error $e(t)$

$$\begin{aligned}
 E(s) &= \frac{R(s)}{[1 + G(s)H(s)]} \\
 &= \frac{1/s}{\left[1 + \frac{2K}{s(s+1)}\right]} \\
 &= \frac{(s+1)}{(s^2 + s + 2K)}
 \end{aligned}$$

error in
steady state e_{ss}

$$\begin{aligned}
 e_{ss} &= \lim_{s \rightarrow 0} s \cdot E(s) = \\
 &= \lim_{s \rightarrow 0} s \cdot \frac{(s+1)}{(s^2 + s + 2K)} \\
 &= 0
 \end{aligned}$$

Example 7: (continued)

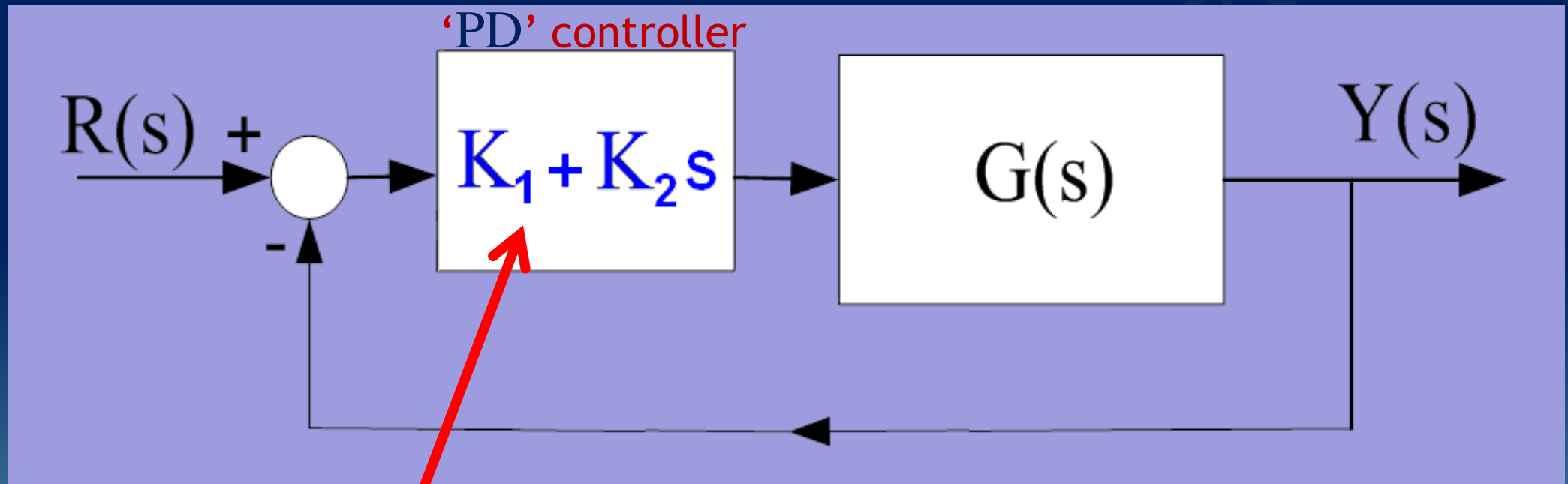


thus, now it is possible, for example, to adjust K such that the *steady state error* is

$$e_{ss} = 0$$

we should choose $K > 0$

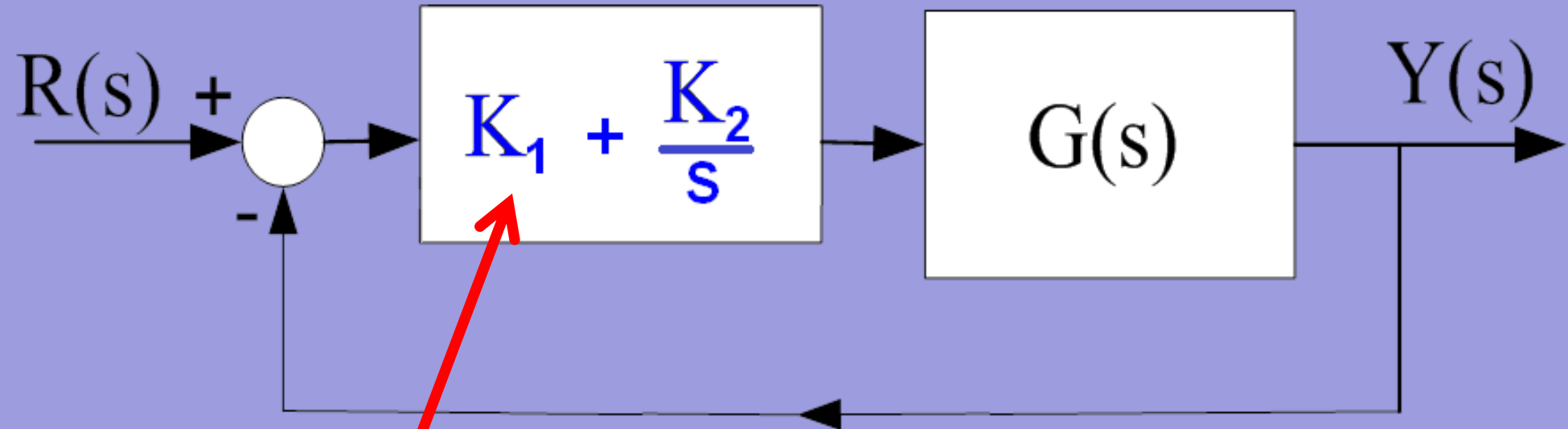
There are several types of controllers



Using $K_1 + K_2 s$, we get a
“*proportional derivative controller*”
or a “*type PD controller*”

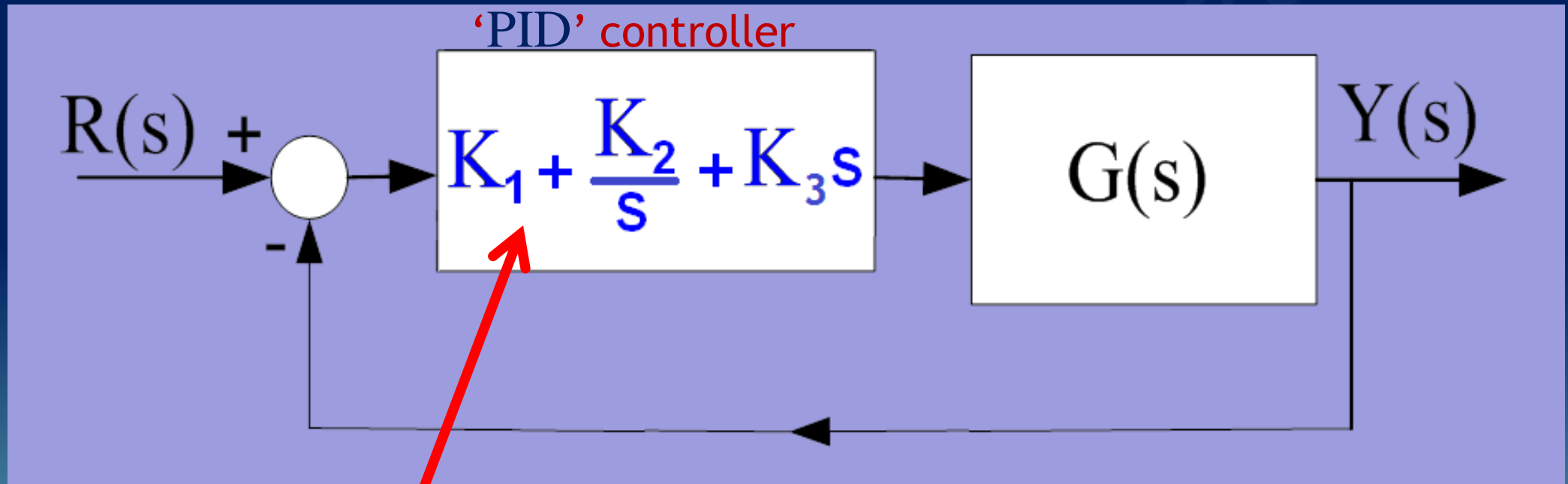
There are several types of controllers

‘PI’ controller

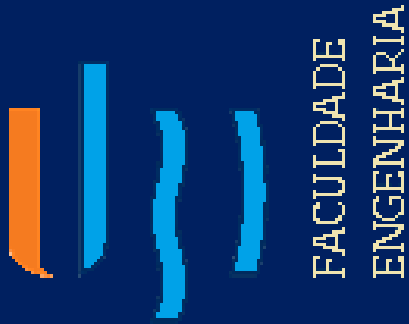


Using $K_1 + K_2/s$, we get a
“*proportional integral controller*”
or a “*type PI controller*”

The most general case is a 'PID controller'



Using $K_1 + K_2/s + K_3s$, we get a
“*proportional integral derivative controller*”
or a “*type PID controller*”



Departamento de
Engenharia Eletromecânica

Thank you!

Felippe de Souza

felippe@ubi.pt